

AD-A061 854

ARGONNE NATIONAL LAB ILL

F/G 1/5

AIRPORT VICINITY AIR POLLUTION MODEL ABBREVIATED VERSION USER'S--ETC(U)

SEP 78 L A CONLEY, D M ROTE

DOT-FA71WA1-223

UNCLASSIFIED

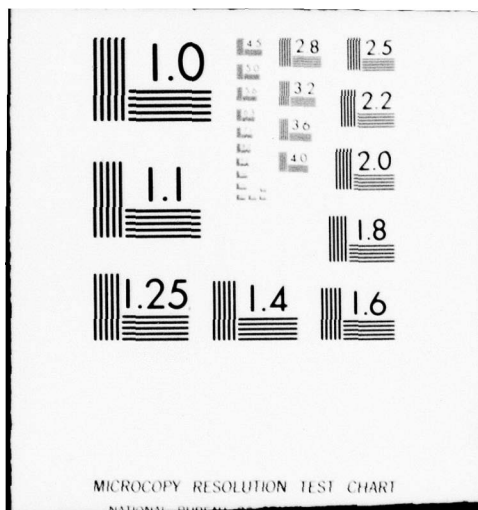
FAA-RD-78-111

NL

1 OF 2

AD
A061854





(12) LEVEL II



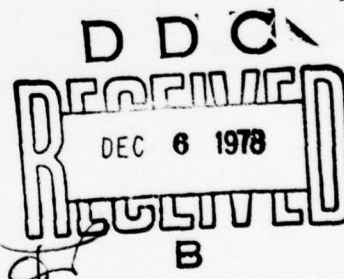
AD A061854

Report No. FAA-RD-78-111

**AIRPORT VICINITY AIR POLLUTION MODEL
ABBREVIATED VERSION
USER'S GUIDE**

L.A. Conley D.M. Rote
Argonne National Laboratory
9700 South Cass Avenue
Argonne, Illinois 60439

DDC FILE COPY



**September 1978
Final Report**

Document is available to the U.S. public through
the National Technical Information Service,
Springfield, Virginia 22161.

Prepared for
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL AVIATION ADMINISTRATION
Systems Research & Development Service
Washington, D.C. 20590

78 12 04.056

NOTICE

This document is disseminated under the sponsorship of the Department of Transportation in the interest of information exchange. The United States Government assumes no liability for its contents or use thereof.

Technical Report Documentation Page

1. Report No. 18 FAA-RD-78-111	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle 6 AIRPORT VICINITY AIR POLLUTION MODEL ABBREVIATED VERSION USER'S GUIDE.	5. Report Date 11 September 1978	6. Performing Organization Code
7. Author(s) 10 L.A. Conley D.M. Rote	8. Performing Organization Report No.	9. Performing Organization Report No.
9. Performing Organization Name and Address Argonne National Laboratory 9700 South Cass Avenue Argonne, Illinois 60439	10. Work Unit No. (TRAIS)	11. Contract or Grant No. 15 DOT-FA71WA 1-223
12. Sponsoring Agency Name and Address U.S. Department of Transportation Federal Aviation Administration Systems Research and Development Service Washington, D.C. 20590	13. Type of Report and Period Covered 9 Final Report	14. Sponsoring Agency Code ARD-550
15. Supplementary Notes	12 125 p.	
16. Abstract This document describes the Airport Vicinity Air Pollution (AVAP) Model modified by the Energy and Environmental Systems Division of Argonne National Laboratory for the Federal Aviation Administration under Inter-Agency Agreement DOT-FA71WA1-223. This version of the model, Airport Vicinity Air Pollution Model Abbreviated Version, provides a "first-guess" estimate of an airport air pollution distribution based on more general input information than is described in Report No. FAA-RD-75-230, the model's primary form. The user must establish a right-handed Cartesian coordinate system as a basis for describing an airport layout, then decide whether to use supplied default values applicable to the types of aircraft and airport facilities. The estimate of pollutant concentrations are computed for selected individual receptor locations based on the dispersion of pollutant emissions from area and line type sources. Pollutant emission levels due to each member of a source type are tabulated. The results of a one one-hour modeling period of aircraft arrival-departure activities, airport ground-support services, and airport access vehicle roadways are tabulated for each receptor location and pollutant species. The document presents a discussion of the theoretical considerations fundamental to the AVAP Model Abbreviated Version as well as program flow diagrams essential to understanding the theory. Required sequential card data input to the program is illustrated along with substitution options for program constants. Additionally, an example problem and a program listing are provided.		
17. Key Words Airport Vicinity Air Pollution Modeling Engines Pollutant Emission		18. Distribution Statement Document is available to the U.S. public through the National Technical Information Service, Springfield, Virginia 22161.
19. Security Classif. (of this report) UNCLASSIFIED	20. Security Classif. (of this page) UNCLASSIFIED	21. No. of Pages 125
		22. Price

METRIC CONVERSION FACTORS

Approximate Conversions to Metric Measures				Approximate Conversions from Metric Measures			
Symbol	When You Know	Multiply by	To Find	Symbol	When You Know	Multiply by	To Find
LENGTH				LENGTH			
in	inches	2.5	centimeters	mm	millimeters	0.04	inches
ft	feet	30	centimeters	cm	centimeters	0.4	inches
yd	yards	0.9	meters	m	meters	3.3	feet
mi	miles	1.6	kilometers	km	kilometers	0.6	miles
AREA				AREA			
m ²	square inches	6.5	square centimeters	cm ²	square centimeters	0.16	square inches
ft ²	square feet	0.09	square meters	m ²	square meters	1.2	square yards
yd ²	square yards	0.8	square meters	km ²	square kilometers	0.4	square miles
mi ²	square miles	2.6	square kilometers	ha	hectares (10,000 m ²)	2.5	acres
MASS (weight)				MASS (weight)			
oz	ounces	28	grams	g	grams	0.035	ounces
lb	pounds	0.45	kilograms	kg	kilograms	2.2	pounds
	short tons (2000 lb)	0.9	tonnes	t	tonnes (1000 kg)	1.1	short tons
VOLUME				VOLUME			
teaspoon	teaspoons	5	milliliters	ml	milliliters	0.03	fluid ounces
fl oz	fluid ounces	30	milliliters	l	liters	2.1	pints
c	cups	0.24	liters	l	liters	1.06	quarts
pt	pints	0.47	liters	l	liters	0.26	gallons
qt	quarts	0.95	liters	m ³	cubic meters	35	cubic feet
gal	gallons	3.8	liters	m ³	cubic meters	1.3	cubic yards
ft ³	cubic feet	0.03	cubic meters				
yd ³	cubic yards	0.76	cubic meters				
TEMPERATURE (exact)				TEMPERATURE (exact)			
°F	Fahrenheit temperature	5/9 (after subtracting 32)	Celsius temperature	°C	Celsius temperature	9/5 (then add 32)	Fahrenheit temperature

* 1 in = 2.54 exactly. For other exact conversions and more data and tables, see NBS Mon. Publ. 286, Units of Weight and Measure, Price \$2.25, SO. Carolina No. C-110-286.

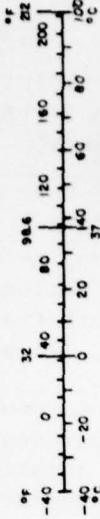


TABLE OF CONTENTS

	<u>Page</u>
1. Introduction	3
2. Formulas for Concentration Calculations	5
2.1 Dispersion Coefficients σ_y and σ_z	5
2.2 Point Source Dispersion Equations	5
2.3 Area Source Dispersion Equations	11
2.4 Finite Line Source Dispersion Equations	12
2.5 Wind Profile Law	13
2.6 Effects of Sky Lid	14
3. Description of Input Data	17
4. Description of Default Data	25
5. Example Problem	32
5.1 Introduction	32
5.2 Statement of the Problem	32
5.3 Summary of the Problem	34
5.4 Listing of Example Problem's Input Data Deck	36
5.5 Listing of Example Problem's Output	37
References	41
Appendix A Concentration Conversions	A-1
Appendix B Flow Diagrams	
Main	B-1
Function CAVL	B-16
Subroutine QMOD	B-29
Function TRAN	B-33
Appendix C FORTRAN listing of the AVAP Model, Abbreviated Version Program	C-1

ACCESSION for	
NTIS	White Section <input checked="" type="checkbox"/>
DDC	Buff Section <input type="checkbox"/>
UNANNOUNCED	<input type="checkbox"/>
JUSTIFICATION _____	
BY _____	
DISTRIBUTION/AVAILABILITY CODES	
Dist. _____ and/or SPECIAL	
A	

1 INTRODUCTION

The Airport Air Pollution Model, Abbreviated Version was developed at Argonne National Laboratory and executed on the IBM 360 Model 195 within a core region of 250K bytes while utilizing less than one minute of computer time. The FORTRAN coded program is yet another version of the Airport Air Pollution (AVAP) Model¹ modified to provide a first-guess estimate of an airport air pollution distribution.

This document discusses the theoretical considerations fundamental to the model, describes data input requirements for using the program, and illustrates the use of model by presenting an example problem. Therefore, users of the document should be technical personnel concerned with using the computer code for assessing air pollution impacts of commercial and general aviation airports. For more comprehensive studies, the model's primary form should be used.

In Section 2, the collection of formulas that form the basis of the computer program are presented. Detailed descriptions are to be found for area source and line source dispersion formulas. Although they are not used in this abbreviated version of AVAP, the Gaussian plume formula for a point source, the Carson-Moses plume rise formula, and the Briggs formula for estimating stack downwash effects are presented.

Section 3 provides guidelines for preparation of the input data. The formats and meanings of the input parameters are given along with their relative card position in the input sequence. Almost all of the input parameters that appear in this section have default values. Those that do not have default values are marked in Table 3.1. with the asterisk (*) character.

Section 4 provides a description and a table of the default values of the input parameters. All of the default values appear in the BLOCK DATA subprogram of the computer program; all or some of them can be changed by the appropriate data-card insertion.

PRECEDING PAGE BLANK

Section 5 presents a complete example problem that details the resultant output from the model. Appendix A illustrates the conversion of pollutant concentration units and Appendix B gives the program flow diagrams of selected computational modules.

A complete listing of the FORTRAN coded program is found in Appendix C.

2 FORMULAS FOR CONCENTRATION CALCULATIONS

The formulas presented in this section will apply to both forms of the AVAP Model except that Point Source calculations are not required when using the abbreviated version. They form an outline of the most basic set of equations for concentration calculations but are not to be regarded as the complete set that covers all practical conditions of application. The user of the AVAP Model should consult the references quoted in this document for more complete descriptions.

2.1 DISPERSION COEFFICIENTS σ_y and σ_z

The dispersion coefficients σ_y and σ_z (miles) indicate the amount the pollutant plume has spread (dispersed) after leaving its source. To avoid unrealistic behavior of the σ functions at very high and very low wind speeds, the following formulas are used:

$$\sigma_y \equiv \sigma_y(T) = \text{Max} [\sigma_{yT}(T), \sigma_{yx}(x)], \quad (1)$$

$$\text{and } \sigma_z \equiv \sigma_z(T) = \text{Max} [\sigma_{zT}(T), \sigma_{zx}(x)], \quad (2)$$

where x is the downwind distance and $T = x/u$ is the travel time. In Eqs. (1) and (2), $\sigma_{yT}(T)$ and $\sigma_{zT}(T)$ denote the travel-time-dependent dispersion coefficients. Curves of $\sigma_{yT}(T)$ for different Turner stability classes are displayed in Figure 2.1. Turner's original values for two-hour sampling time have been converted to one-hour sampling time by multiplication with the factor $(1/2)^{0.2} = 0.87$. No conversion factor for sampling time is applied to the $\sigma_{zT}(T)$ values which are plotted in Figure 2.2. Figures 2.3 and 2.4 show the downwind-distance-dependent dispersion coefficients $\sigma_{yx}(x)$ and $\sigma_{zx}(x)$ derived from curves in Turner's Workbook for 10-minute sampling time, by multiplying the original $\sigma_{yx}(x)$ values by $(60/10)^{.2}$ and the original $\sigma_{zx}(x)$ values by $(20/10)^{.2}$. In doing so we have assumed that the vertical dispersion coefficient is insensitive to sampling times beyond 20 minutes, as suggested by Slade.

2.2 POINT SOURCE DISPERSION EQUATIONS

The short-term average concentration χ_p at the receptor point (x, y, z) due to a point source at

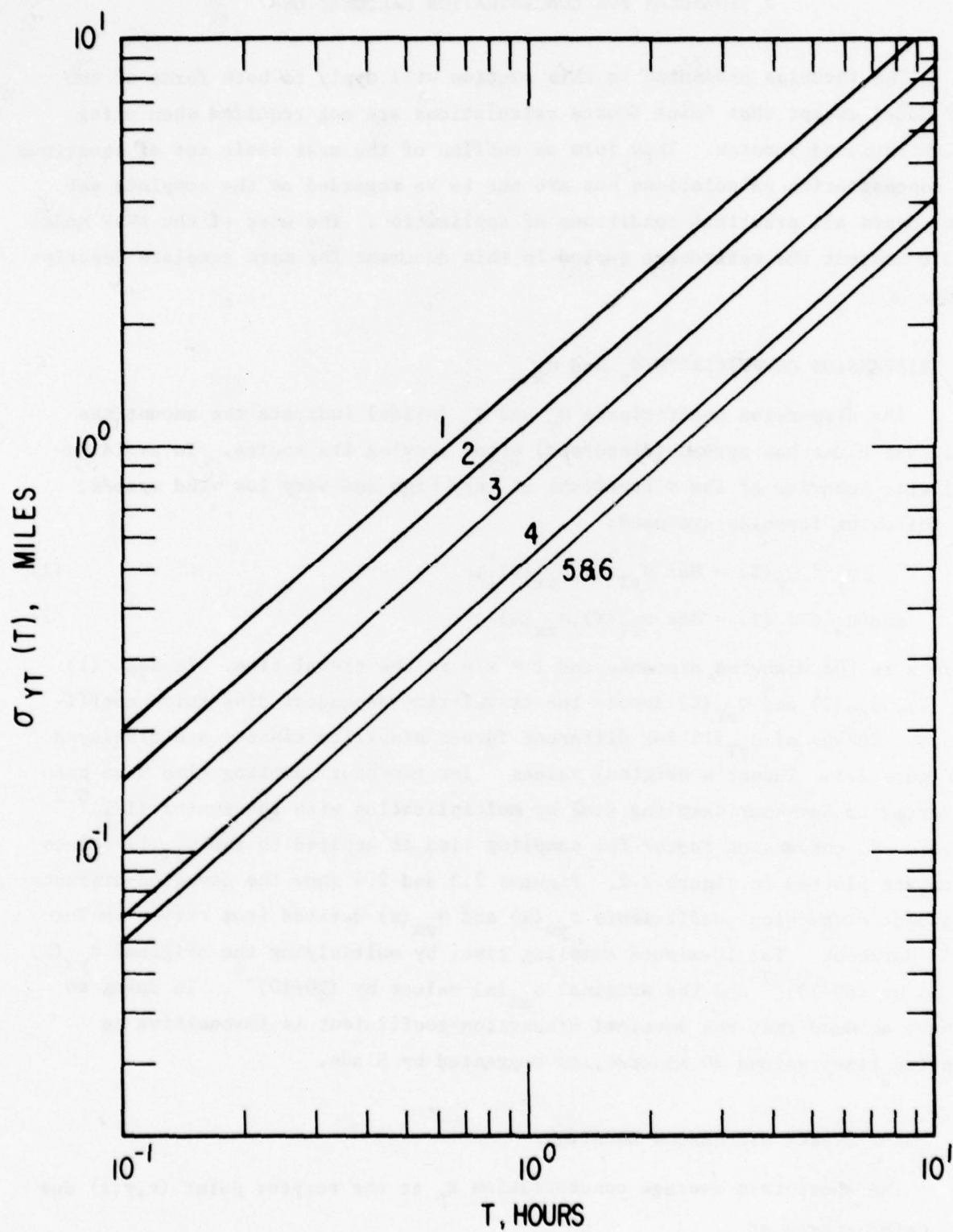


Figure 2.1. Time-Dependent Horizontal Dispersion Coefficients for 1-Hour Sampling Time.

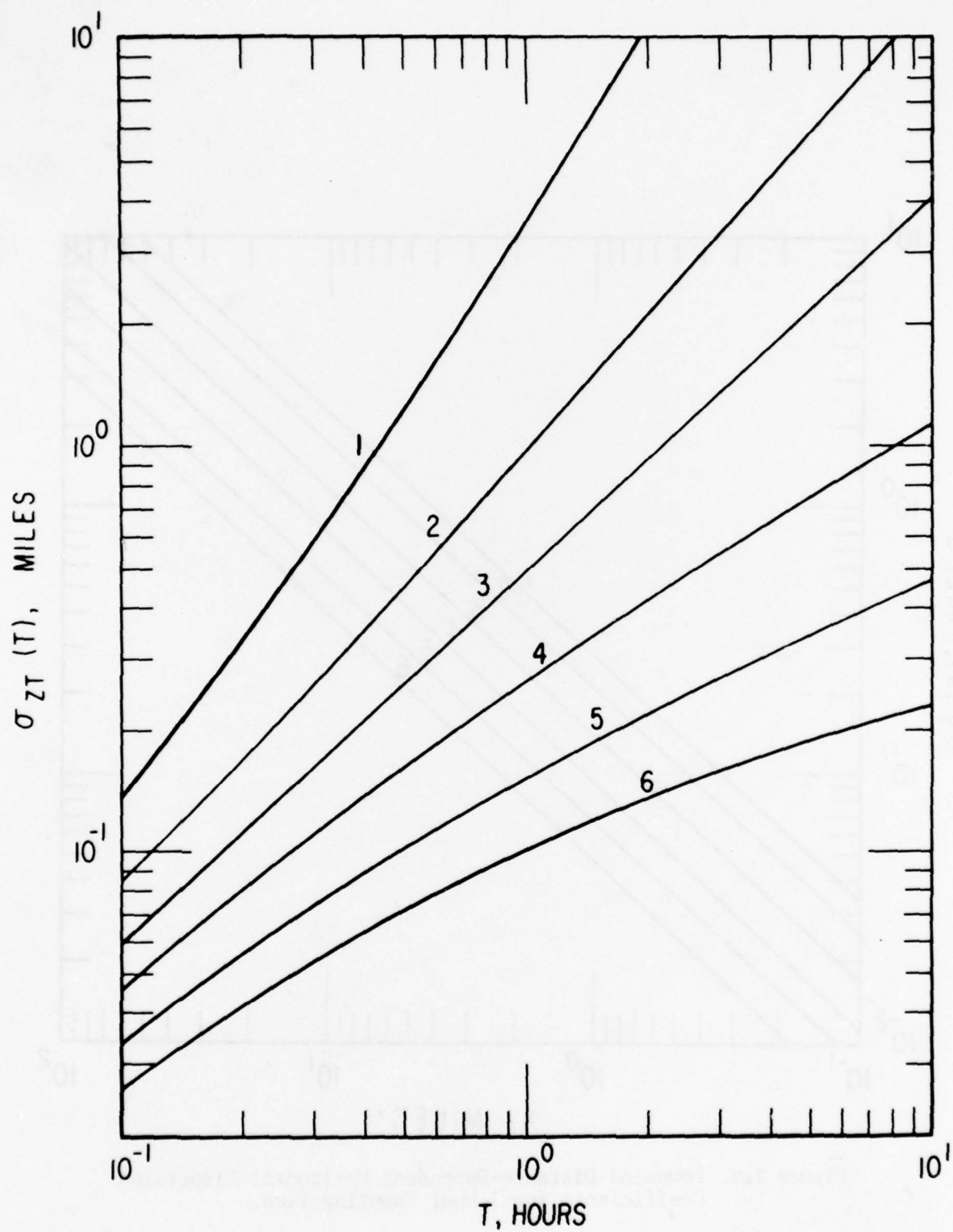


Figure 2.2. Time-Dependent Vertical Dispersion Coefficients for 1-Hour Sampling Time.

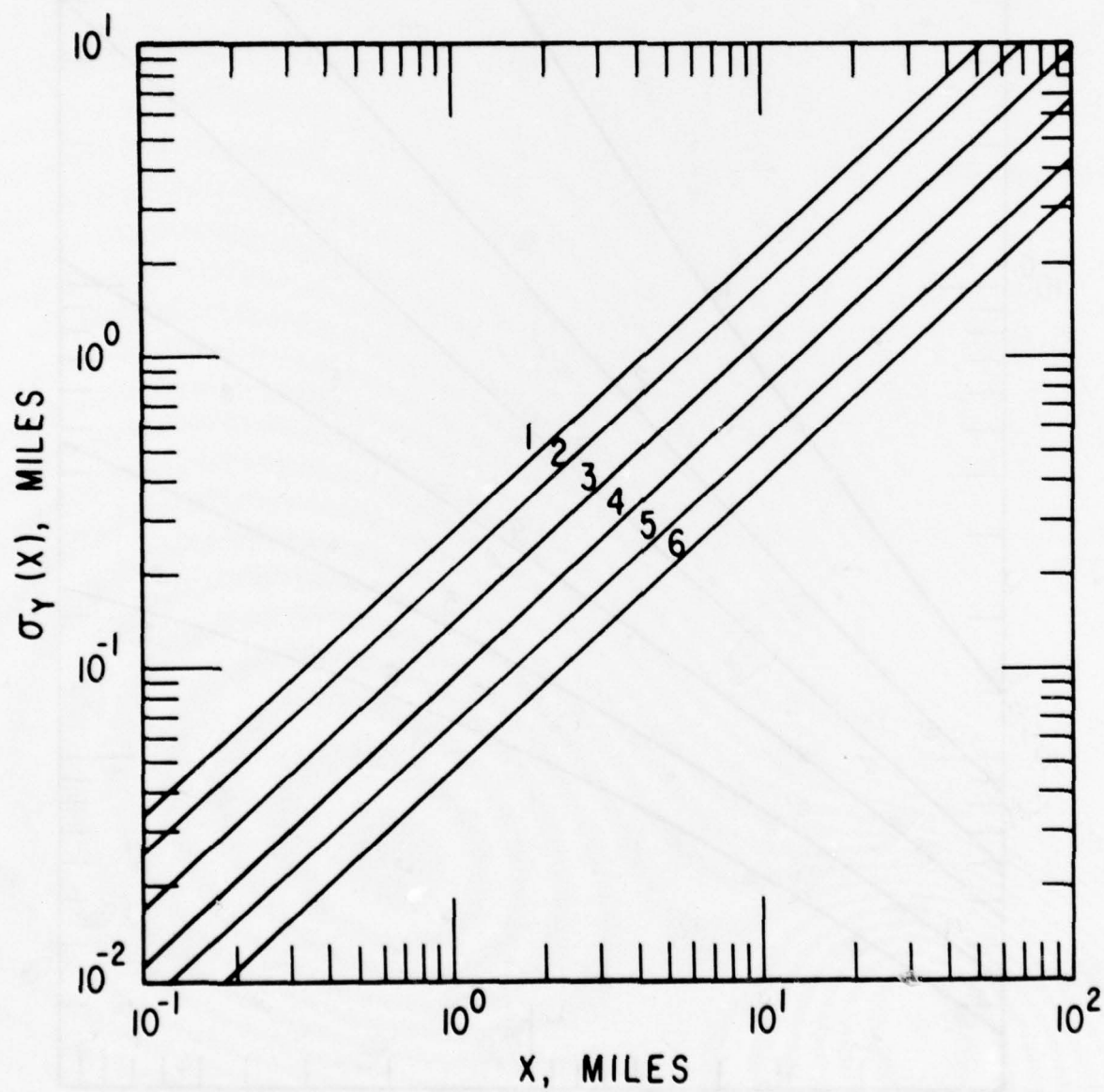


Figure 2.3. Downwind-Distance-Dependent Horizontal Dispersion Coefficients for 1-Hour Sampling Time.

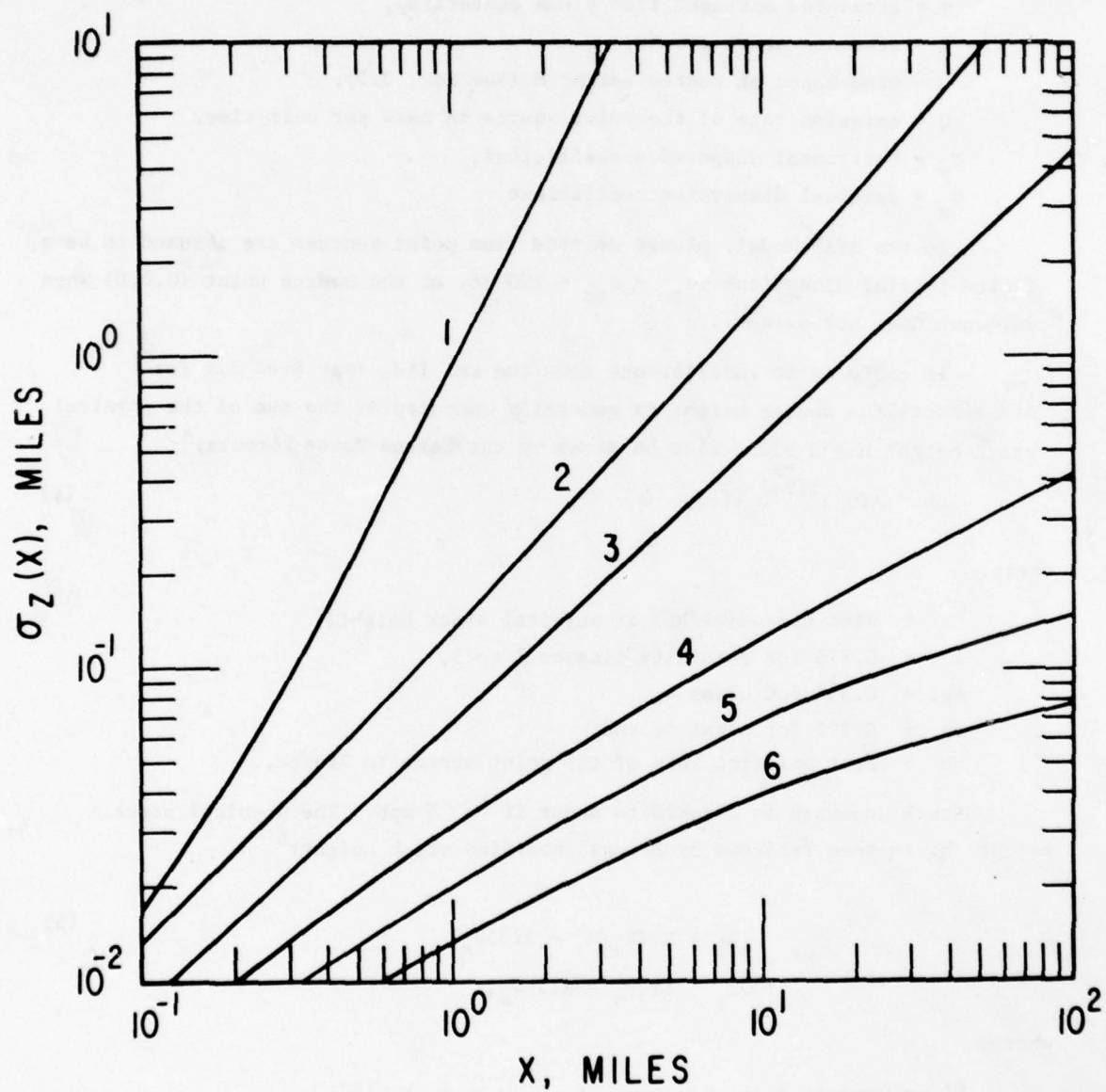


Figure 2.4. Downwind-Distance-Dependent Vertical Dispersion Coefficients for 1-Hour Sampling Time.

$$x_p = \frac{Q}{2\pi u \sigma_y \sigma_z} \exp \left[-\frac{1}{2} \left(\frac{y}{\sigma_y} \right)^2 \right] \cdot \left\{ \exp \left[-\frac{1}{2} \left(\frac{Z-H}{\sigma_z} \right)^2 \right] + \exp \left[-\frac{1}{2} \left(\frac{Z+H}{\sigma_z} \right)^2 \right] \right\}. \quad (3)$$

where

y = crosswind distance from plume centerline,

Z = distance above ground,

u = wind speed at source height H (See Sec. 2.5).

Q = emission rate of the point source in mass per unit time,

σ_y = horizontal dispersion coefficient,

σ_z = vertical dispersion coefficient

In the AVAP Model, plumes emitted from point sources are assumed to have finite initial dimensions ($\sigma_{y0} = \sigma_{z0} = 100$ ft. at the source point (0,0,H) when downwash does not appear).

If there is no interference from the sky lid, (see Sec. 2.6 for its effects) the source height is generally computed as the sum of the physical stack height h and plume rise Δh given by the Carson-Moses formula:⁵

$$\Delta h = A(Q_h)^{1/2} / U_s \text{ (ft)}, \quad (4)$$

where:

U_s = wind speed (mi/hr) at physical stack height,

A = 0.870 for stability classes 1 to 3,

sgl = 0.354 for class 4,

sp = 0.222 for class 5, and

Q_h = heat emission rate of the point source in Btu/hr.

Stack downwash is assumed to occur if $U_s > 6$ mph. The physical stack height h is then replaced by Briggs' modified stack height:⁶

$$h' = \begin{cases} Z_s + 2 (V_s / U_s - 1.5) D_s, \\ Z_s \quad \text{if } V_s > 1.5 U_s, \end{cases} \quad (5)$$

where:

h' = modified stack height after stack downwash,

V_s = stack effluent velocity, and

D_s = stack diameter.

Also, with stack downwash the initial plume dimensions are reassigned in the AVAP Model to simulate average city block size and building height ($\sigma_{y0} = 250$ ft; $\sigma_{z0} = 40$ ft).

For point sources with poor aerodynamic characteristics, such as vents or very short stacks on buildings, σ_{y0} is automatically assumed to be 250 ft and the building height h is used to compute σ_{z0} ($\sigma_{z0} = h/1.2$). If h is not supplied by the user the default value of 40 ft is used for σ_{z0} .

2.3 AREA SOURCE DISPERSION EQUATIONS

In the AVAP Model, two sets of dispersion equations are used for area sources. For convenience, area sources are classified as "near" sources and "far" sources depending on the relative location of the receptor and the area source.

First, the critical distance for mixing, x_c , is computed from the mixing height value L by the equation

$$\sigma_z(T = x_c/u) = 0.47 L. \quad (6)$$

If the critical distance measured upwind from the receptor is downwind of the downwind edge of the area source, the area source is defined as a "far" source. If the critical distance measured upwind from the receptor extends beyond the upwind edge of the source, the entire area source is treated as "near." There will be cases in which an area source is partitioned into a "near" and a "far" source relative to the receptor. The detailed logic for area source classification is presented in Appendix B on p. B-14.

The far area sources are treated conventionally, with the horizontal and vertical dispersions represented separately, each by an upwind virtual point source, so that at the downwind edge of the area source $\sigma_y = \sigma_{y0}$ and at the center $\sigma_z = \sigma_{z0}$. For an area source of side length d and vertical spread h , the initial Gaussian widths are given by $\sigma_{y0} = d/2.4$ and $\sigma_{z0} = h/1.2$.

For a complete discussion of the treatment of near area sources, the reader is referred to a separate report.⁷ Briefly, it is to treat the area source in such a manner that the z component is represented by an upwind virtual line segment along the wind direction instead of a single point, with the simplifying assumption that σ_y is held constant over the area source. The z - component is analytically integrated over the line segment. Therefore, for receptor locations immediately downwind of the area source, the model is expected to give more realistic concentration profiles than the conventional area source model.

The short-term average concentration χ_a at the receptor point (x,y,z) , due to an area source having its geometrical center at $(0,0,z_a)$, is given by

$$\chi_a = \frac{Q_a \cdot F}{2\pi \sigma_y d(1-b)} \exp \left[-\frac{1}{2} \left(\frac{y}{\sigma_y} \right)^2 \right] \cdot \left\{ \exp \left[-\frac{1}{2} \left(\frac{z - z_a}{\sigma_z(T_2)} \right)^2 \right] + \exp \left[-\frac{1}{2} \left(\frac{z + z_a}{\sigma_z(T_2)} \right)^2 \right] \right\}, \quad (7)$$

where,

$$F = \frac{T_2}{\sigma_z(T_2)} - \frac{T_1}{\sigma_z(T_1)},$$

$$b = \frac{\ln(\sigma_z(T_1)/\sigma_z(T_2))}{\ln(T_1/T_2)}$$

If $b = 1$, the factor $F/(1-b)$ in Eq. 7 should be replaced by $T_1 \ln(T_2/T_1)/\sigma_z(T_1)$.

In the above equations, T_1 denotes the sum of T_z (pseudo travel time corresponding to σ_{z0}) and the travel time from the downwind edge of the area source to the receptor, and T_2 denotes the sum of T_z and the travel time from the upwind edge of the area source to the receptor. If the receptor is inside the area source, $T_1 = 0$. σ_y is computed with a travel time so that $\sigma_y = d/2.4$ at the downwind edge of the source, or if the receptor is inside the source it is assumed to be $d/2.4$ at the receptor.

2.4 FINITE LINE SOURCE DISPERSION EQUATIONS

The short-term average concentration χ_ℓ at the receptor point (x,y,z) due to a finite line source with inclination angle θ relative to ground, azimuthal angle ϕ relative to the wind vector and its end points at $(0,0,0)$ and $(L \cos \theta \cos \phi, L \cos \theta \sin \phi, L \sin \theta)$ is given by

$$\chi_\ell = \frac{q_\ell}{2\pi u \bar{\sigma}_y \bar{\sigma}_z} \cdot J, \quad (8)$$

with

$$J = (\sqrt{\pi}/2) \cdot A \cdot \sum_{i=1}^2 \left\{ \exp(B_i^2 - C_i^2) \left[\operatorname{erf}(B_i + L/A) - \operatorname{erf}(B_i) \right] \right\}$$

where

$$A = \sqrt{2} \bar{\sigma}_y \bar{\sigma}_z (\cos^2 \theta \sin^2 \phi \bar{\sigma}_z^2 + \sin^2 \theta \bar{\sigma}_y^2)^{-1/2}$$

$$\begin{aligned}
B_1 &= -2 \left(\bar{\sigma}_y \bar{\sigma}_z \right)^{-2} \cdot A. \left[y \cos \theta \sin \phi \bar{\sigma}_z^2 + (Z-H) \sin \theta \bar{\sigma}_y^2 \right], \\
B_2 &= -2 \left(\bar{\sigma}_y \bar{\sigma}_z \right)^{-2} \cdot A. \left[y \cos \theta \sin \phi \bar{\sigma}_z^2 + (Z+H) \sin \theta \bar{\sigma}_y^2 \right], \\
C_1 &= \left[\frac{y^2}{2\bar{\sigma}_y^2} + \frac{(Z-H)^2}{2\bar{\sigma}_z^2} \right]^{1/2}, \\
C_2 &= \left[\frac{y^2}{2\bar{\sigma}_y^2} + \frac{(Z+H)^2}{2\bar{\sigma}_z^2} \right]^{1/2}.
\end{aligned}$$

The above formula is applicable only under certain conditions. For a complete discussion of the various criteria and the reasons behind them, the user is referred to Refs. 8 and 9. Normally, when the line source subtends a sufficiently large angle relative to the wind vector, for example, a uniform, horizontal line with ϕ greater than 45° , the formula is used without the segmentation scheme discussed in the references mentioned above. The dispersion coefficients $\bar{\sigma}_y$ and $\bar{\sigma}_z$ are evaluated with an effective downwind distance corresponding to a point on the line that is directly upwind of the receptor. When the relative angle is very small ($\leq 10^\circ$), the following approximation formula is used:

$$\chi_{\ell o} = \frac{1}{2\sqrt{2}\pi} \left(\frac{q_{\ell L}}{u} \right) \left(\bar{\sigma}_y \bar{\sigma}_z \right)^{-1} \exp \left[- \frac{y^2}{2\bar{\sigma}_y^2} - \frac{z^2}{2\bar{\sigma}_z^2} \right]. \quad (9)$$

Again, for a long line source, the line is divided into shorter segments, and an effective $\bar{\sigma}_y$ and $\bar{\sigma}_z$ for each segment is evaluated for the downwind distance corresponding to the midpoint of the segment. For angles between 10° and 45° Eq. 8 is used with the segmentation scheme.

2.5 WIND PROFILE LAW

To convert the wind speed measured by anemometer at a local airport (typically 30 ft above ground) to that at the physical stack height h or to that at the effective source height H we use a power law relation of the form:

$$u(Z) = u(Z_o) (Z/Z_o)^P. \quad (10)$$

The exponent P, as determined by DeMarrais¹⁰, depends on the stability class and is given in Table 2.1.

Table 2.1 Exponents for Wind Profile

Stability Class		P
Unstable	(<3)	0.2
Neutral	(4)	0.3
Stable	(5)	0.4
Very Stable	(6)	0.5

2.6 EFFECTS OF SKY LID

The lower surface of an elevated inversion layer is referred to as the sky lid, and as a rough approximation it is assumed to act as a perfect reflector. Thus the plume would generally be reflected repeatedly from two parallel surfaces, the ground and the sky lid. If the reflected plumes from a point source are represented by multiple image sources (see Fig. 2.5), then the net concentration at the receptor can be expressed in terms of a multiple image series:

$$\chi_p = \sum_{i=0}^N \chi_{pi}, \quad (11)$$

where χ_{po} = concentration due to original source, and

χ_{pi} = concentration due to i^{th} image source.

The above formula is used with $N = 6$ (i.e., three image sources below ground and three above the sky lid) when the downwind distance x of the receptor from the source is less than $2 x_c$ as calculated from Eq.(6). For downwind distances $x \geq 2 x_c$, the net concentration is calculated with the assumption of full mixing in the mixing layer, and

$$\chi_p = \frac{Q}{\sqrt{2\pi} Lu \sigma_y} \exp \left[-1/2 \left(\frac{y}{\sigma_y} \right)^2 \right]. \quad (12)$$

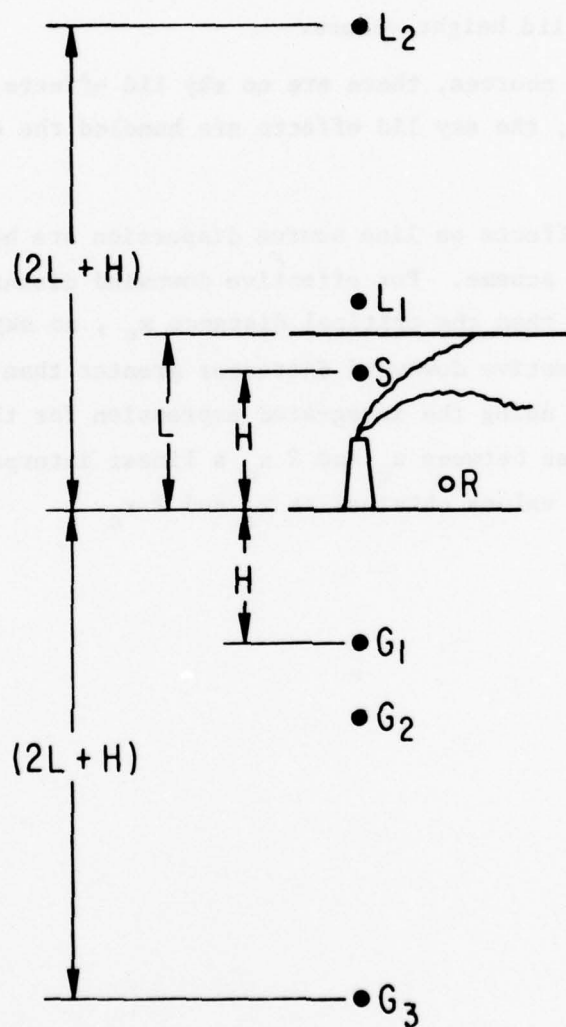


Figure 2.5. Multiple Reflections Between a Stable Layer and Ground Represented by Two Sets of Image Sources.

For some point sources (e.g., power plants with tall stacks), the calculated effective emission height H may be greater than the lid height, especially when the latter is small. These cases are not eliminated from consideration in the AVAP Model, but are simulated by using dispersion coefficients and plume rise for stably stratified air (stability class 5). Depending on the relative position of the lid, the physical stack height, and the computed effective stack height, the model will in some cases reassign the effective stack height or the lid height values.

For near area sources, there are no sky lid effects by definition. For far area sources, the sky lid effects are handled the same way as the point sources.

The sky lid effects on line source dispersion are handled by a simple linear interpolation scheme. For effective downwind distances (see Section 2.4 for definition) less than the critical distance x_c , no sky lid effects are assumed; and for effective downwind distances greater than $2 x_c$, uniform vertical mixing is assumed by using the integrated expression for the Z-component. For downwind distances between x_c and $2 x_c$ a linear interpolation is applied to the concentration values obtained at x_c and $2 x_c$.

3 DESCRIPTION OF INPUT

The first six (6) cards in the data deck (see Table 3.1) are the problem title and program parameter input cards required for every application of the model.

Card 1 is a single card of input having no computational value internal to the code. It may be punched or left blank. If punched, the same will appear as the first line of printed output.

Card 2 provides at least one identifying symbol chosen from the following set:

- CO - Carbon Monoxide
- THC - Total Hydrocarbons
- NOX - Nitrogen Oxides
- PART - Total Suspended Particulate

If the card is multiply punched, the program will calculate in turn the estimates of pollutant concentrations corresponding to the specified species.

Card 3 will provide the necessary meteorological data. Of the entries made on this card, the atmospheric stability index (JSTAB) should be deduced on the basis of wind speed, cloud cover, time of the day and other isolation parameters according to the scheme outlined by Turner¹³. Then lid height (NLID), if not obtainable by processing local sounding data, is estimated on the basis of JSTAB and the monthly average afternoon maximum mixing depths (meters above surface) tabulated by Holzworth¹¹. The twelve (12) average values that are directly coded into the program (FUNCTION HMIX) apply to the Washington, D.C., region and are ordered by month (NMONTH) as follows: 400, 570, 1000, 930, 1120, 1310, 1180, 990, 980, 570, 680, and 480 (meters).

Card 4 provides an accounting of the receptors (points at which the model must estimate the pollutant concentration), the aircraft and aircraft-engine types, and the airport-access vehicle roadways. The aircraft area source comprises four emission sources: (1) ground service vehicles, (2) auxiliary powerunits, (3) aircraft taxi within the area, and (4) aircraft-engine idle within the area. Therefore, an entry should exclude the aircraft area source (NACA=0) whenever the effects of all the above emission sources are suppressed. The non-aircraft area source is assigned pollutant emission levels later in the input stream, but may be excluded by setting NANA to zero (0).

Card 5 provides the indicators for user selected input. All of the punched card columns require that all corresponding card numbers, punched with all associated data, appear in the appropriate order of the input stream. For example, columns 18 and 21 are punched in order to indicate that card number 10 and card number 11 will appear in the input stream (see Table 3.1). Both of these bears entries for the number of engines with which each aircraft type is equipped, and the second bears entries that indicate the engine types.

Card 6 provides the location of specific receptor points.

The remainder of the input data deck is described in a list form in order to identify clearly those cards that are required for every application of the model and those cards that are used to over-ride program default values.

Card 7 thru Card 11	Refer to default values on page 27.
Card 12	Refer to default values on page 28.
Card 13	Refer to default values on page 30.
Card 14	Airport runway coordinates are always present.
Card 15	Refer to default values on page 30.
Card 16 thru Card 18	Refer to default values on page 29.
Card 19	Refer to default values on page 30.
Card 20 and Card 21	Airport taxiway coordinates are always present.
Card 22	Refer to default values on page 30.
Card 23 and 24	Runway apron coordinates are always present.
Card 25 thru Card 27	Refer to default values on page 30.
Card 28	Is required for access vehicle roadway coordinates.
Card 29	Is required for airport terminal area coordinates.
Card 30 and Card 31	Refer to default values on page 30.
Card 32	Refer to default values on page 31.
Card 33	Refer to default values on page 29.
Card 34	Refer to default values on page 31.
Card 35 and Card 36	Refer to default values on page 29.
Card 37	Is required for airport non-aircraft area coordinates.
Card 38	Is required for airport non-aircraft area pollutant emission level.

Note that, for the hour of interest, the user specifies the number of arriving aircraft of each type in Card 7. The number of aircraft departing during that same hour is assumed equal to the number of arrivals.

Table 3.1. Card Input Sequence

Card Type	Columns	Format	Comment
1 (1 card)* TITLE	1-80	(20A4)	Title card may be punched or left blank.
2 (1 card)* CO THC NOx PART	1-2 5-7 9-11 13-16	(A4) (A4) (A4) (A4)	Four fields having four columns each are provided so that one or more pollutant species may be chosen for the model run.
3 (1 card)* HTAERO WSP DIR TEMP JSTAB NLID MONTH NR	1-8 9-16 17-24 25-32 33-40 41-48 49-50 51-52	F8.0 F8.0 F8.0 I8 I8 I2 I2	Height (feet) at which wind speed and direction are measured. Wind speed (knots). Wind direction (degrees). Ambient temperature (degrees F). Atmospheric stability index. Lid height (tens of feet). Month of year (required whenever NLID=0). Hour of day (required whenever NLID=0 and JSTAB=4).
4 (1 card)* NSR NACT NENT NAVR NACA NANA	 16-20 21-25 26-30 31-35 36-40 41-45	I5 I5 I5 I5 I5 I5 I5	The total number (≤ 20) of receptor locations at which the model must estimate pollutant levels The number (≤ 10) of different aircraft types (B727, T0, etc.) using airport facilities. The number (≤ 5) of different aircraft engine types (JT8D, TPE331) with which the above aircraft are equipped. The number (≤ 60) of motor vehicle roadways leading into the airport. 1 if aircraft area source is included. 0 otherwise. 1 if non-aircraft area source is included. 0 otherwise.
5 (1 card)+ DEFAULT =	1 9 2 12 3 15 4 18 5 21 6 24 7 27 8 30 9 33 10 35-36 11 38-39 12 41-42 13 44-45 14 47-48 15 50-51 16 53-54	 I3	If a blank or zero appears in any column the default value is used. Card 7 data -- user defined. Card 8 data -- user defined. Card 9 data -- user defined. Card 10 data -- user defined. Card 11 data -- user defined. Card 12 data -- user defined. Card 13 data -- user defined. Card 15 data -- user defined. Card 16 data -- user defined. Card 17 data -- user defined. Card 18 data -- user defined. Card 19 data -- user defined. Card 22 data -- user defined. Card 25 data -- user defined. Card 26 data -- user defined. Card 27 data -- user defined.

Table 3.1. Card Input Sequence (contd.)

Card Type	Columns	Format	Comment
	17 56-57		Card 30 data -- user defined.
	18 59-60		Card 31 data -- user defined.
	19 62-63		Card 32 data -- user defined.
	20 65-66		Card 33 data -- user defined.
	21 68-69		Card 34 data -- user defined.
	22 71-72		Card 35 data -- user defined.
	23 74-75		Card 36 data -- user defined.
5 (NSR cards)*			
NRUSED	1-2	I2	Any reference number.
XRECP	3-10	F8.0	X coordinate of receptor (mi
YRECP	11-18	F8.0	Y coordinate of receptor (mi
ZRECP	17-26	F8.0	Height of receptor (ft
7 (1 card)			
NAC(K)	6-55	(5X, 10I5)	NACT entries of the number of arriving aircraft of each type K. (Number of departures assumed to be the same as the number of arrivals).
8 (1 card)			
FLNDG(K)	6-55	(5X, 10F5.0)	NACT entries of time (hours) in landing mode for aircraft type K.
9 (1 card)			
FTKOF(K)	6-55	(5X, 10F5.0)	NACT entries of time (hours) in take-off mode for aircraft type K.
0 (1 card)			
NGIN(K)	6-55	(5X,10I5)	NACT entries for the number of engines with which aircraft type K is equipped.
1 (1 card)			
INGN(K)	6-55	(5X,10I5)	NACT entries for the engine type with which aircraft type K is equipped.
2 (NENT x 4 cards)			
EMI (I,J,K)	16-55	(15X, 5F10.0)	For each of the above engine types, enter an emission rate (lbs/hr) for each pollutant K (specified on card type 2). Cards 1 thru 4 for each engine type throttle setting will correspond to taxi, idle, landing and take-off modes, respectively.
3 (1 card)			
DSRW	16-25	F10.0	Width (mi) of initial dispersion on runway.
HRW	26-35	F10.0	Height (mi) of initial dispersion on runway.

Table 3.1. Card Input Sequence (contd.)

Card Type	Columns	Format	Comment
17	56-57		Card 30 data -- user defined.
18	59-60		Card 31 data -- user defined.
19	62-63		Card 32 data -- user defined.
20	65-66		Card 33 data -- user defined.
21	68-69		Card 34 data -- user defined.
22	71-72		Card 35 data -- user defined.
23	74-75		Card 36 data -- user defined.
6 (NSR cards)*			
NRUSED	1-2	I2	Any reference number.
XRECP	3-10	F8.0	X coordinate of receptor (mi
YRECP	11-18	F8.0	Y coordinate of receptor (mi
ZRECP	17-26	F8.0	Height of receptor (ft
7 (1 card)			
NAC(K)	6-55	(5X, 10I5)	NACT entries of the number of arriving aircraft of each type K. (Number of departures assumed to be the same as the number of arrivals).
8 (1 card)			
FLNDG(K)	6-55	(5X, 10F5.0)	NACT entries of time (hours) in landing mode for aircraft type K.
9 (1 card)			
FTKOF(K)	6-55	(5X, 10F5.0)	NACT entries of time (hours) in take-off mode for aircraft type K.
10 (1 card)			
NGIN(K)	6-55	(5X,10I5)	NACT entries for the number of engines with which aircraft type K is equipped.
11 (1 card)			
INGN(K)	6-55	(5X,10I5)	NACT entries for the engine type with which aircraft type K is equipped.
12 (NENT x 4 cards)			
EMI (I,J,K)	16-55	(15X, 5F10.0)	For each of the above engine types, enter an emission rate (lbs/hr) for each pollutant K (specified on card type 2). Cards 1 thru 4 for each engine type throttle setting will correspond to taxi, idle, landing and take-off modes, respectively.
13 (1 card)			
DSRW	16-25	F10.0	Width (mi) of initial dispersion on runway.
HRW	26-35	F10.0	Height (mi) of initial dispersion on runway.

Table 3.1. Card Input Sequence (contd.)

Card Type	Columns	Format	Comment
14 (1 card)*			
X1	16-25	F10.0	X coordinate of runway (mi) (Aircraft touch-down end)
Y1	26-35	F10.0	Y coordinate of runway (mi) (Aircraft touch-down end)
Z1	36-45	F10.0	Z height (ft) of runway. (Aircraft touch-down end)
X2	46-55	F10.0	X2 coordinate of opposite end point (mi)
Y2	56-65	F10.0	Y2 coordinate of opposite end point (mi)
Z2	66-75	F10.0	Z2 height of opposite end point (ft)
15 (1 card)			
VA1	16-25	F10.0	Initial velocity of arriving aircraft (mi/hr)
VA2	26-35	F10.0	Final velocity of arriving aircraft (mi/hr)
VD1	36-45	F10.0	Initial velocity of departing aircraft (mi/hr)
VD2	46-55	F10.0	Final velocity of departing aircraft (mi/hr)
TIME	56-65	F10.0	Aircraft take-off roll-time (hrs)
TAIL	66-75	F10.0	Exhaust tail length (mi)
16 (1 card)			
FTAXI(K)	6-55	(5X, 10F5.0)	NACT entries of aircraft taxi speed (mi/hr) while in the gate area for each aircraft type K.
17 (1 card)			
FTXII(K)	6-55	(5X, 10F5.0)	NACT entries of aircraft inbound taxi speed (mi/hr)
18 (1 card)			
FTXIO(K)	6-55	(5X, 10F5.0)	NACT entries of aircraft outbound taxi speed (mi/hr)
19 (1 card)			
DSTW	16-25	F10.1	Width (mi) of initial dispersion on taxiway.
HTW	26-35	F10.1	Height (mi) of initial dispersion on taxiway.
20 (1 card)*			
X1	16-25	F10.0	X coordinate of inbound taxiway (mi)
Y1	26-35		Y coordinate of inbound taxiway (mi)
Z1	36-45		Z height of inbound taxiway (ft)
X2	46-55		X2 coordinate of inbound taxiway (mi) (Airport terminal end)
Y2	56-65		Y2 coordinate of inbound taxiway (mi) (Airport terminal end)
Z2	66-75		Z2 height of inbound taxiway (ft) (Airport terminal end)

Table 3.1. Card Input Sequence, (contd.)

Card Type	Columns	Format	Comment
21 (1 card)*			
X1	16-25	F10.0	X coordinate of outbound taxiway (mi)
Y1	26-35	F10.0	Y coordinate of outbound taxiway (mi)
Z1	36-45	F10.0	Z height of outbound taxiway (ft)
X2	46-55	F10.0	X2 coordinate of outbound taxiway (mi) (apron end)
Y2	56-65	F10.0	Y2 coordinate of outbound taxiway (mi) (apron end)
Z2	66-75	F10.0	Z2 height of outbound taxiway (ft) (apron end)
22 (1 card)			
DSRA	16-25	F10.0	Width (mi) of initial dispersion on apron.
HRA	26-35	F10.0	Height (mi) of initial dispersion on apron.
23 (1 card)*			
X1	16-25	F10.0	X coordinate of inbound apron (mi)
Y1	26-35	F10.0	Y coordinate of inbound apron (mi)
Z1	36-45	F10.0	Z height of inbound apron (ft)
X2	46-55	F10.0	X2 coordinate of inbound apron (mi) (from here we start the inbound taxiway)
Y2			Y2 coordinate of inbound apron (mi) (from here we start the inbound taxiway)
Z2			Z2 height of inbound taxiway (ft)
24 (1 card)*			
X1	16-25	F10.0	X coordinate of outbound apron (mi)
Y1	26-35	F10.0	Y coordinate of outbound apron (mi)
Z1	36-45	F10.0	Z height of outbound apron (ft)
X2	46-55	F10.0	X2 coordinate of outbound apron (mi)
Y2	56-65	F10.0	Y2 coordinate of outbound apron (mi)
Z2	66-75	F10.0	Z2 height of outbound apron (ft)
25 (1 card)	Omit if NAVR = 0.		
EFUH(J)	16-65	(15X, 5F10.0)	For each of the pollutants specified on card type 2, enter the urban automobile emission factor (gm/km) based on 25 mi/hr traffic speed.
26 (1 card)	Omit if NAVR = 0.		
EFUL(J)	16-65	(15X, 5F10.0)	For each of the pollutants specified on card type 2, enter the urban automobile emission factor (gm/km) based on 10 mi/hr traffic speed.
27 (1 card)	Omit if NAVR = 0.		
DSAR	16-25	F10.0	Width (mi) of initial dispersion on access roadways.
HAR	26-35	F10.0	Height (mi) of initial dispersion on access roadways.

Also, with stack downwash the initial plume dimensions are reassigned in the AVAP Model to simulate average city block size and building height ($\sigma_{y0} = 250$ ft; $\sigma_{z0} = 40$ ft).

Table 3.1. Card Input Sequence (contd.)

Card Type	Columns	Format	Comment
28 (NAVR cards)*			Access vehicle roadways:
X1	11-20	F10.0	X coordinate of first end point (mi)
Y1	21-30	F10.0	Y coordinate of first end point (mi)
Z1	31-40	F10.0	Z coordinate of first end point (ft)
X2	41-50	F10.0	X coordinate of second end point (mi)
Y2	51-60	F10.0	Y coordinate of second end point (mi)
Z2	61-70	F10.0	Z coordinate of second end point (ft)
VNOON	71-78	F8.0	Average traffic volume
IFS	79-80	I2	Roadway classification: 1=congested, 0=non-congested
29 (1 card)*	Omit if NACA = 0.		
XS	16-25	F10.0	X coordinate of terminal area center (mi)
YS	26-35	F10.0	Y coordinate of terminal area center (mi)
STKH	36-45	F10.0	Height of terminal (ft)
WIT	46-55	F10.0	Side length of terminal (mi)
30 (1 card)	Omit if NACA = 0.		Pollutant emission rate of diesel engine powered service vehicles.
EFD(1)	16-25	F10.0	CO (gm/gal)
EFD(2)	26-35	F10.0	HC (gm/gal)
EFD(3)	36-45	F10.0	NOx (gm/gal)
EFD(4)	46-55	F10.0	PART (gm/gal)
EFD(5)	56-65	F10.0	SOx (gm/gal)
31 (1 card)	Omit if NACA = 0.		Pollutant emission rate of gasoline engine powered service vehicles.
EFG(1)	16-25	F10.0	CO (gm/mi)
EFG(2)	26-35	F10.0	HC (gm/mi)
EFG(3)	36-45	F10.0	NOx (gm/mi)
EFG(4)	46-55	F10.0	PART (gm/mi)
EFG(5)	56-65	F10.0	SOx (gm/mi)
32 (14 cards)	Omit if NACA = 0.		
SRVTIM(1,K)	6-55		NACT entries of service vehicle operation time (min) during the aircraft service operation in the terminal area. See Page 31 for a list of 14 modeled service vehicles.
33 (1 card)	Omit if NACA = 0.		
KAPU(K)	6-55	(5X, 10I5)	NACT entries denoting 1=the use of an auxiliary power unit: 0=no auxiliary power unit used for aircraft type K.
34 (1 card)	Omit if NACA = 0.		
APU(J)	16-65	(15X, 5F10.0)	For each of the pollutants specified on card type 2, enter the emission factors (lb/hr) for auxiliary power units.

expected to give more realistic concentration profiles than the conventional area source model.

Table 3.1. Card Input Sequence (contd.)

Card Type	Columns	Format	Comment
35 (1 card) FIDLE(K)	Omit if NACA = 0. 6-55	(5X, 10F5.0)	NACT entries of time (hr) for aircraft K engine idle.
36 (1 card) TGND(K)	Omit if NACA = 0. 6-55	(5X, 10F5.0)	NACT entries of time (min) for aircraft K gate occupancy.
37 (1 card)* XS	Omit if NANA = 0. 16-25	F10.0	X coordinate of non-aircraft area source center (mi)
YS	26-35	F10.0	Y coordinate of non-aircraft area source center (mi)
STKH	36-45	F10.0	Height of non-aircraft area source (ft)
WIT	46-55	F10.0	Side length of non-aircraft area source (mi)
38 (1 card)* EMIT(J)	Omit if NANA = 0. 16-65	(15X, 5F10.0)	For each of the pollutants specified on card type 2, enter the non-aircraft area source emission rate (lbs/hr)

* Default values for these data are not available.

+ See Table 4.1. Program Default Values by Card Input Sequence Number.

4 DESCRIPTION OF DEFAULT DATA

This section describes for the user what is required as input data should the option to over-ride program constants be exercised. Also, it lists the values of program constants (Table 4.1) as they appear in the BLOCK DATA subprogram of the computer code. All or some of the values will change whenever the appropriate card is inserted into the input stream.

The computer program is designed to model activity of ten (10) different aircraft types. These are listed in the first column of Table 4.1 (page 27) and may be replaced with types having identical, or nearly identical operational parameters, engine configurations, and ground service requirements.

Operational parameters include time period values during which the aircraft-engine throttle setting is adjusted to one of the following operational modes:

- 1 Landing - Aircraft touch-down to beginning of taxi on the inbound apron.
- 2 Take-off - After alignment of aircraft with runway to liftoff.
- 3 Idle - Arriving aircraft awaiting gate position.

These operating times are shown in Table 4.1, page 27, columns 3 and 4, and page 29, column 6, respectively. Other operational parameters presented on page 29, columns 2, 3 and 4 consider the speed of aircraft while they are in the gate area, on the inbound taxiway and on the outbound taxiway, respectively. Those that detail the average performance characteristics of all aircraft types during flight modes of operation are shown on page 30 (Card 15).

Engine configuration and their emission characteristics are assigned integer values to denote for each aircraft type, and each engine type the number of engines per aircraft and their pollutant emission rates during 4 modes of operation (Taxi, Idle, Landing and Take-off). These values are shown in Table 4.1, page 27, columns 5 and 6 respectively, with corresponding pollutant emission rate shown on page 28.

The ground service requirements of each aircraft type are fulfilled using fourteen (14) different pieces of motorized equipment (page 31, Card 32), all of which operate within the gate area to load and unload cargo and otherwise prepare the airplane for its next departure. It can be seen by the service times entered into the table that the equipment in use is

dependent upon the type of aircraft being serviced. The pollutant emission rates (page 30, Cards 30, 31) are presented for both diesel and gasoline engine powered equipment. Note that an auxiliary power unit will provide electrical power, whenever used (Page 29, Column 5), for the entire gate time (Page 29, Column 7) of the aircraft. Its emissions rates are shown on Page 31, Card 34.

Table 4.1. Program Default Values by Card Input Sequence

Aircraft Type	Card 7 Hourly Arrivals	Card 8 Time (hr) Landing	Card 9 Time (hr) Take-off	Card 10 Number of Engines	Card 11 Engine Type
1 (Boeing 727)	10	0.0153	0.0111	3	1 (JT8D)
2 (Douglas DC9)	10	0.0153	0.0111	2	1 (JT8D)
3 (Boeing 737)	10	0.0153	0.0111	2	1 (JT8D)
4 (Convair 580)	10	0.0153	0.0111	2	3 (A-501-D13)
5 (BAC 111)	10	0.0153	0.0111	2	4 (SPEY-511)
6 (NAMC YS11)	10	0.0153	0.0111	2	3 (A-501-D13)
7 (Beech 99)	10	0.0110	0.0111	2	2 (TPE 331)
8 (Fairchild FH-227)	10	0.0153	0.0111	2	3 (A-501-D13)
9 (Twin Otter)	10	0.0110	0.0111	2	2 (TPE 331)
10 (Piston Engine)	10	0.0110	0.0111	2	5 (320)

Table 4.1. Program Default Values by Card Input Sequence (Contd)
 Card 12 Pollutant Emission Rate for Each Engine
 Type During 4 Modes of Operation (lbs/hr)

	CO	HC	NO _x	PART	SO ₂
Engine Type 1 (JT8D)					
Taxi	37.0	9.0	2.0	0.5	0.9
Idle	37.0	9.0	2.0	0.5	0.9
Landing	25.6	5.6	36.3	6.8	3.2
Take-off	6.0	0.4	133.3	21.0	8.6
Engine Type 2 (TPE 331)					
Taxi	3.53	0.88	0.96	0.10	0.5
Idle	3.53	0.88	0.96	0.10	0.5
Landing	2.58	0.24	1.69	0.38	0.9
Take-off	0.39	0.05	3.64	0.62	1.9
Engine Type 3 (All. 501-D13)					
Taxi	15.0	6.0	2.0	0.10	0.5
Idle	15.0	6.0	2.0	0.10	0.5
Landing	10.1	3.8	8.0	0.30	0.9
Take-off	2.0	0.4	23.0	0.60	1.9
Engine Type 4 (Spey 511)					
Taxi	60.0	66.0	1.0	0.04	0.6
Idle	60.0	66.0	1.0	0.04	0.6
Landing	45.6	40.3	42.1	0.30	2.2
Take-off	14.0	0.0	153.0	0.80	6.2
Engine Type 5 (Ø-320)					
Taxi	11.41	0.38	0.01	0.06	0.01
Idle	11.41	0.38	0.01	0.06	0.01
Landing	11.41	0.38	0.01	0.06	0.01
Take-off	72.52	1.66	0.23	0.12	0.07

Table 4.1 (Cont'd)

<u>Card 13</u>	Initial dimensions of dispersion on runway. Width = DSRW = 0.030 miles Height = HRW = 0.002 miles
<u>Card 15</u>	Runway parameters for arrival and departure aircraft. VA1 = Runway - arrival initial velocity = 145 (mi/hr) VA2 = Runway - arrival final velocity = 25 (mi/hr) VD1 = Runway - departure initial velocity = 0.0 (mi/hr) VD2 = Runway - departure final velocity = 180 (mi/hr) TIME = Take-off roll time = .0111 (hrs) TAIL = Exhaust tail length = .8523 (mi)
<u>Card 19</u>	Initial dimensions of dispersion on taxiway. Width = DSTW = 0.030 (mi) Height = HTW = 0.002 (mi)
<u>Card 22</u>	Initial dimensions of dispersion on runway apron. Width = DSRA = 0.095 (mi) Height = HRA = 0.002 (mi)
<u>Card 25</u>	Urban automobile pollutant emission factors (gm/km) based on 25 (mi/hr) traffic speed. CO = 32.36, HC = 4.75, NO _x = 3.46, PART = 0.19, SO _x = 0.11
<u>Card 26</u>	Urban automobile pollutant emission factors (gm/km) based on 10 (mi/hr) traffic speed. CO = 70.18, HC = 8.62, NO _x = 2.86, PART = 0.19, SO _x = 0.11
<u>Card 27</u>	Initial dimensions of dispersion on access roadway. Width = DSAR = 0.0095 (mi) Height = HAR = 0.001 (mi)
<u>Card 30</u>	Pollutant emission factor for diesel engine powered service vehicles in (gm/gal). CO = 126.6, HC = 21.9, NO _x = 185.82, PART = 5.9, SO _x = 0.0
<u>Card 31</u>	Pollutant emission factor for gasoline engine powered service vehicles in (gm/mi). CO = 138.81, HC = 21.35, NO _x = 9.32, PART = 0.85, SO _x = 0.0

Table 4.1 (Cont'd)

Aircraft Type	Card 16	Card 17	Card 18	Card 33	Card 35	Card 36
	Speed (mi/hr) Gate area taxi	Speed (mi/hr) Inbound taxi	Speed (mi/hr) Outbound taxi	APU use flags	Time (hr) Engine idle	Time (min) Gate occupancy
1 (Boeing 727)	10	15	12	1	.033	52.
2 (Douglas DC9)	10	15	12	1	.033	52.
3 (Boeing 737)	10	15	12	1	.033	52.
4 (Convair 580)	10	15	12	1	.033	52.
5 (BAC 111)	10	15	12	0	.033	52.
6 (NAMCO YS 11)	10	15	12	0	.033	52.
7 (Beech 99)	10	15	12	0	.033	52.
8 (Fairchild FH 227)	10	15	12	0	.033	52.
9 (Twin Otter)	10	15	12	0	.033	52.
10 (Piston Engine)	10	15	12	0	.033	52.

Table 4.1 (Cont'd)

Card 34 Pollutant emission factors for auxiliary power units in (lbs/hr).
 CO = 2.82, HC = 0.11, NO_x = 1.24, PART = 0.0, SO_x = 0.0

Card 32. Minutes of Service Vehicle Operation While Servicing
 Aircraft Type I

Vehicle Type	Aircraft Type									
	1* 727	2* DC9	3* 737	4* C5	5 BAC	6 YS	7 B9	8 FH	9 TO	10 GA
1 Tractor	66	48	85	55	50	50	0	0	0	0
2 Belt Loader	28	15	30	0	25	25	0	0	0	0
3 Container Loader	6	0	0	0	0	0	0	0	0	0
4 Cabin Service	12	0	15	0	0	0	0	0	0	0
5 Lavatory Truck	15	15	15	10	10	10	5	5	5	0
6 Water Truck	0	10	0	10	10	10	5	5	5	0
7 Food Truck	17	17	20	10	10	10	0	0	0	0
8 Fuel Truck	20	15	15	10	20	20	10	10	10	0
9 Tow Tractor	10	5	5	5	5	5	0	0	0	0
10 Conditioner	0	0	0	0	0	0	0	0	0	0
11 Airstart Transporting and Diesel Engines	0	0	0	0	0	0	0	0	0	0
12 Ground Power Transporting and Gasoline Engines	0	0	0	0	0	0	0	0	0	0
13 Ground Power Unit Diesel Engine	0	0	0	0	0	0	0	0	0	0
14 Transporter	3	0	0	0	0	0	0	0	0	0

* Also serviced by an Auxiliary Power Unit (APU)

5 EXAMPLE PROBLEM

5.1 INTRODUCTION

In order to clarify the procedure for using the AVAP Model Abbreviated Version, a "first-guess" estimate of pollutant concentration is presented for the example airport-layout shown in Figure 5.1. It is instructive to state that the locations of line type sources (runway, taxiway, apron, access roadway) are specified by the coordinates at their edge (from end to end), but the locations of airport terminal and non-aircraft area sources are specified by the coordinates at their center. Since aircraft movement on the runway is almost always into the wind (given as 180 degrees) the pattern of runway-apron-taxiway usage emerges. The pattern, for the airport-layout shown, is clockwise starting from the northern most point of the runway (landing aircraft touch-down). The input coordinates must be ordered to preserve this pattern. Therefore, all aircraft prepared for departure are queued before take-off on Apron 2 (outbound).

In this example, of the ten different aircraft types for which the Abbreviated Version is internally coded, seven are considered. They are listed with their associated engine type as follows:

(Boeing 727 & 737, Douglas DC9) JT8D turbofan engine
(Beech 99) TPE 331 turboprop engine
(Convair 580, NAMC YS11) All. 501-D13 turboprop engine
(Small Piston Engine aircraft) Ø320 small piston engine

5.2 STATEMENT OF THE PROBLEM

GIVEN: Two pollutant species: Carbon Monoxide and Oxides of Nitrogen

Height of aerovane	10 ft
Wind speed	13 knots
Wind direction	180 degrees
Ambient temperature	36 degrees F
Stability index	4
Lid height	0 (Uses coded table from Holzworth)

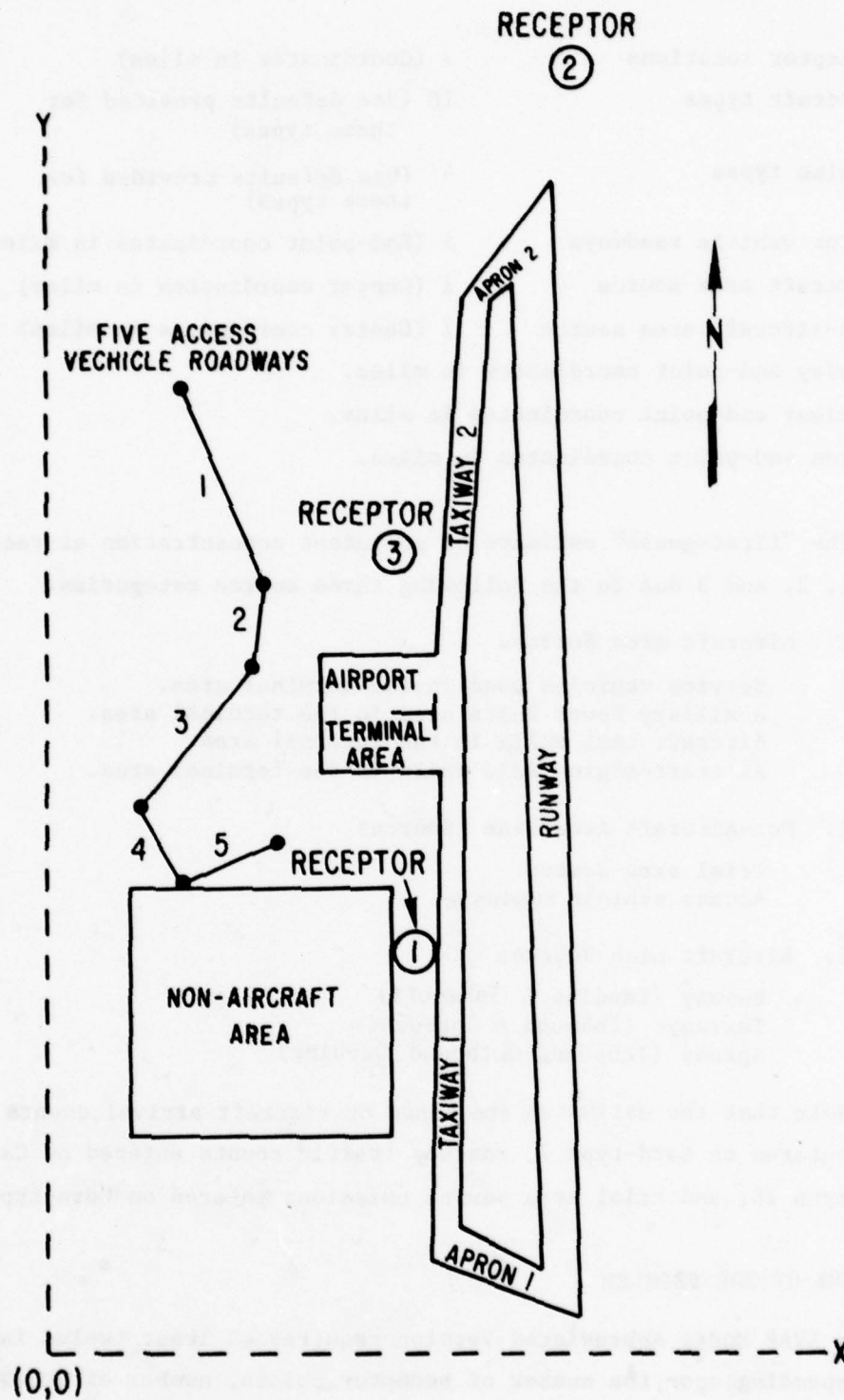


Figure 5.1 Example Airport-Layout

Receptor locations	3 (Coordinates in miles)
Aircraft types	10 (Use defaults provided for these types)
Engine types	4 (Use defaults provided for these types)
Motor vehicle roadways	5 (End-point coordinates in miles)
Aircraft area source	1 (Center coordinates in miles)
Non-aircraft area source	1 (Center coordinates in miles)
Runway end-point coordinates in miles.	
Taxiway end-point coordinates in miles.	
Apron end-point coordinates in miles.	

FIND: The "first-guess" estimate of pollutant concentration at receptors 1, 2, and 3 due to the following three source categories:

1. Aircraft Area Sources

Service vehicles used in the terminal area.
 Auxiliary Power Units used in the terminal area.
 Aircraft taxi while in the terminal area.
 Aircraft-engine idle while in the terminal area.

2. Non-Aircraft Area-Line Sources

Trial area source
 Access vehicle roadways

3. Aircraft Line Sources

Runway (Landing & Take-off)
 Taxiways (Inbound & Outbound)
 Aprons (Inbound, Outbound Queuing)

Note that the estimates are based on aircraft arrival counts entered on Card-type 7, roadway traffic counts entered on Card-type 28, and trial area source emissions entered on Card-type 38.

5.3 SUMMARY OF THE PROBLEM

The AVAP Model Abbreviated Version requires at least twelve input cards. Depending upon the number of receptor points, number of access vehicle roadways and choice of default values, there may be more. The format for each card is given in Table 3.1. Table 5.1 lists the input for the sample problem; Table 5.2 lists the results. Note that a descriptive list of program values starts the table of results. Also note

that a tabulation of pollutant emission levels for each area and line type source is provided. The micrograms-per-cubic-meter notation, as seen in the concentrations tabulation, is used for Total Suspended Particulates (PART) if it is one of the pollutants being modeled.

Table 5.1 Input for Example Problem

SPORT MODEL TEST JAN. 1977 EXAMPLE 1

CO	NOX	10.	13.	130.	36.	4	0	315	MET DATA
CONTROL CARD		3	10	4	5	1	1		
DEFAULT 1									
1	.44.	.452	6.562						
2	.590	1.51	6.562						
3	.375	.525	6.562						
A/C	7	8	2	1	0	2	1	0	11
RUNWAY COORD.			.524	1.338			10.	.616	.063
TAXIWAY COORD 1			.473	.091			10.	.376	.724
TAXIWAY COORD 2			.376	.801			10.	.438	1.240
APRON COORD 1			.616	.063			10.	.473	.091
APRON COORD 2			.524	1.338			10.	.438	1.240
ROADWAY 1		.0730	1.0653	5.			.1938	1.0675	5.
ROADWAY 2		.1938	1.0675	5.			.1781	.7353	5.
ROADWAY 3		.1781	.7353	5.			.0406	.5343	5.
ROADWAY 4		.0406	.5343	5.			.0938	.4376	5.
ROADWAY 5		.0938	.4376	5.			.281	.528	5.
A/C AREA			.395	.753			11.	.077	
NON-A/C AREA			.168	.288			16.	.3	
NON-A/C EMIS			793.8	0.0			0.0	0.0	0.0

Table 5.2 Results of Example Problem

```

SHORT MODEL TEST JAN. 1977          EXAMPLE 1
POLLUTANT CHOICE:                    CO          NOX
AIRPORT PARAMETERS:
      NUMBER OF RECEPTORS----- 3
      NUMBER OF RUNWAYS----- 1
      NUMBER OF TAXIWAYS----- 2
      NUMBER OF APRONS----- 2
      NUMBER OF TERMINAL AREAS----- 1
      NUMBER OF AIRCRAFT TYPES----- 10
      NUMBER OF AIRCRAFT ENGINE TYPES----- 4
      NUMBER OF SERVICE VEHICLE TYPES----- 14
      NUMBER OF ACCESS VEHICLE ROADWAYS----- 5
      NUMBER OF AIRPORT NON-AIRCRAFT AREA SOURCES----- 1
3 RECEPTOR COORDINATES (X,Y,Z):
      0.4440  0.4520  6.5620
      0.5960  1.5100  6.5620
      0.3750  0.9250  6.5620
140 1 2 3
ARRIVAL HEIGHT = 10.0 FT.  WIND SPEED = 14.95 MPH  WIND DIRECTION = 180. DEGREES
ADJACENT TEMPERATURE = 36.0 F DEGREES  STABILITY CLASS INDEX = 4  LID HEIGHT = 3281.0 FT.
ARRIVAL ACTIVITY FOR AIRCRAFT TYPES 1 THROUGH 10      7  6  2  1  0  2  1  0  0  11
LANDING TIME      0.015300,0.15300,0.15300,0.15300,0.15300,0.15300,0.11000,0.15300,0.11000,0.11100
TAKE-OFF TIME     0.011100,0.11100,0.11100,0.11100,0.11100,0.11100,0.11100,0.11100,0.11100,0.11100
      1 37.00      2.00
      2 37.00      2.00
      3 25.60     36.30
      4  6.00     123.30
      1  3.53      0.96
      2  3.55      0.96
      3  2.58      1.09
      4  0.39      3.64
      1 15.00      2.00
      2 15.00      2.00
      3 10.10      8.00
      4  2.00     23.00
      1 60.00      1.00
      2 60.00      1.00
      3 45.00     42.10
      4 14.00     153.00
      1 11.41      0.01
      2 11.41      0.01
      3 11.41      0.01
      4 72.52      0.23
- POINT COORDINATES OF RUNWAYS
      0.52400  1.33500  10.00000  0.61600  0.06300  10.00000
- JAWAY PARAMETERS:
      145.00000  25.00000  0.0  180.00000  0.01110  0.06523
TAKE SPEED      10.0  10.0  10.0  10.0  10.0  10.0  10.0  10.0  10.0  10.0
LANDING SPEED   15.0  15.0  15.0  15.0  15.0  15.0  15.0  15.0  15.0  15.0
CUTBACK SPEED   12.0  12.0  12.0  12.0  12.0  12.0  12.0  12.0  12.0  12.0

```

Table 5.2 Results of Example Problem (contd.)

[illegible]

Table 5.2 Results of Example Problem (contd.)

POLLUTANT EMISSION RATE (POUNDS)		
	CO	NOX
* AIRCRAFT LANDING	19.8	23.5
* AIRCRAFT TAKE-OFF	20.6	62.3
* INBOUND APRON	18.1	0.9
* OUTBOUND QUEUING	198.8	10.3
* INBOUND TAXIWAY	79.6	4.1
* OUTBOUND TAXIWAY	68.9	3.6
* SERVICE VEHICLE	265.0	8.8
* AUX. POWER UNIT	44.0	19.3
* TERM. AREA TAXI	14.4	0.7
* TERM AREA ENG. IDLE	61.5	3.2
* AIRCRAFT AREA	384.9	32.0
* NON-AIRCRAFT AREA	793.8	0.0
* ACCESS VEHICLE		
1	7.0	0.7
2	15.3	1.6
3	8.4	0.9
4	5.4	0.6
5	13.1	1.4

Table 5.2 Results of Example Problem (contd.)

```

*****
*
* POLLUTANT CONCENTRATIONS : M/CM=MICROGRAMS PER CUBIC METER
*
* RECEPTOR 1
*
* COORDINATES ( 0.444, 0.452)
*
*
* CO (PPM) NOX (PPM)
* AIRCRAFT AREA 0.0 0.0
* NON-AIRCRAFT AREA-LINES 0.171 0.0
* AIRCRAFT LINE 0.303 0.010
* TOTAL 0.475 0.010
*****

```

```

*****
*
* POLLUTANT CONCENTRATIONS : M/CM=MICROGRAMS PER CUBIC METER
*
* RECEPTOR 2
*
* COORDINATES ( 0.590, 1.510)
*
*
* CO (PPM) NOX (PPM)
* AIRCRAFT AREA 0.039 0.002
* NON-AIRCRAFT AREA-LINES 0.030 0.000
* AIRCRAFT LINE 0.075 0.043
* TOTAL 0.144 0.045
*****

```

```

*****
*
* POLLUTANT CONCENTRATIONS : M/CM=MICROGRAMS PER CUBIC METER
*
* RECEPTOR 3
*
* COORDINATES ( 0.375, 0.925)
*
*
* CO (PPM) NOX (PPM)
* AIRCRAFT AREA 1.413 0.072
* NON-AIRCRAFT AREA-LINES 0.192 0.000
* AIRCRAFT LINE 0.410 0.013
* TOTAL 2.015 0.084
*****

```


REFERENCES

1. I. T. Wang, L. A. Conley, D. M. Rote, "Airport Vicinity Air Pollution Model User Guide," Report No. FAA-RD-75-230, prepared for U.S. Dept. of Transportation, Federal Aviation Administration (1975).
2. D. B. Turner, "A diffusion Model for An Urban Area," J. Appl. Meteorological 3, No. 999-AP-26 (1967).
3. D. B. Turner, "Workbook of Atmospheric Dispersion Estimates," U.S. Dept. of Health, Education, and Welfare, U.S. Public Health Service Publication No. 999-AP-26 (1967).
4. D. H. Slade, Ed., "Meteorology and Atomic Energy," TID-24190 (1968).
5. J. E. Carson and H. Moses, "The Validity of Currently Popular Plume Rise Formulas," Proc. USAEC Meteorological Information Meeting, Held at Chalk River Nuclear Laboratories, September 11-14, 1967, AECL-2787, I-20 (1967).
6. G. A. Briggs, "Diffusion Estimation for Small Emissions," Air Resources Atmospheric Turbulence and Diffusion Laboratory, NOAA, Oak Ridge, Tennessee (1973).
7. D. M. Rote, "Airea Source Modeling," Report being prepared for the U.S. Air Force (1975).
8. D. M. Rote, I. T. Wang, L. E. Wangen, R. W. Hecht, R. R. Cirillo, and J. Pratapas, "Airport Vicinity Air Pollution Study", Report No. FAA-RD-73-113, prepared for U.S. Dept. of Transportation, Federal Aviation Administration (1973).
9. I. T. Wang and D. M. Rote, "A Finite Line Source Dispersion Model for Mobile Source Air Pollution." Journal of Air Pollution Control Association, 25, 730-733 (1975).
10. G. A. DeMarrais, "Wind-Speed Profile at Brookhaven National Laboratory", J. Meteorol., 16, 181-190 (1959).
11. G. C. Holzworth, "Estimates of Mean Maximum Mixing Depths in the Contiguous United States, "Monthly Weather Review", 92, 235-242 (1964).

APPENDIX A

CONCENTRATION CONVERSIONS

Concentration ($\mu\text{g}/\text{m}^3$) = $1.22 \times 10^4 \frac{P}{T} \cdot \text{MW} \cdot \text{concentration (ppm)}$ where

P = pressure in atmospheres,

T = absolute temperature ($^{\circ}\text{K}$)

MW = molecular weight

Example: NO_2

P = 1 atm

T = $77^{\circ}\text{F} \equiv 25^{\circ}\text{C} \equiv 273 + 25 = 298^{\circ}\text{K}$

MW = $14 + 32 = 46$

$$\begin{aligned} \text{Concentration } (\mu\text{g}/\text{m}^3) &= 1.22 \times 10^4 \times \frac{1}{298} \times 46 \times \text{concentration (ppm)} \\ &= 1883 \times \text{concentration (ppm)} \end{aligned}$$

for T = 32°F ,

$$\text{Concentration } (\mu\text{g}/\text{m}^3) = 2056 \times \text{concentration (ppm)}$$

Note that for a pollutant class like THC or NO_x , it is customary to convert from ppm to $\mu\text{g}/\text{m}^3$ by representing the class in terms of a single pollutant such as CH_4 or NO_2 . Consequently, under the same conditions as given above (T = 32°F),

THC Concentration ($\mu\text{g}/\text{m}^3$) (treated as CH_4) =

$$\frac{1.22 \times 10^4 \times 1 \times 16}{273} = 715 \times \text{THC conc. (ppm)}$$

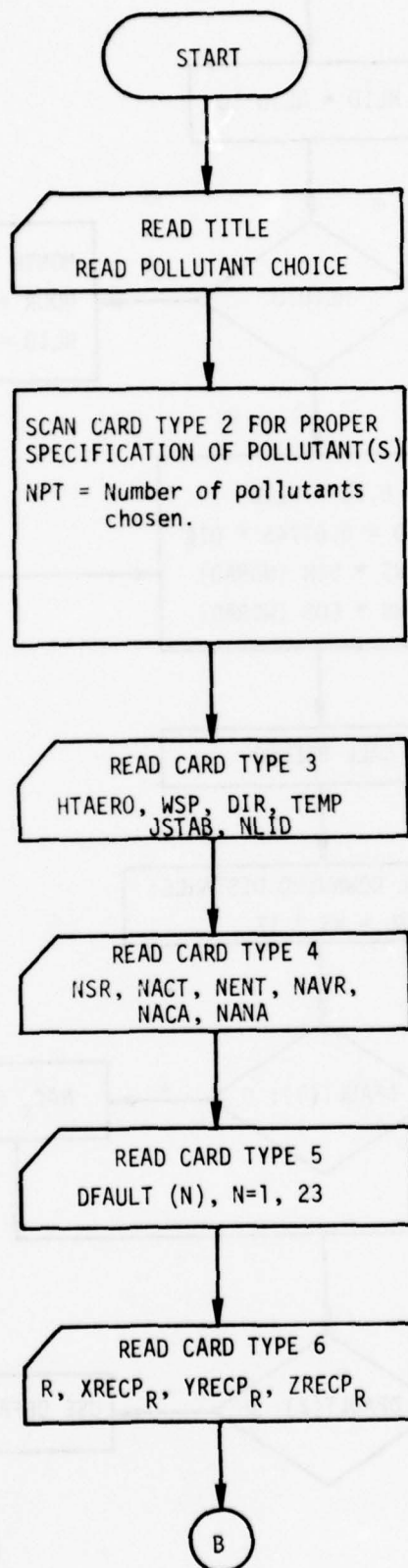
and

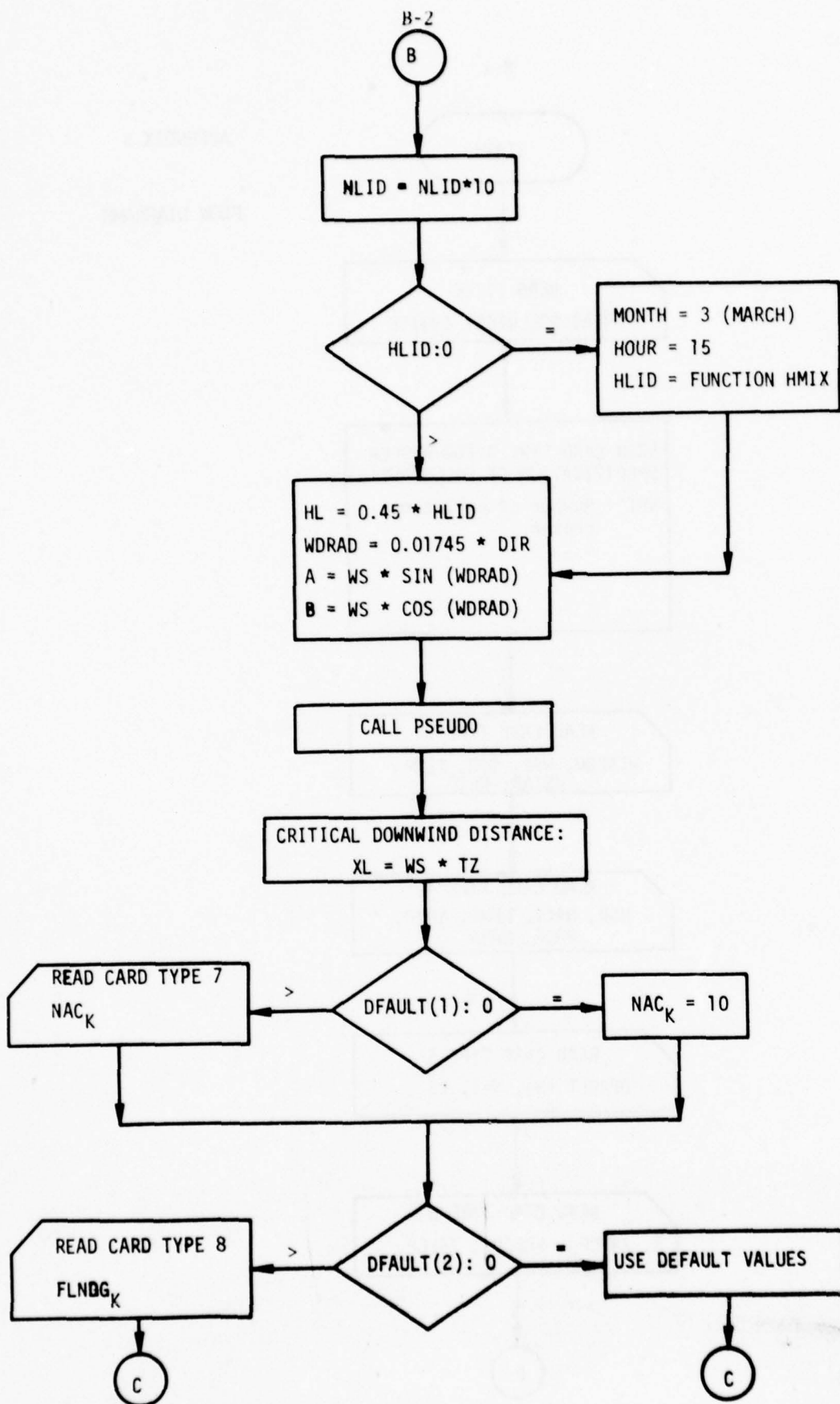
NO_x Concentration ($\mu\text{g}/\text{m}^3$) (treated as NO_2) = $2056 \times \text{NO}_x \text{ conc. (ppm)}$

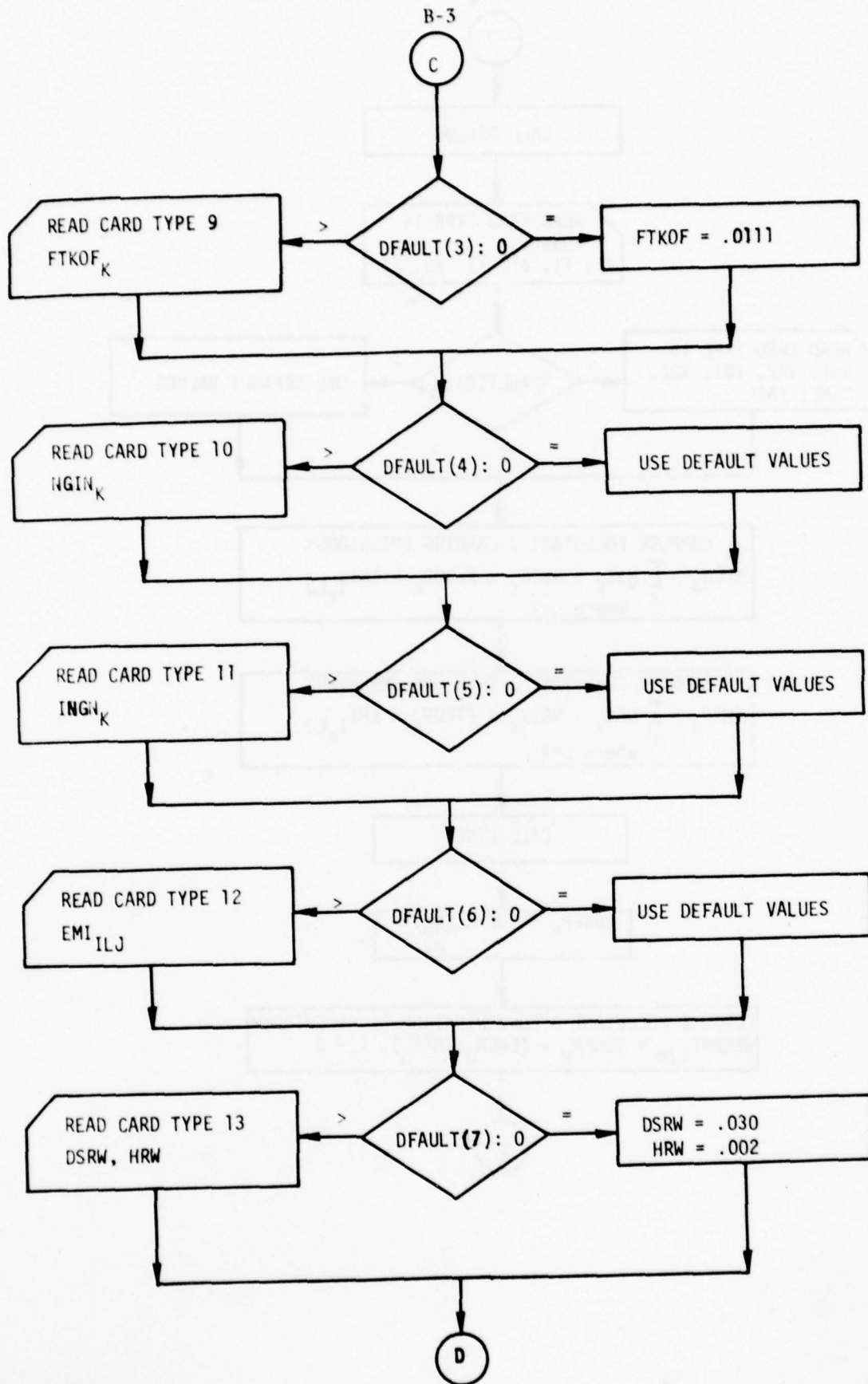
B-1

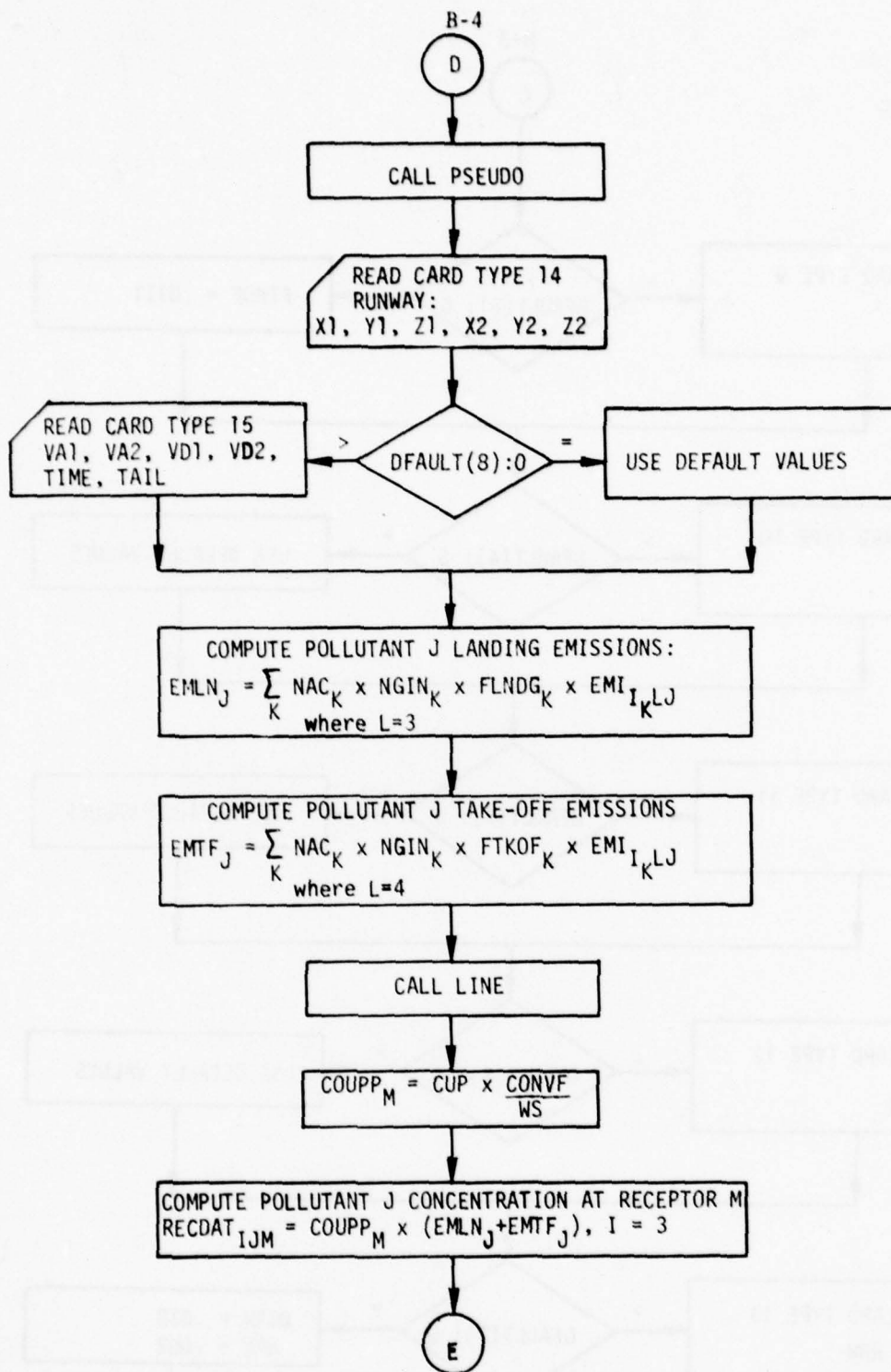
APPENDIX B

FLOW DIAGRAMS

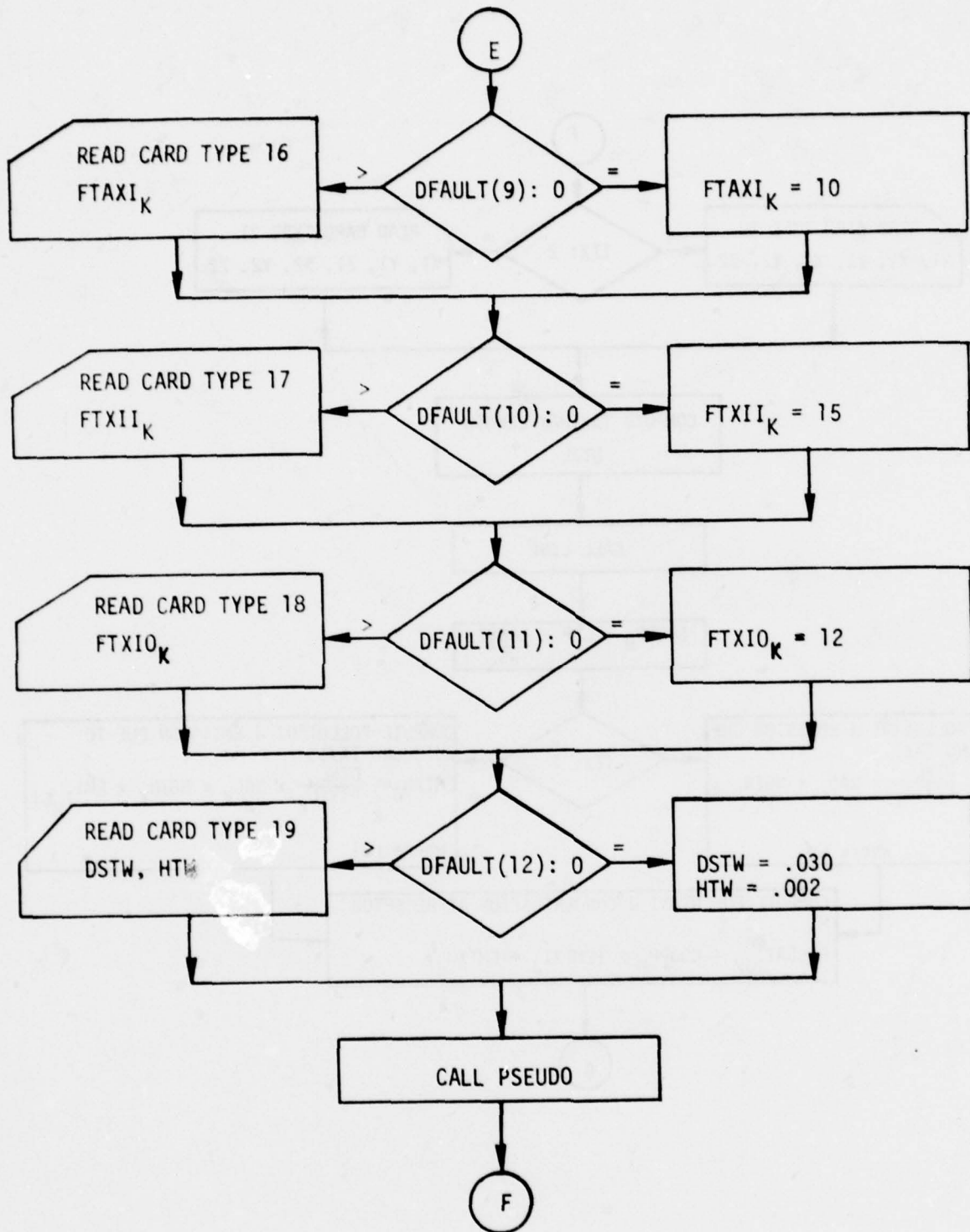


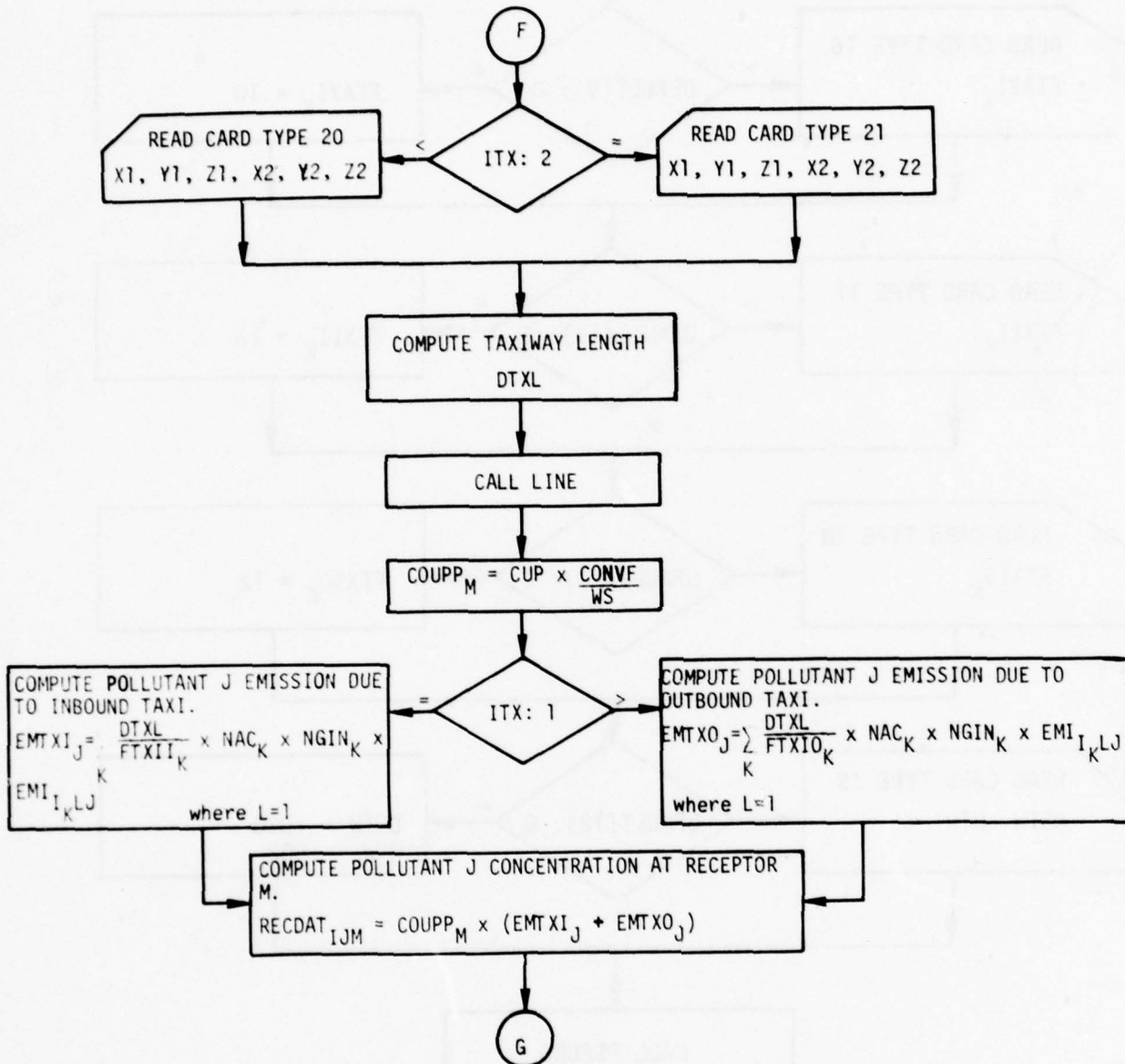


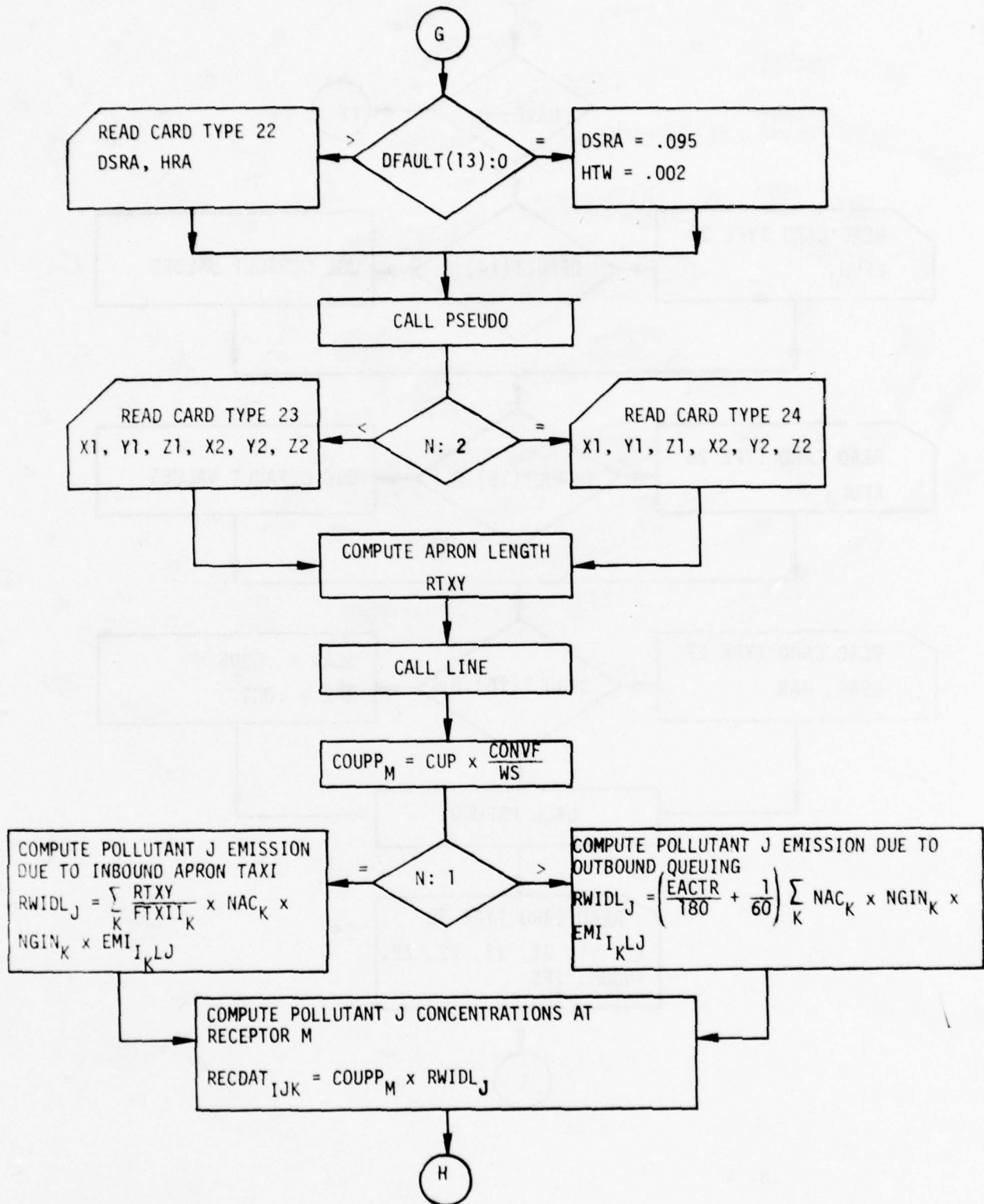


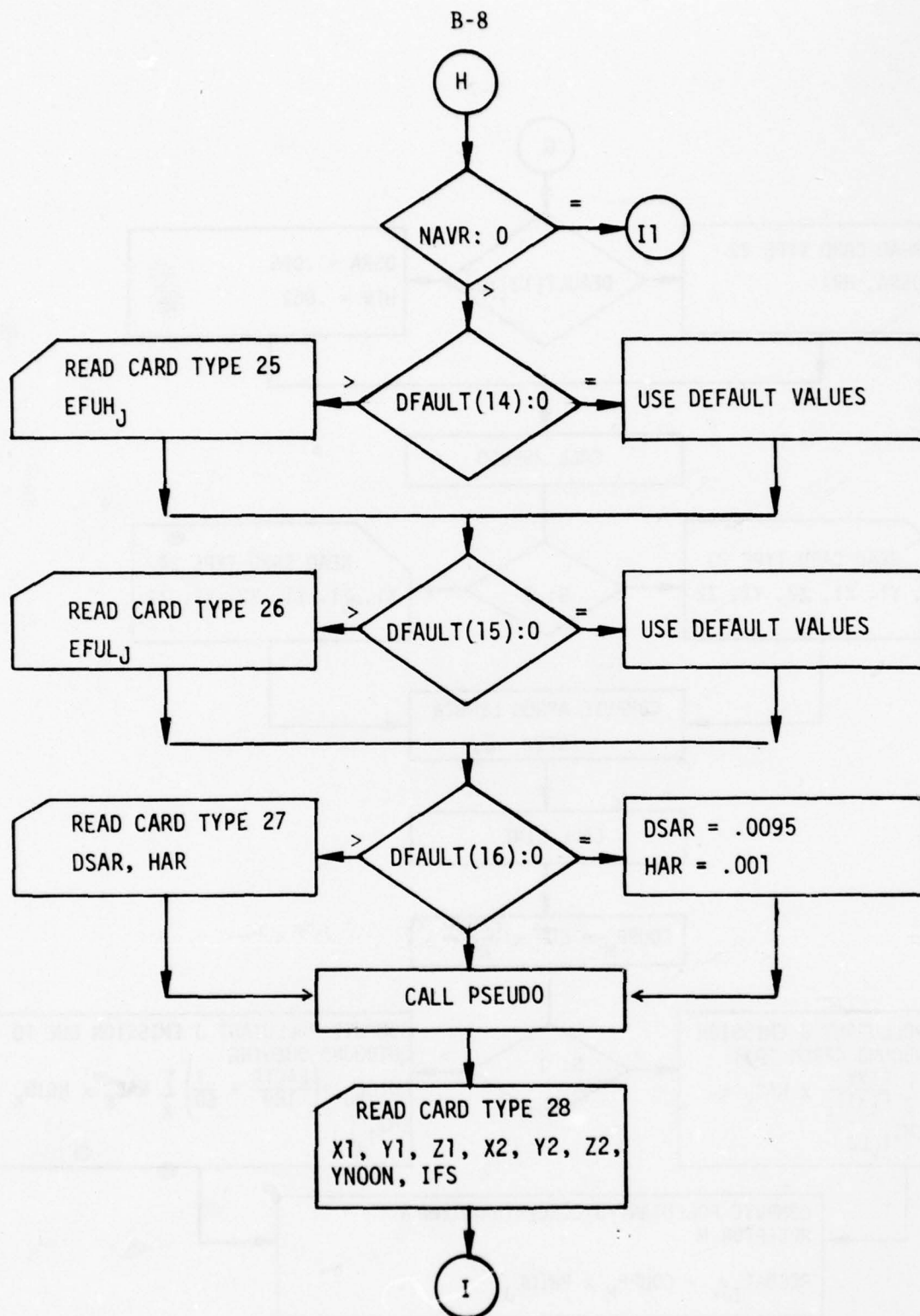


B-5

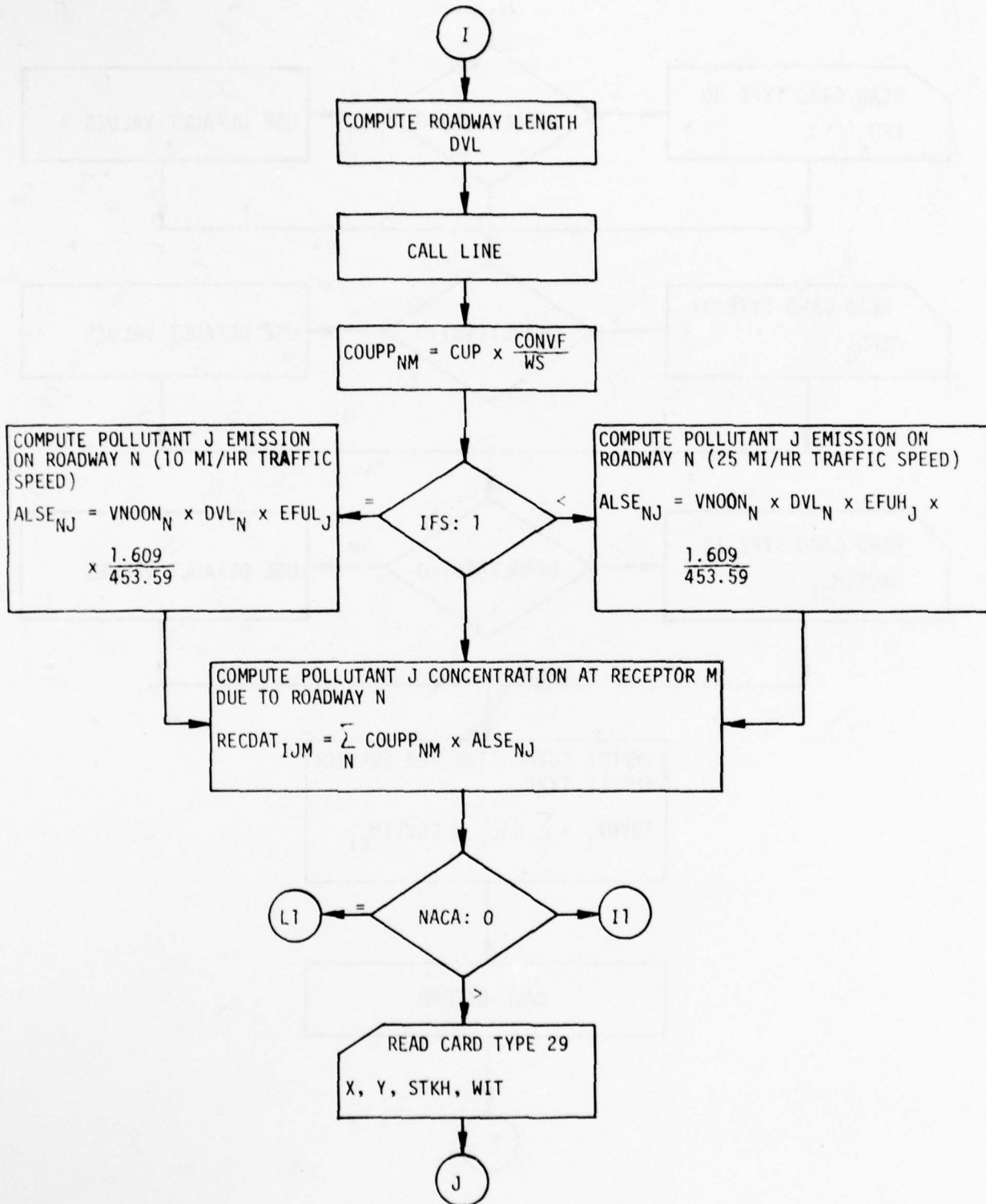






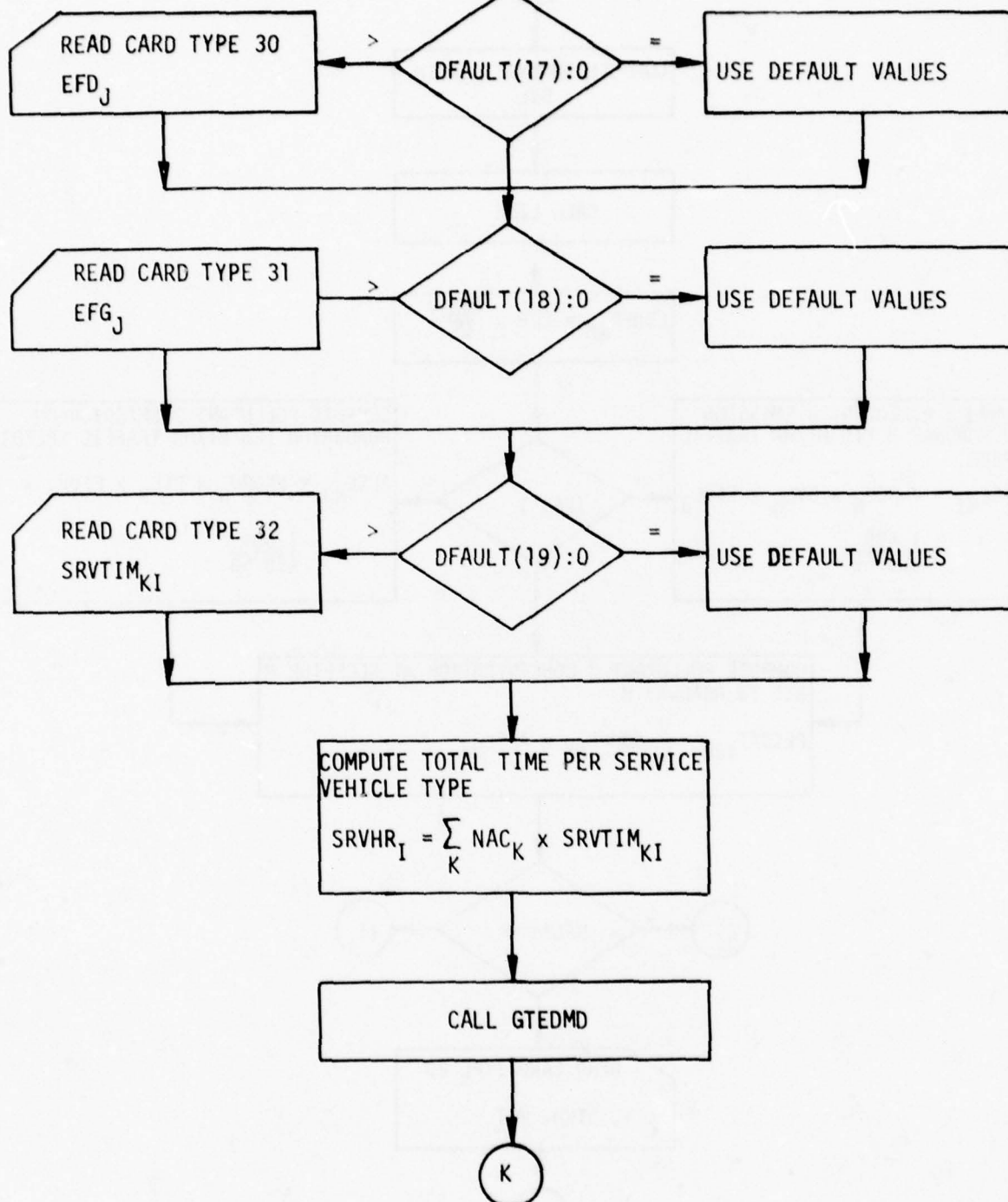


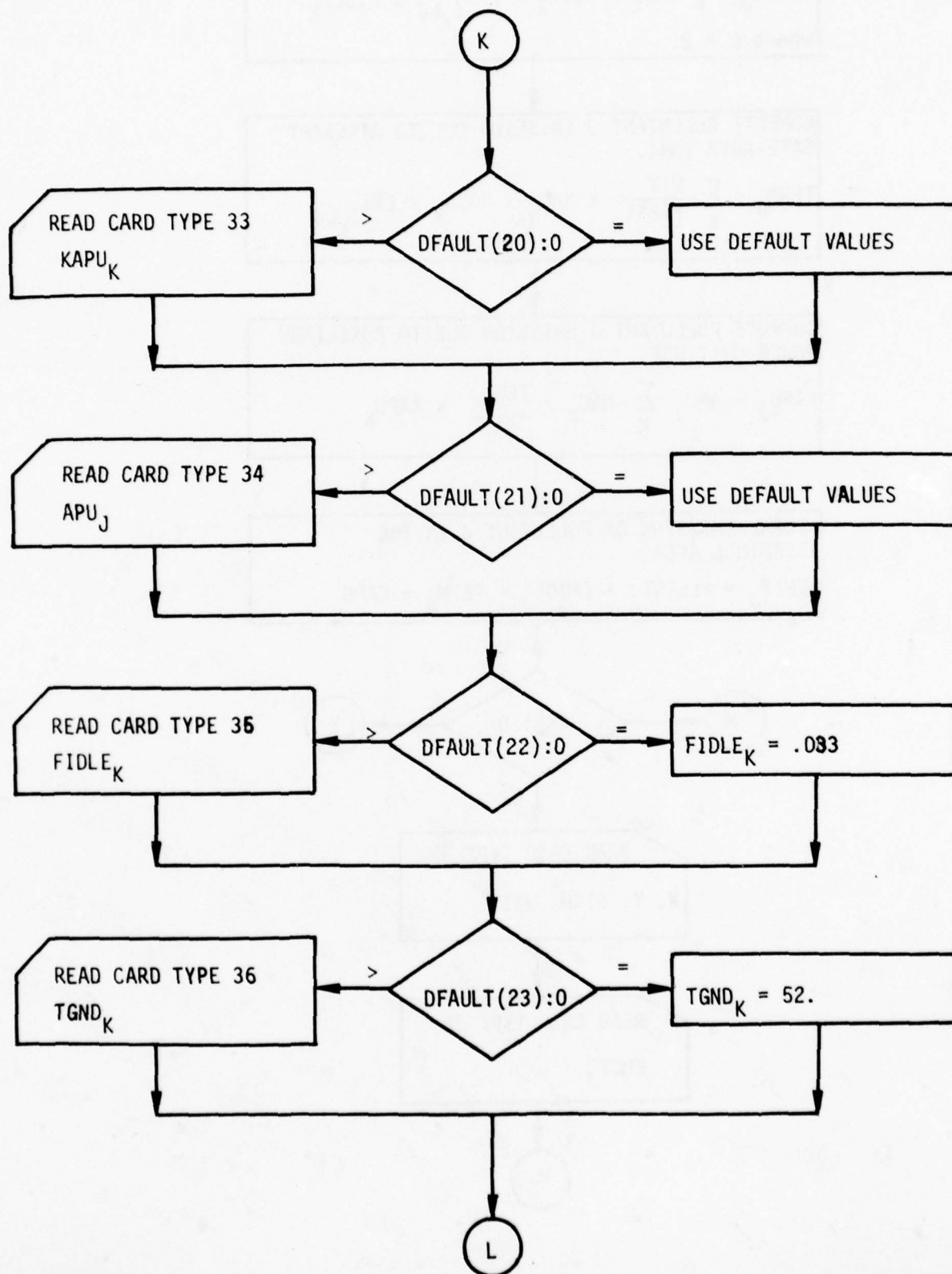
B-9



B-10

J





B-12

L

COMPUTE POLLUTANT J EMISSION DUE TO AIRCRAFT
IDLE

$$EMIDL_J = \sum_K NAC_K \times NGIN_K \times EMI_{I_K L J} \times FIDLE_K$$

where L = 2

COMPUTE POLLUTANT J EMISSION DUE TO AIRCRAFT
GATE-AREA TAXI.

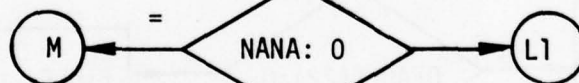
$$TERM_J = \sum_K \frac{WIT}{FTAXI_K} \times NAC_K \times NGIN_K \times EMI_{I_K L J}$$

COMPUTE POLLUTANT J EMISSION DUE TO AUXILIARY
POWER UNIT USE

$$EAPU_J = APU_J \sum_K NAC_K \times \frac{TGND_K}{60.} \times KAPU_K$$

TOTAL EMISSION OF POLLUTANT J IN THE
TERMINAL AREA

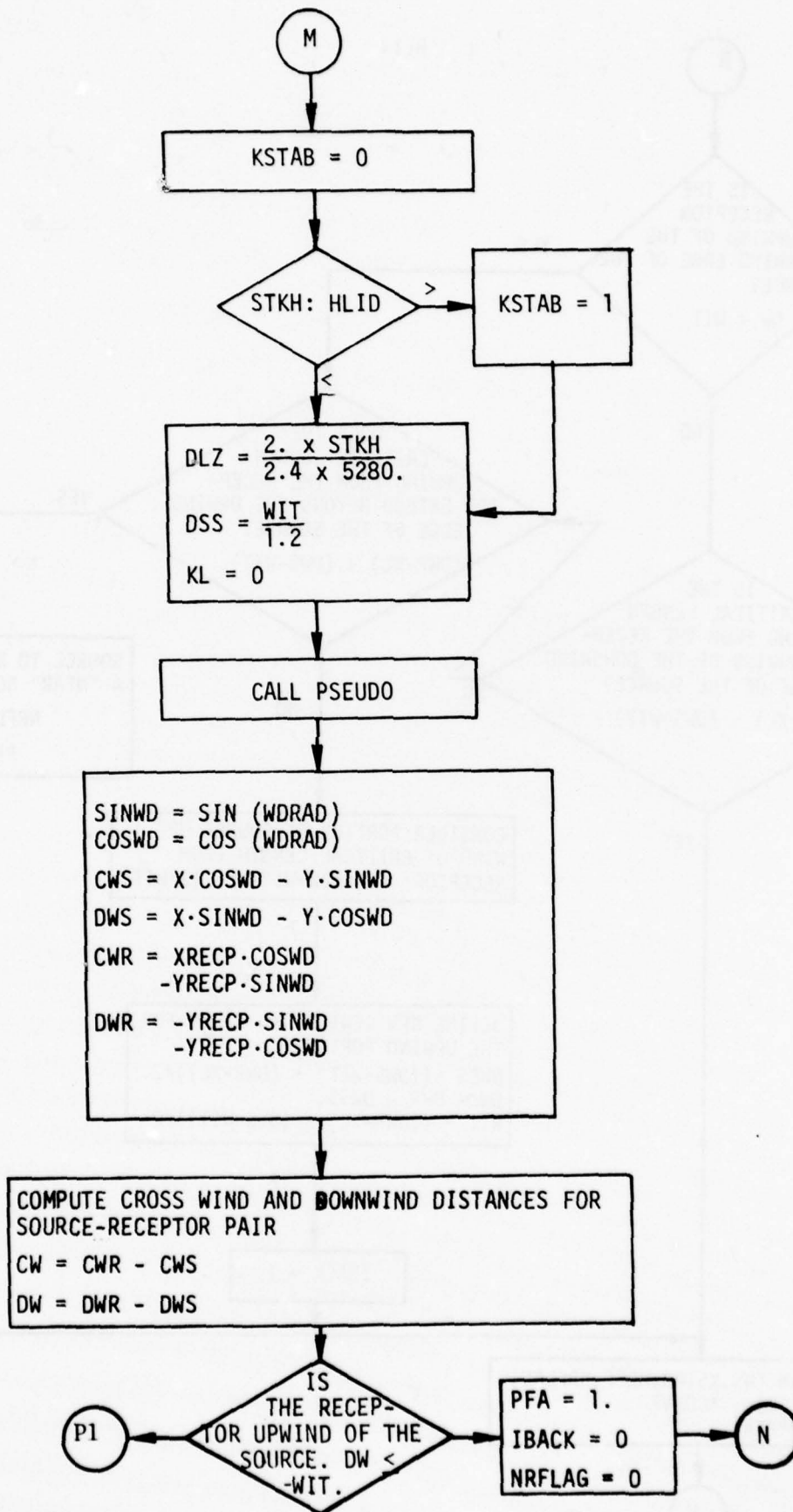
$$EMIT_J = PLLTNT_J + EMIDL_J + TERM_J + EAPU_J$$

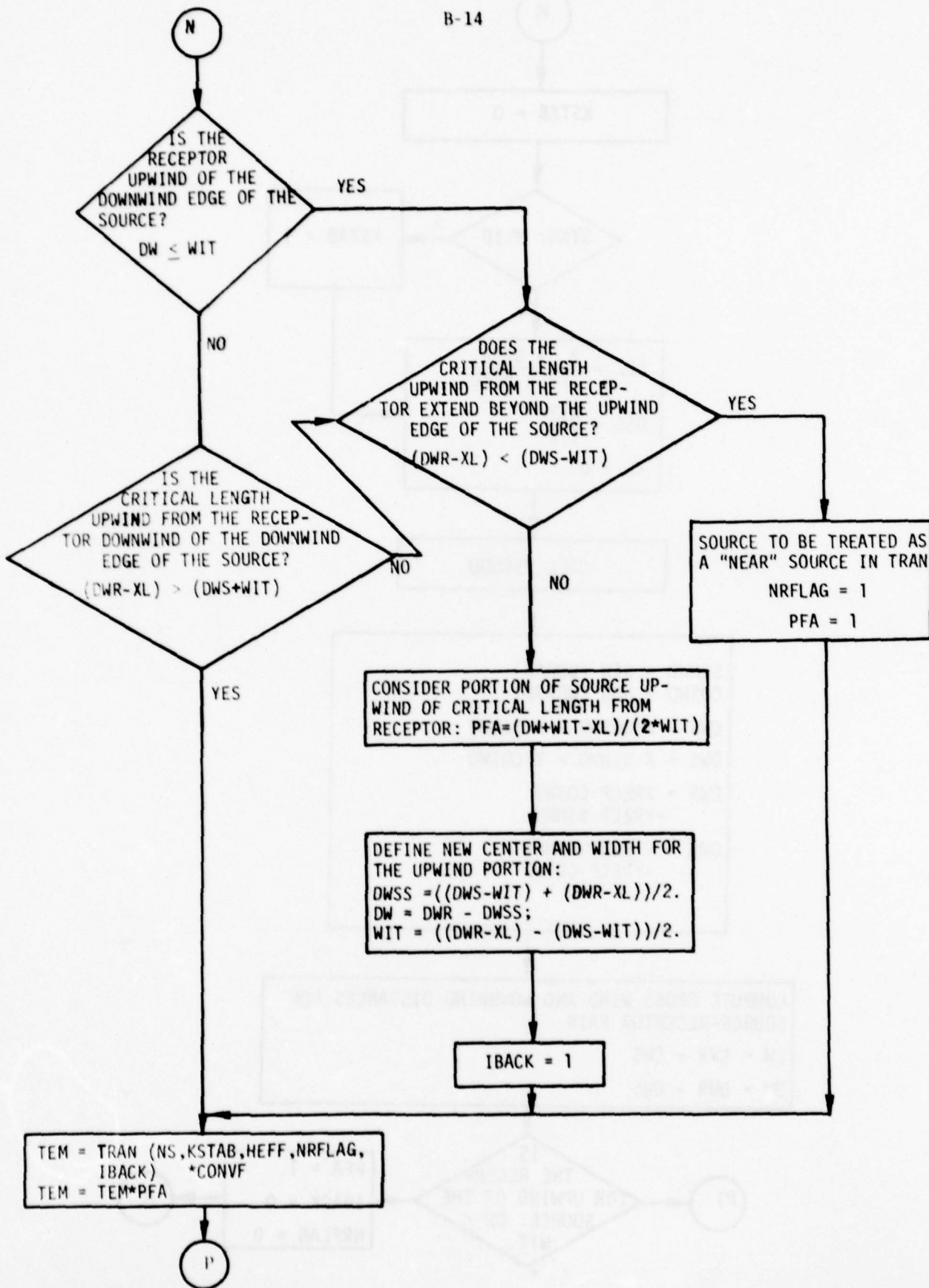


READ CARD TYPE 37
X, Y, STKH, WIT

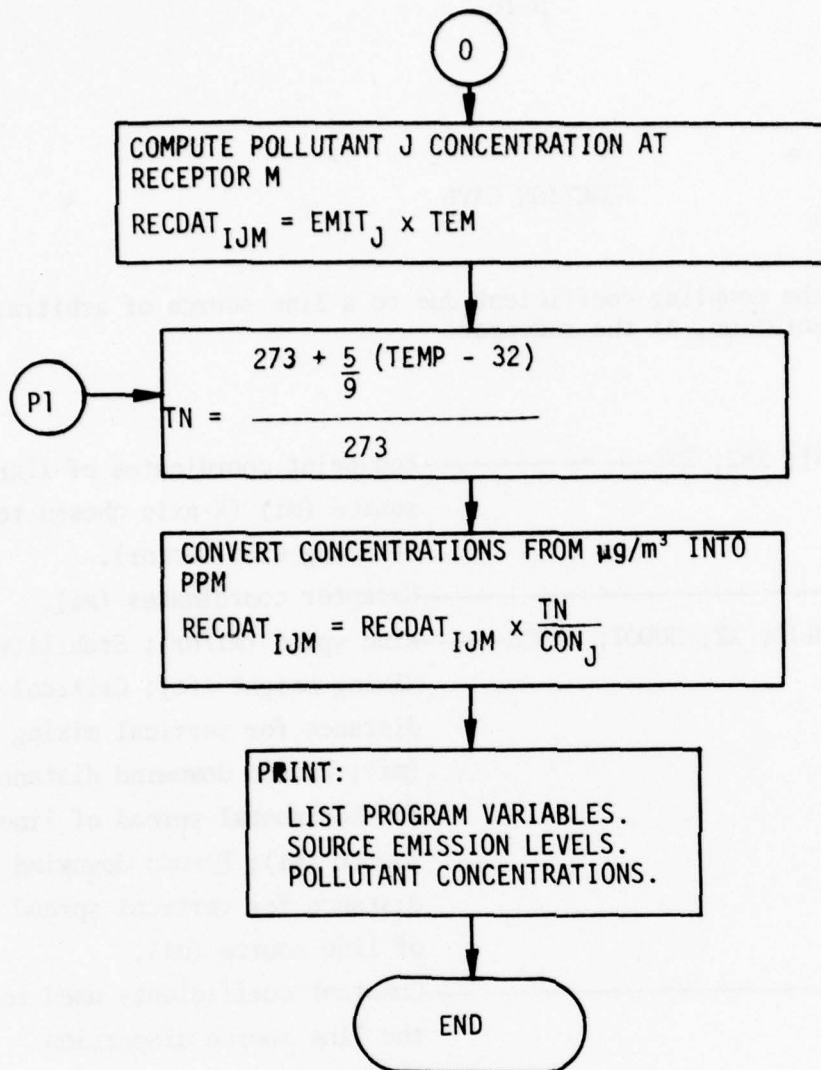
READ CARD TYPE 38
EMIT_J

M





B-15



FUNCTION CAVL

Purpose:

To compute the coupling coefficient due to a line source of arbitrary spatial orientation, at the receptor.

Input:

XW1, YW1, ZW1; XW2, ZW2 ————— End-point coordinates of line source (mi) (X-axis chosen to be along wind vector).

XR, YR, ZR ————— Receptor coordinates (mi).

WS; JSTAB; HLID; XZ; SUDOY; SUDOZ ————— Wind speed (mi/hr); Stability; Mixing height (ft); Critical distance for vertical mixing (mi); Pseudo downwind distance for horizontal spread of line source (mi); Pseudo downwind distance for vertical spread of line source (mi).

COEF1; COEF2 ————— Constant coefficients used in the line source dispersion equations.

Output:

CAVL (XR, YR, ZR) ————— Coupling coefficient (mi^{-2}) at the receptor point (XR, YR, ZR).

Procedure:

1. Test whether the receptor is located with respect to the line source such that the concentration is completely negligible.
2. If angle between wind vector and line is sufficiently small, and line source is sufficiently long, a flag is set for the line to be segmented. Each segment is then treated as an individual line.
3. Compute effective downwind distance.
4. Compute horizontal and vertical dispersion coefficients, using external function routines SIGY and SIGZ.
5. Compute the Z-component of the dispersion expression.

6. Test whether the line source has a uniform density. If it is a runway used for aircraft arrival or departure (nonuniform line density), subroutine QMOD is called.
7. Compute and output the concentration for the given receptor.

Functions Called:

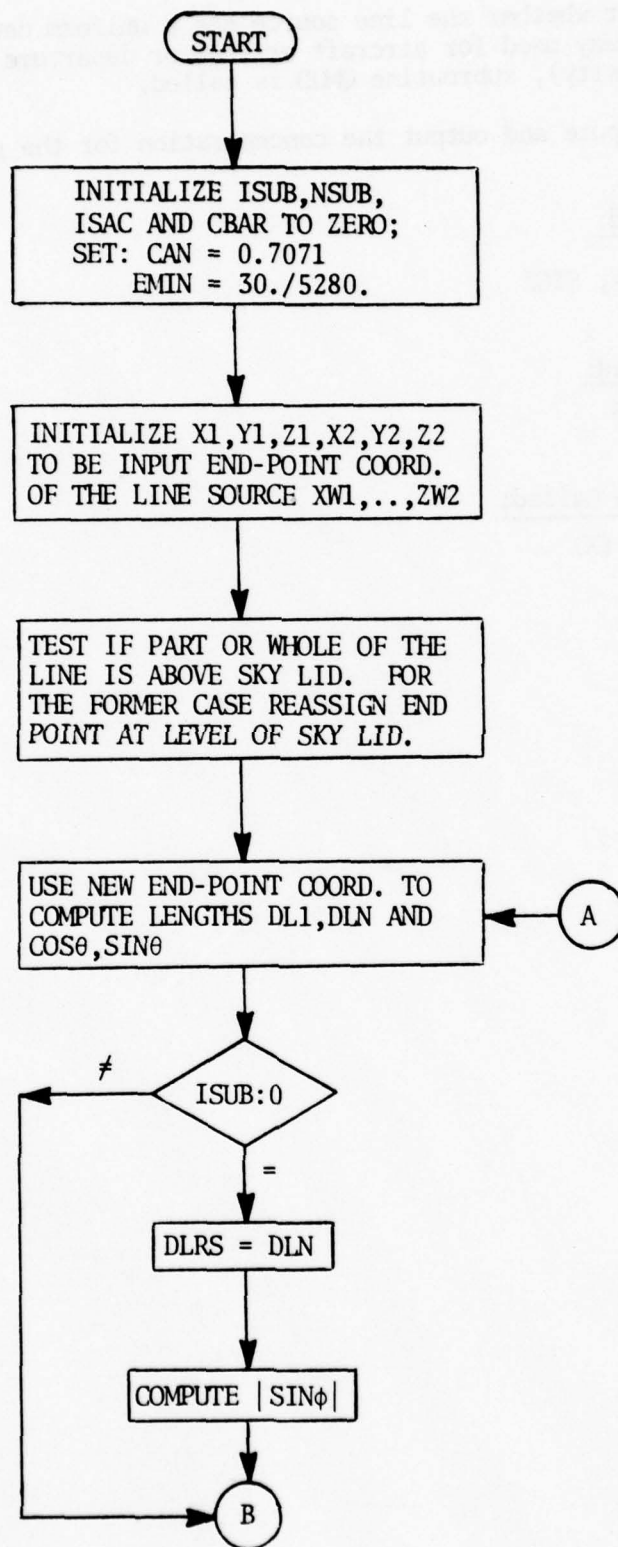
SIGY, SIGZ

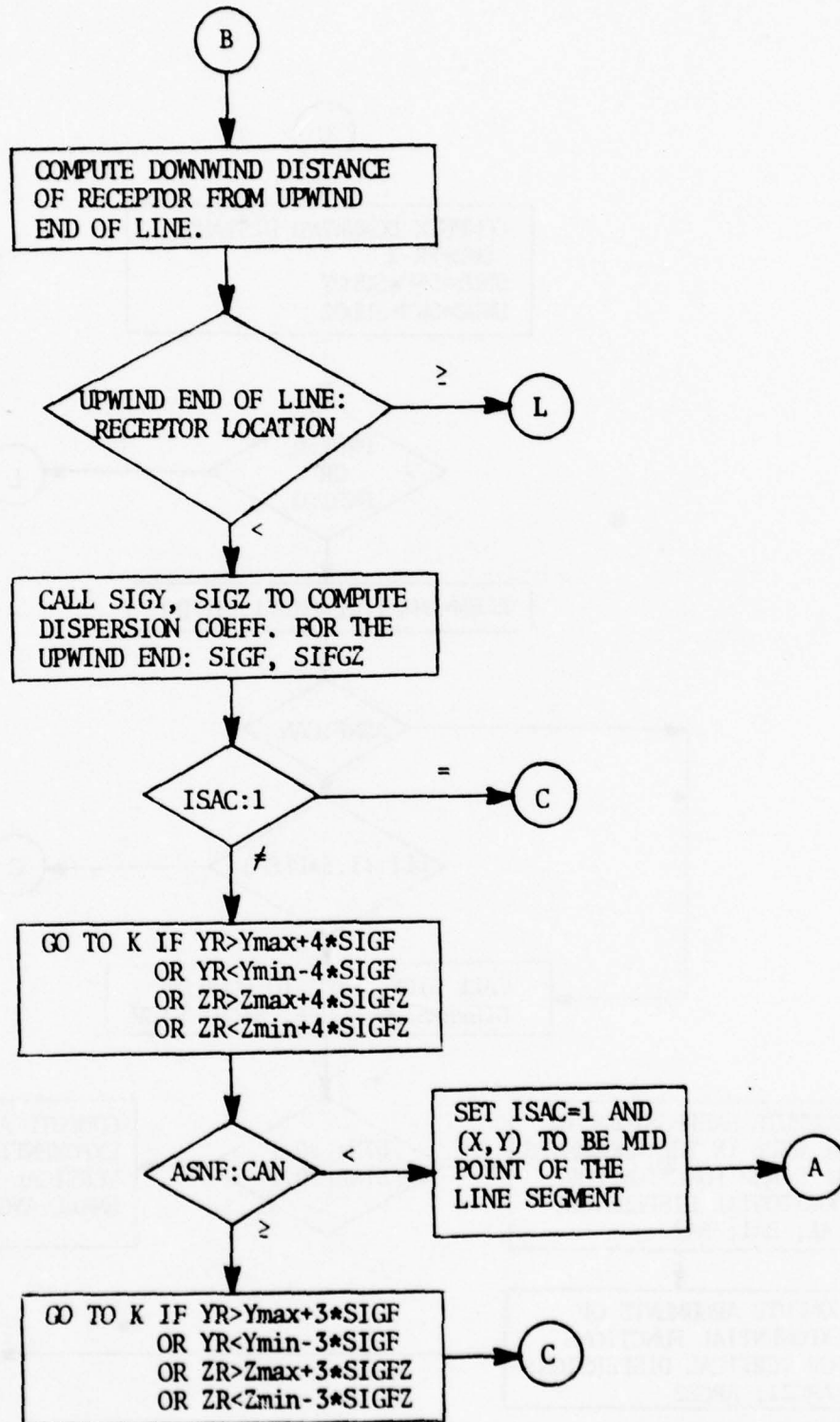
Subroutine Called:

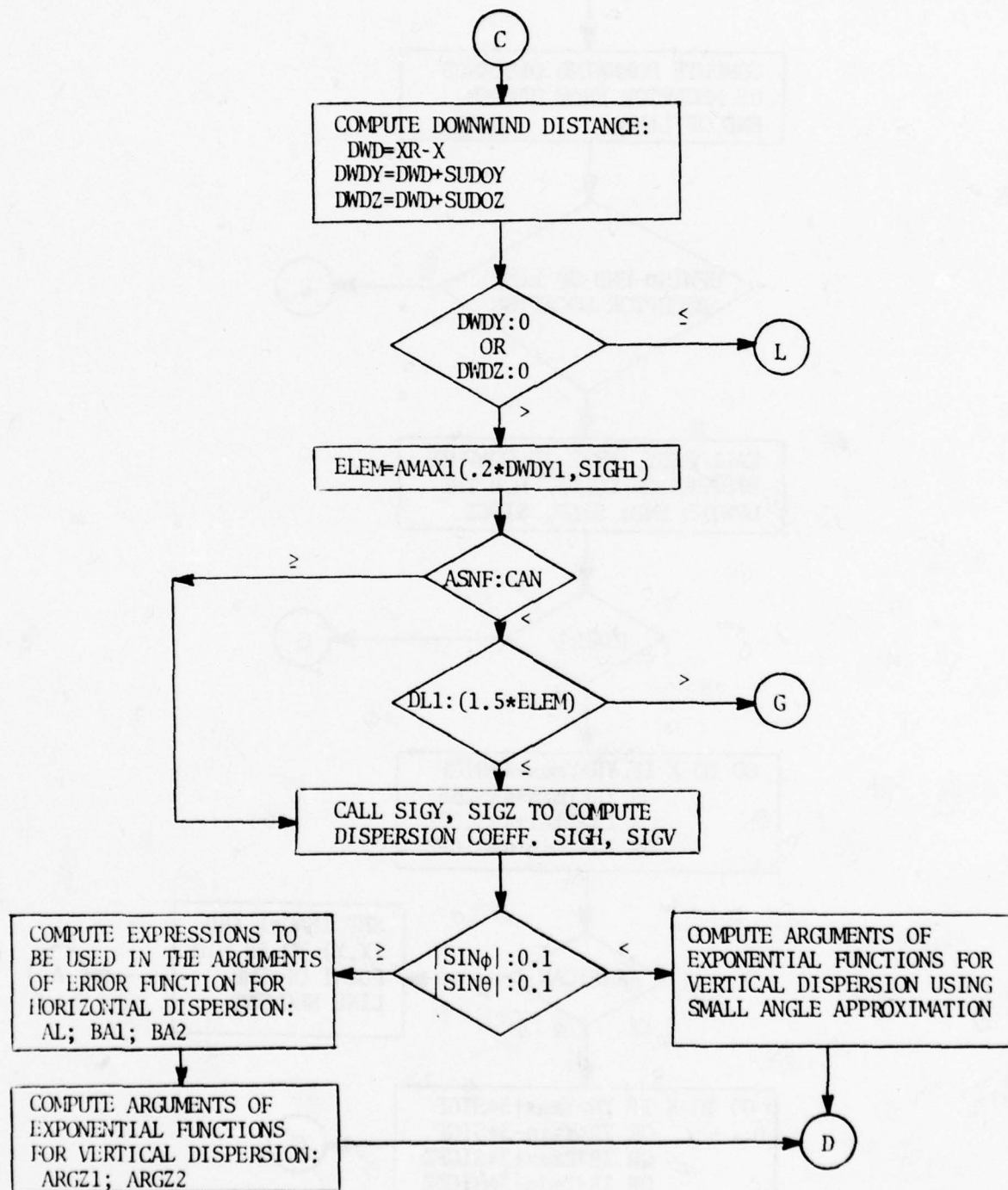
QMOD

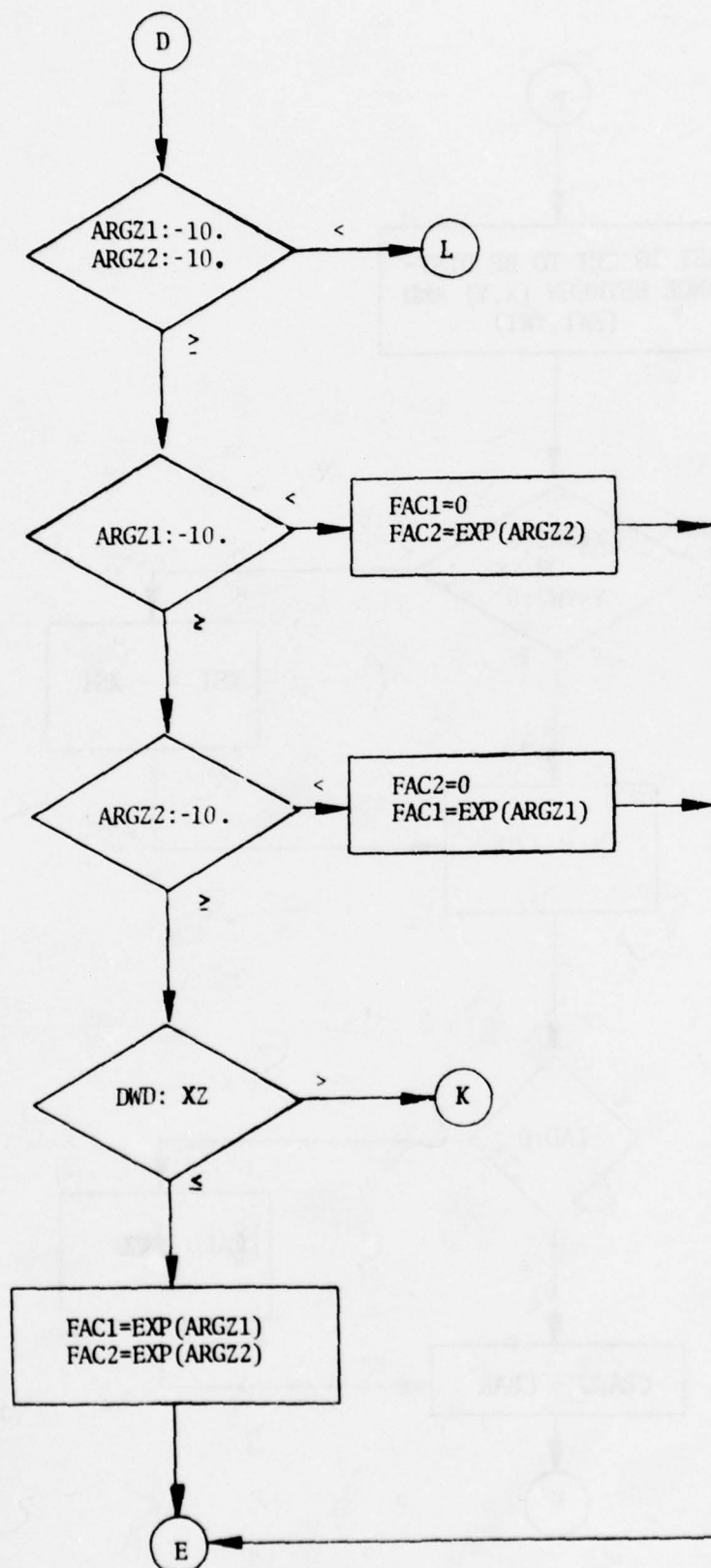
Special Function Called:

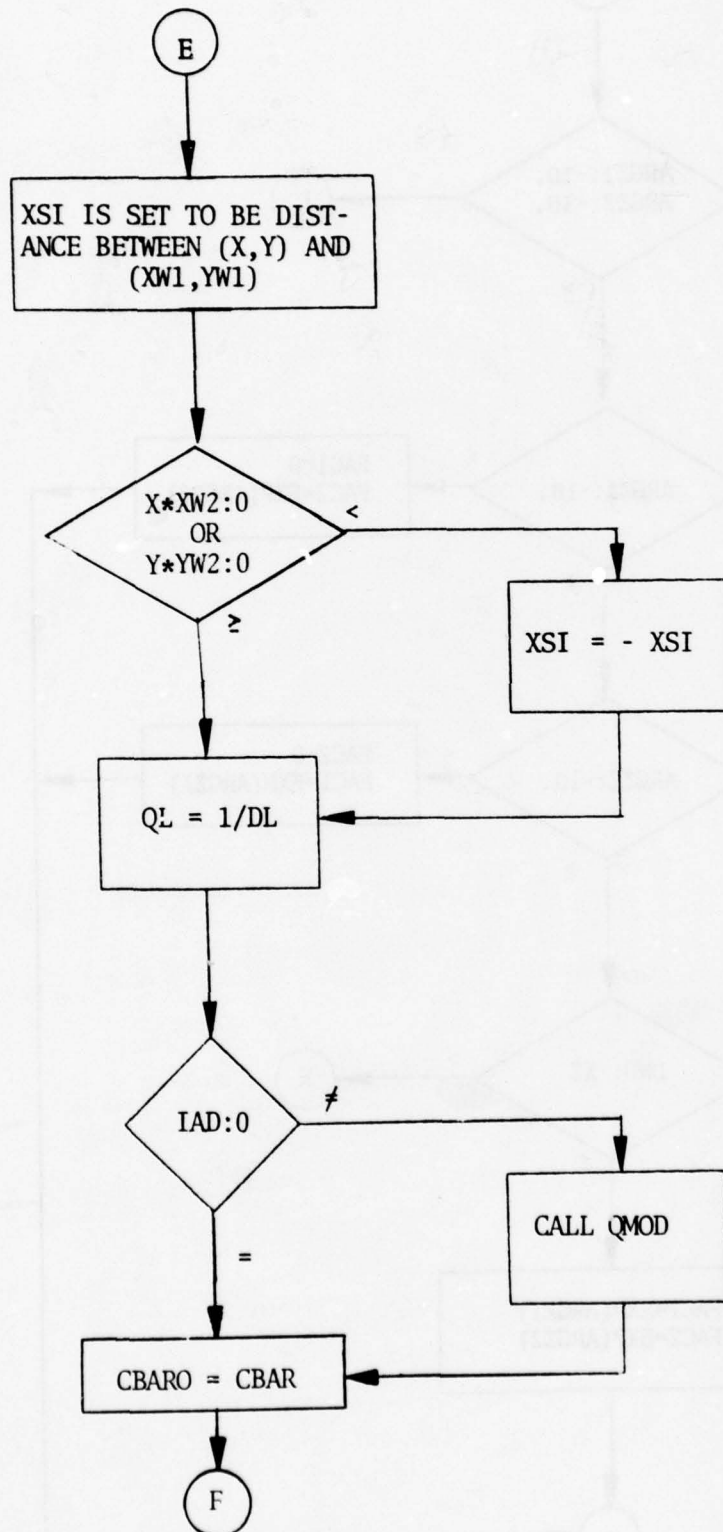
ERF (X)

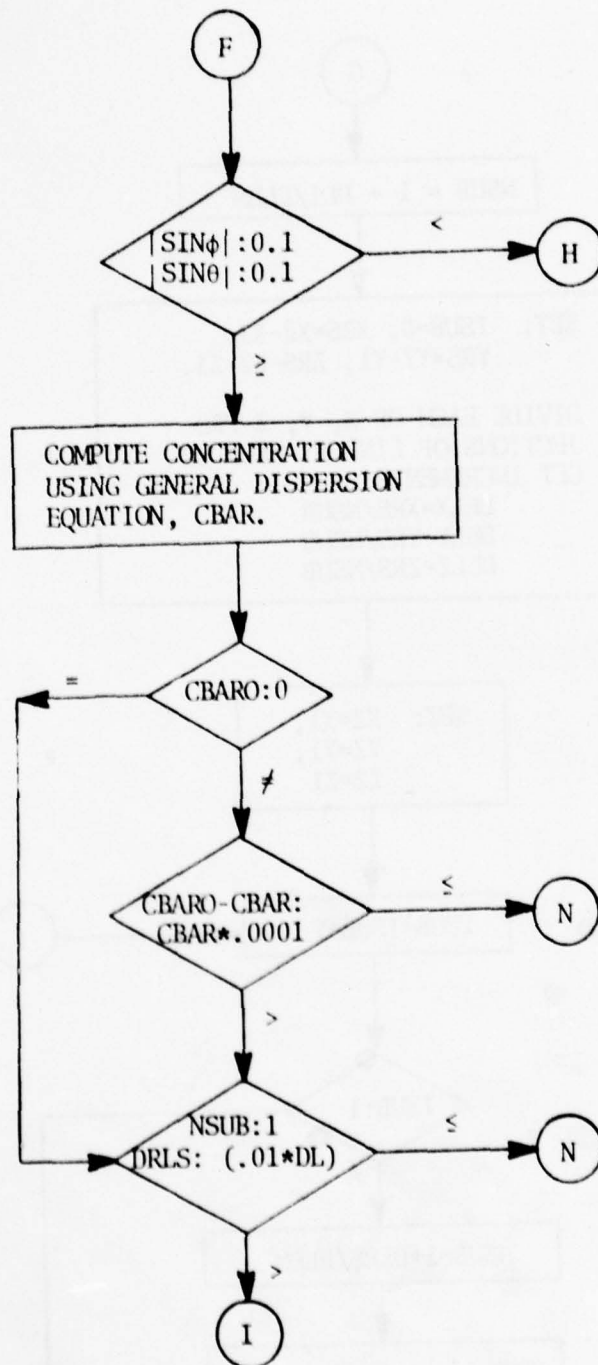


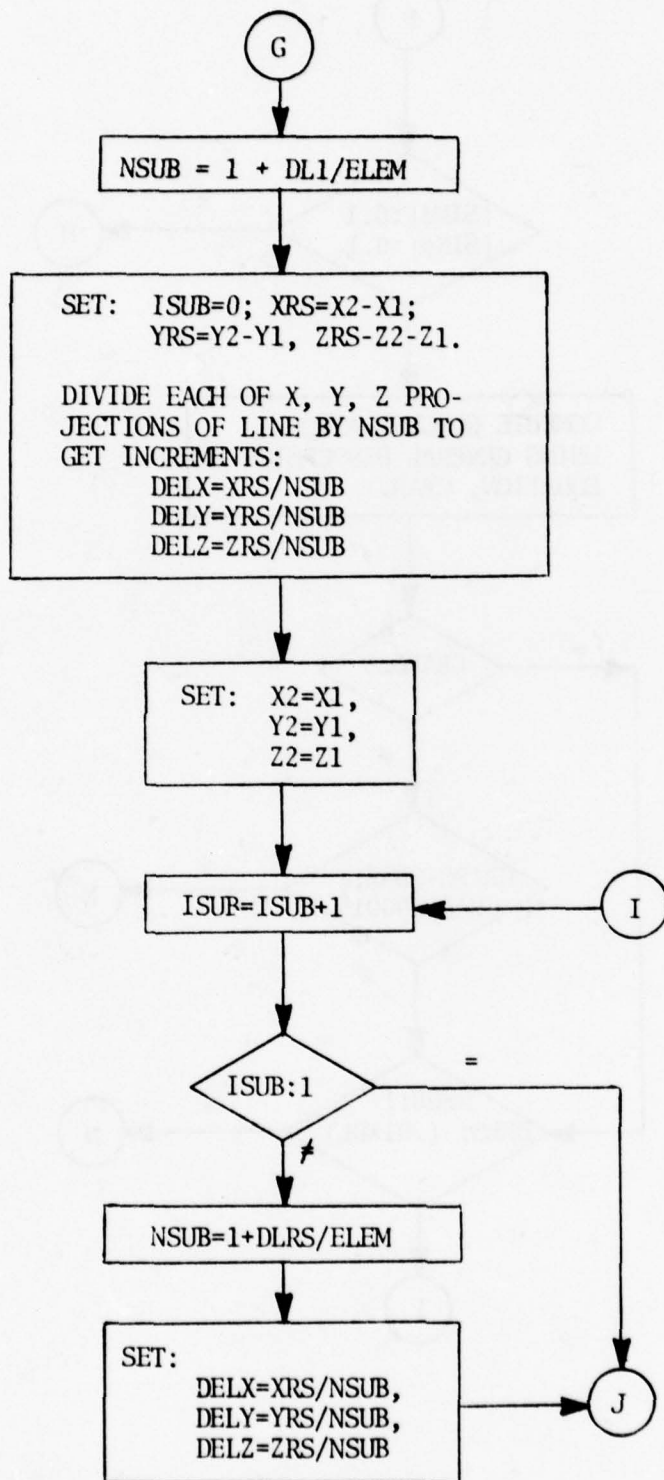


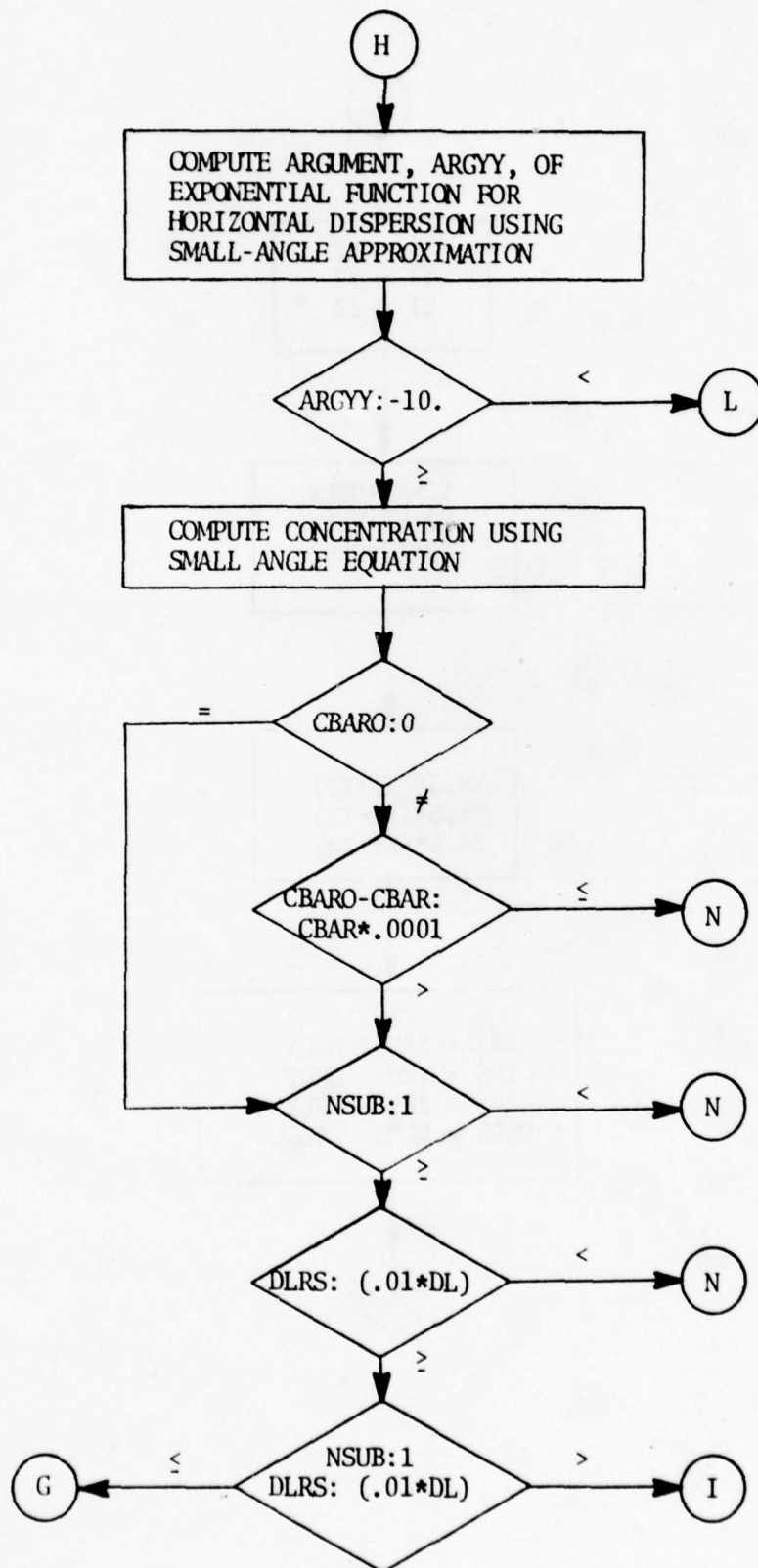


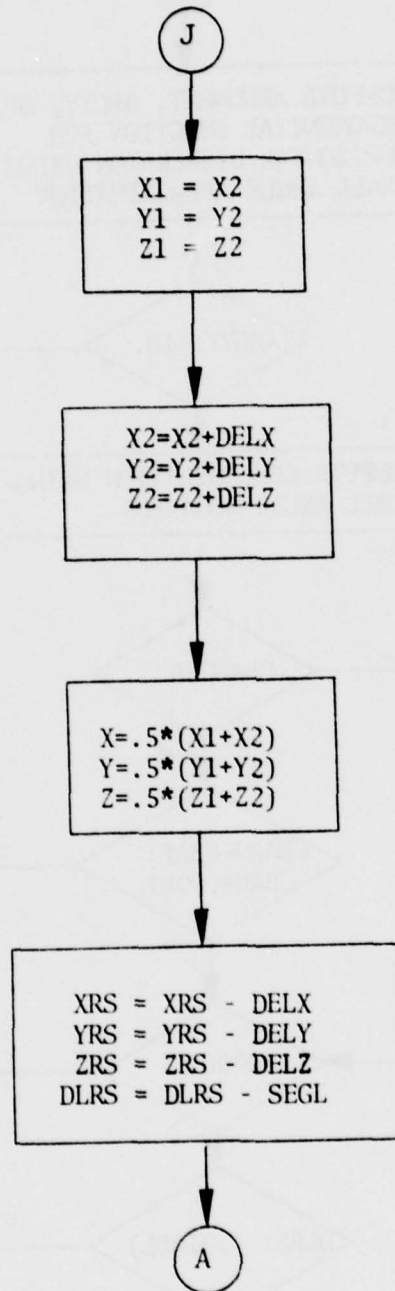


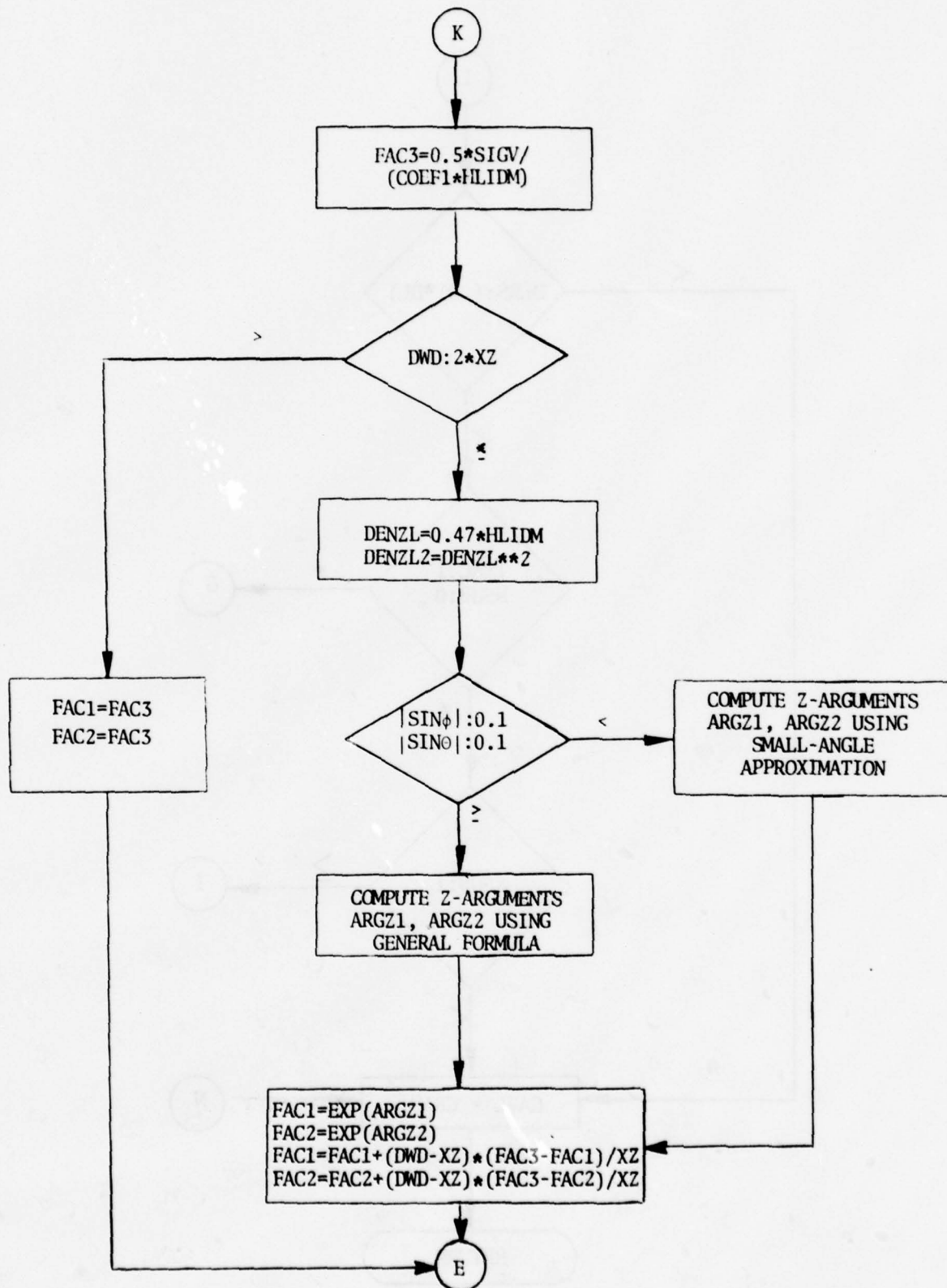


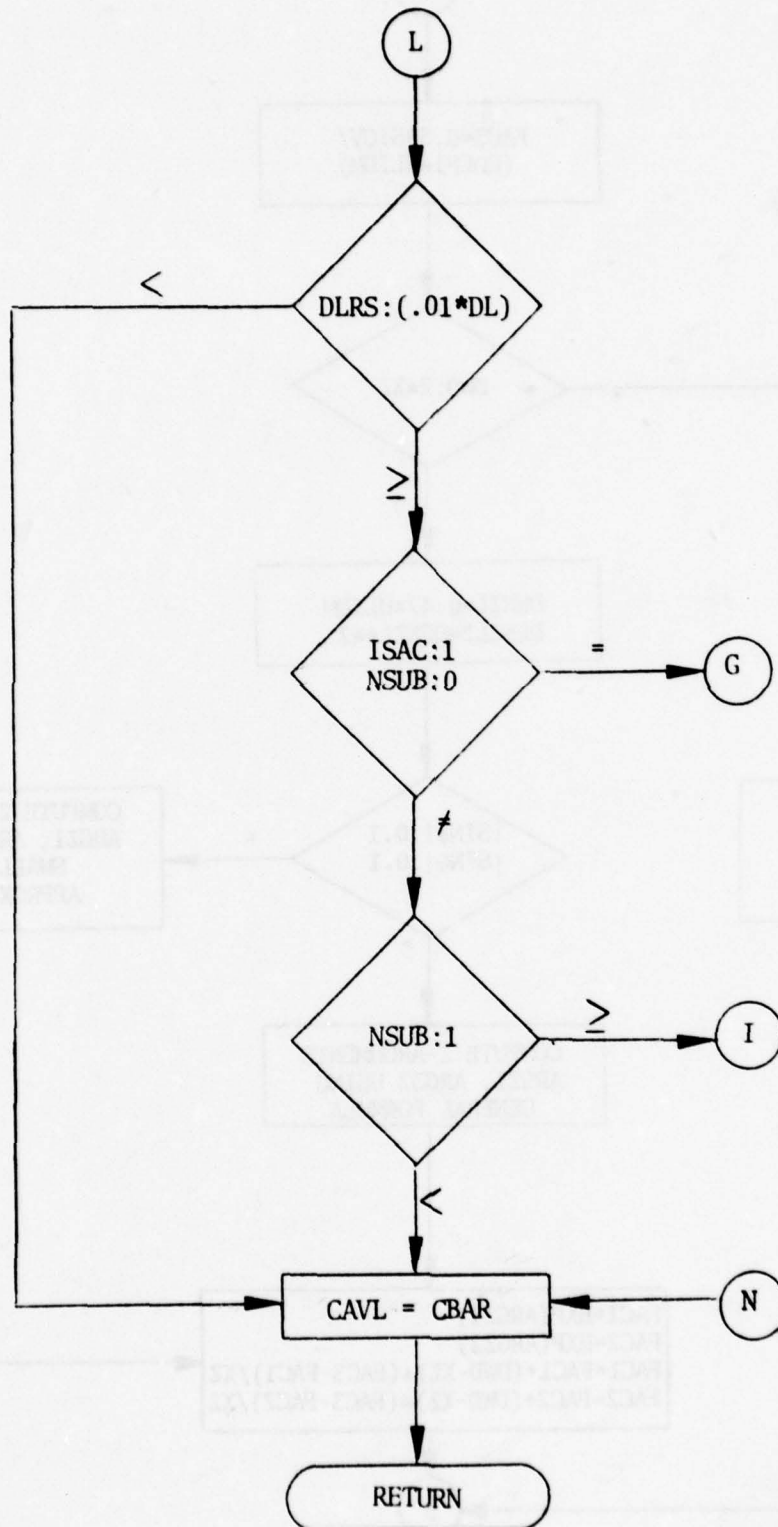












SUBROUTINE QMOD

Purpose:

To compute the linear distribution (in $(\text{Length})^{-1}$) of pollutant along runway due to aircraft emission during landing or takeoff.

Input:

YS1 ----- Distance along runway measured from the tip of
exhaust plume near the starting end of runway.
TAIL ----- Length or penetration of the exhaust plume of
aircraft at rest.
DL ----- Total length of the smoke slug on the runway.
A ----- Acceleration (or deceleration) of the aircraft.
V12 ----- Initial Velocity, V_1 , squared.
VS ----- Average velocity of the exhaust particles relative
to the air mass in the tail or exhaust plume.
WS2 ----- Wind speed squared.
WSC ----- $2 * (\text{Wind Speed}) * (-\cosine \text{ of angle between runway and } \\ \text{wind vector}).$
RR ----- A/G , where A is the acceleration of the aircraft and
G is the normalization constant for line density.

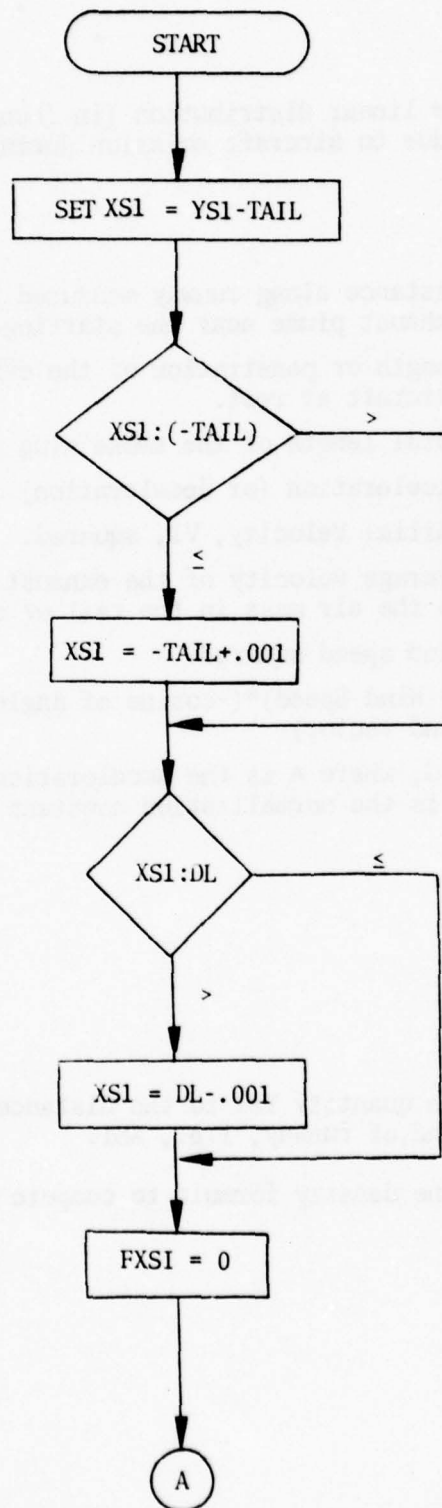
Output:

QL

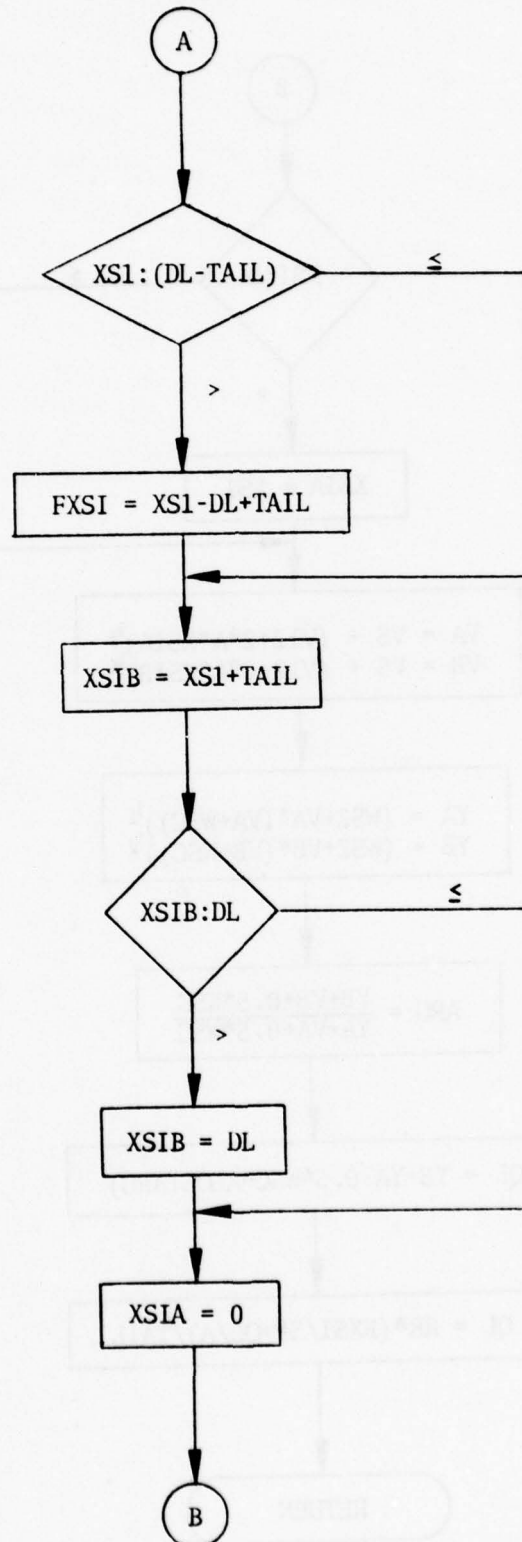
Procedure:

1. Convert the quantity YS1 to the distance measured from the physical end of runway, i.e., XS1.
2. Use the line density formula to compute $QL(1/\text{Length})$.

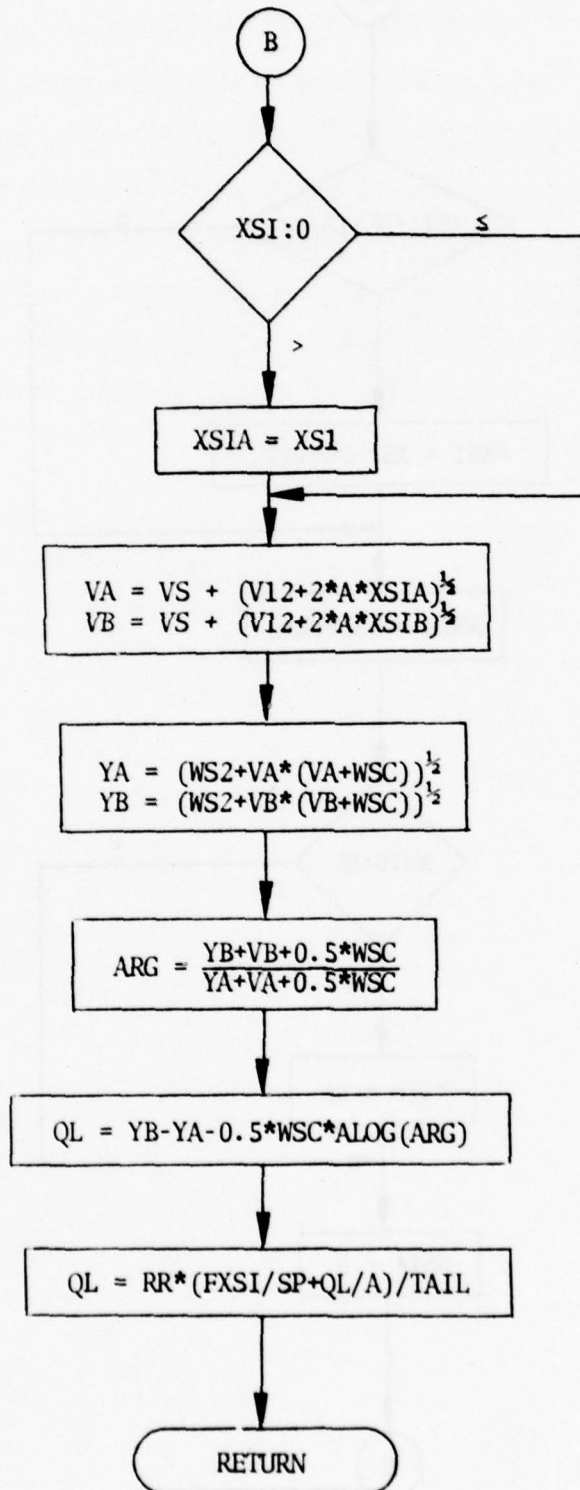
SUBROUTINE QMOD



SUBROUTINE QMOD (Continued)



SUBROUTINE QMOD (Continued)



FUNCTION TRAN

Purpose:

To compute the coupling coefficient at the receptor point due to a point or area source.

Input:

1. Meteorological parameters: wind speed; stability; mixing height; critical distance for mixing.
2. Source parameters: horizontal and vertical spreads; pseudo transport times corresponding to the horizontal and vertical spreads; area source flags: KSTAB, NRFLAG, and IBACK.
3. Receptor parameters: downwind and crosswind distances; receptor height.

Output:

Point or area source coupling coefficient: TRAN.

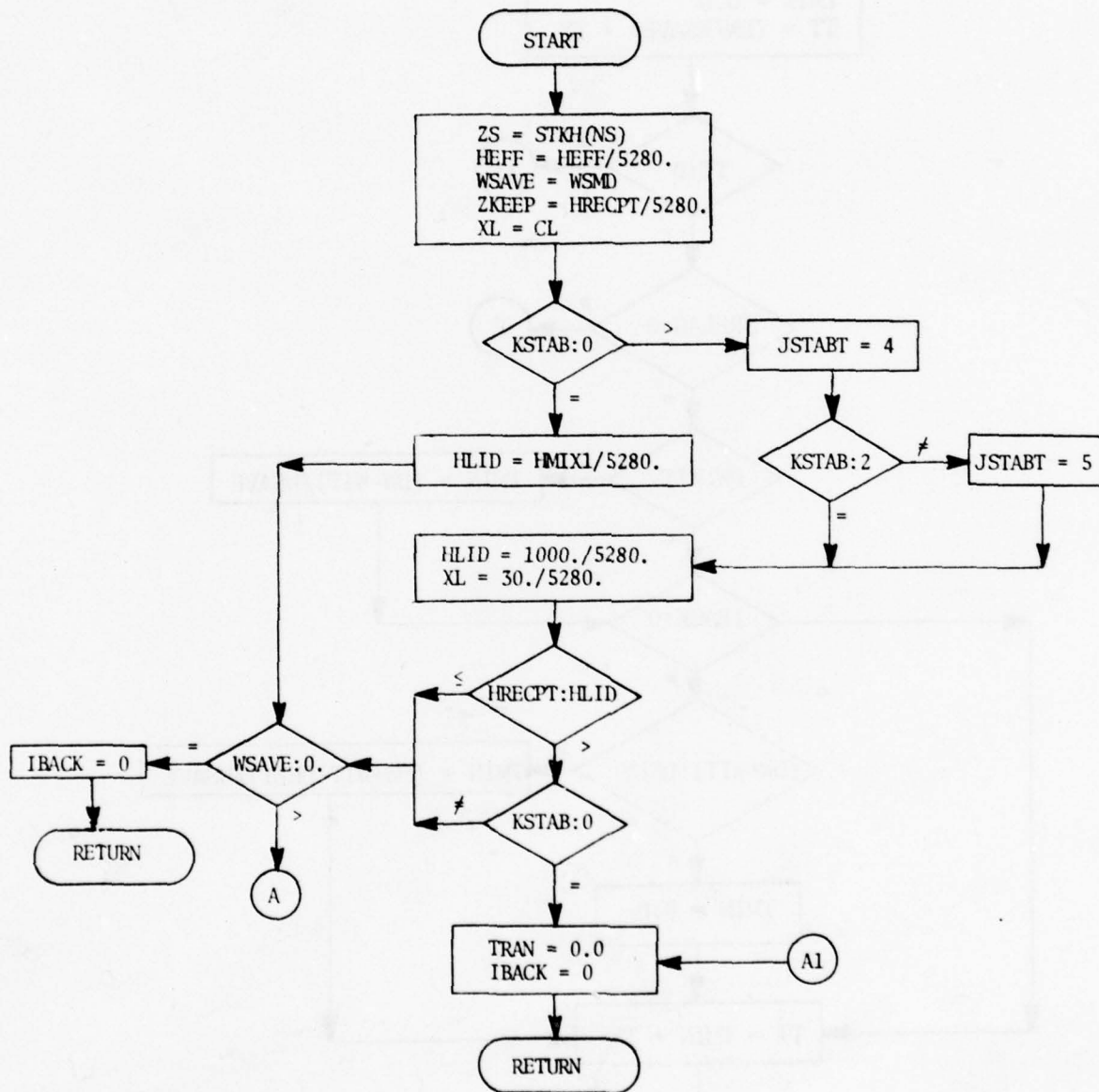
Procedure:

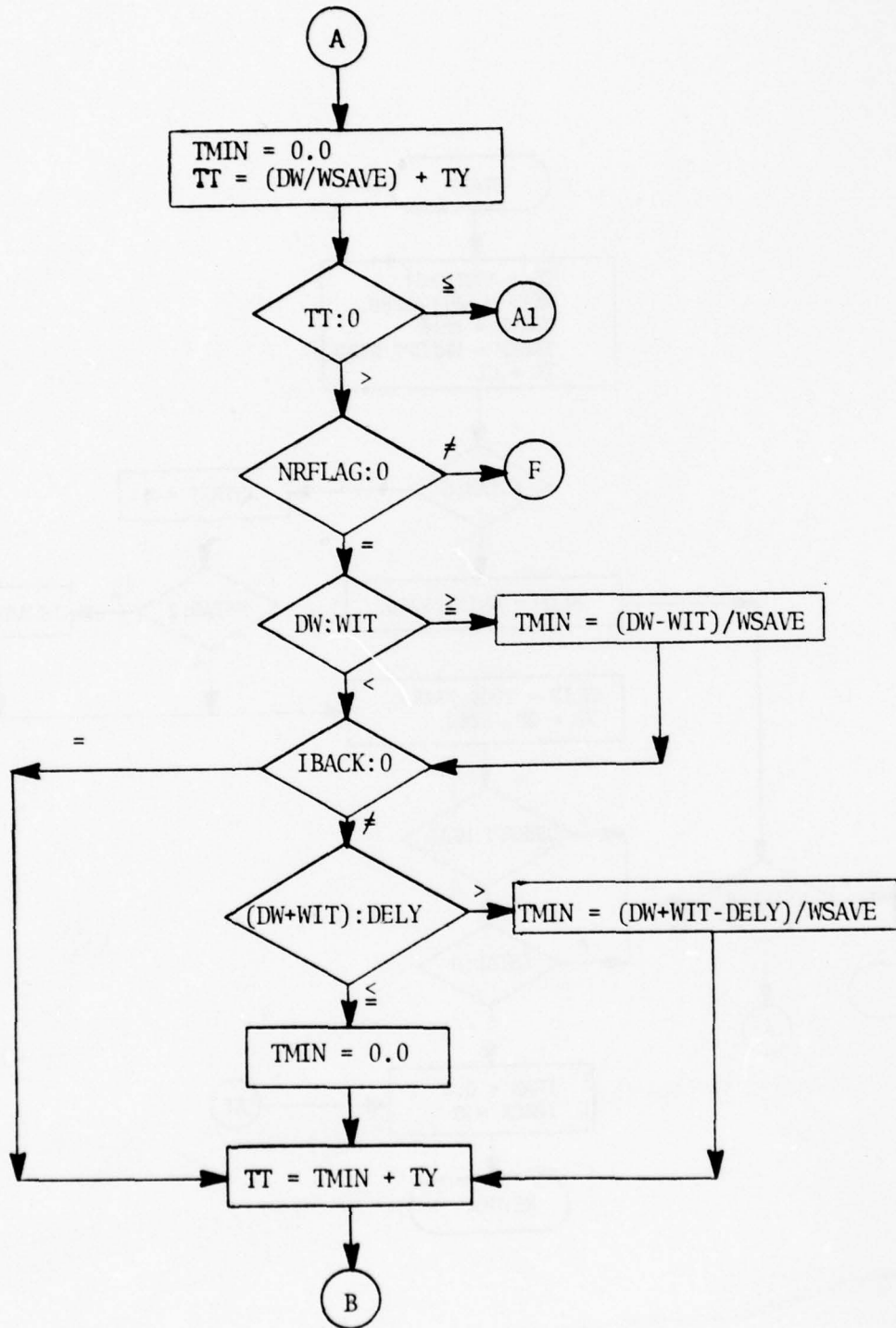
1. If the effective stack height exceeds the height of the sky lid, then stability index is reassigned according to the current hourly atmospheric stability and the source flag KSTAB computed in PLUME.
2. For point source and area source with source flag NRFLAG = 0, compute the travel time for z dispersion from the center and that for y dispersion from the downwind edge of the source.
3. For sources with NRFLAG = 0 the effects of ground and sky lid are treated by the image method. Up to 6 terms are included in the coupling coefficient.
4. For area source with NRFLAG = 1, the travel times from the downwind and upwind edges of the area sources are determined on the basis of receptor location relative to the area source. These plus the pseudo travel time T_z due to the Z-spread are used to compute the Z-dispersion coefficients $\sigma_z(T_1)$ and $\sigma_z(T_2)$.
5. For area source with NRFLAG = 1, the y-dispersion coefficient $\sigma_y(TT)$ is determined on the basis of the pseudo travel time T_y due to the y-spread and the travel time from the downwind edge to the receptor.
6. The coupling coefficient for area source with NRFLAG = 1 is then computed using the integrated expression for "near" source.

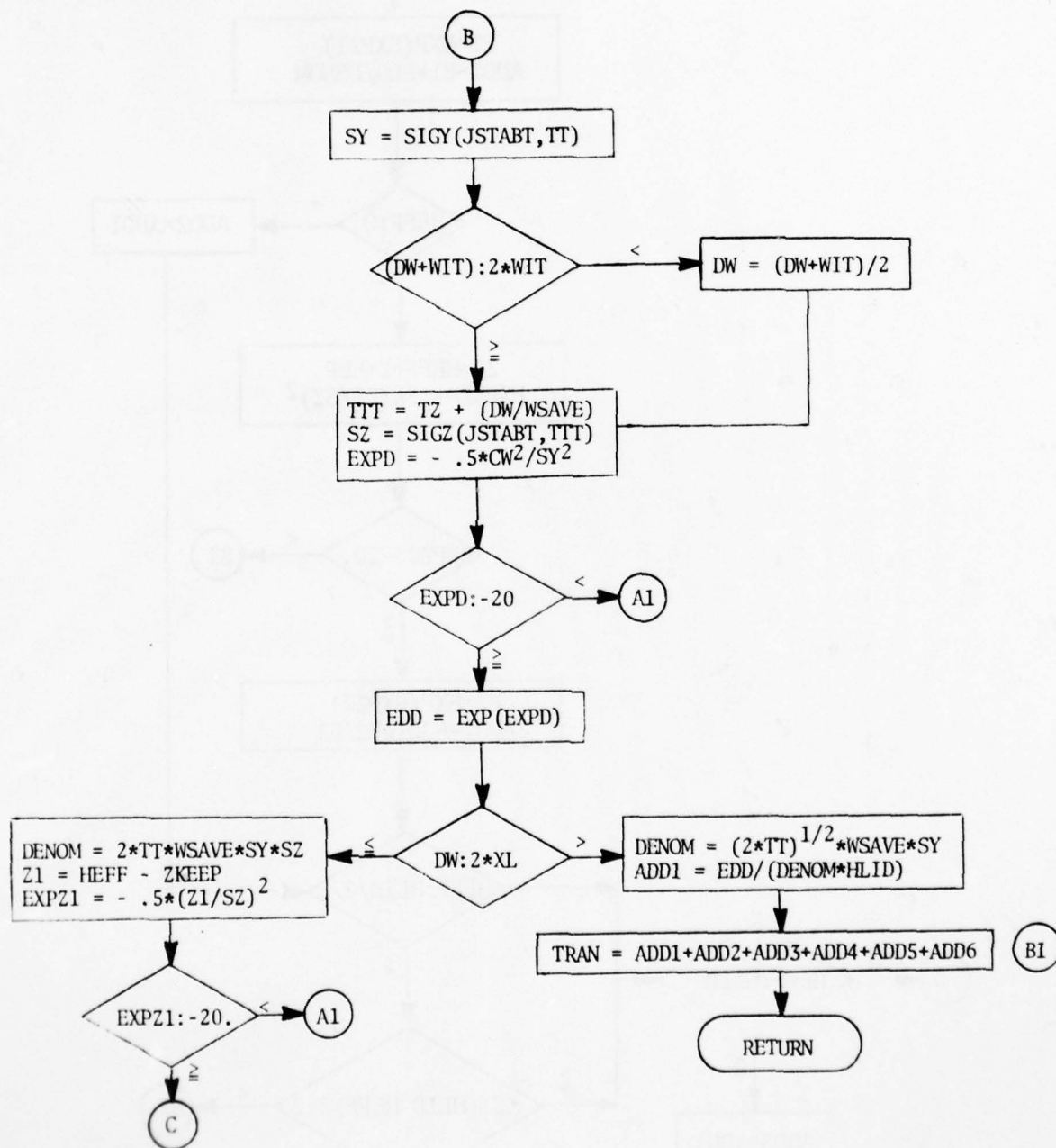
7. If the source flag IBACK is 1, part of the area source is to be treated as "near" and part as "far" area sources. When both contributions to the coupling coefficient are computed and summed, IBACK is then set to 0.

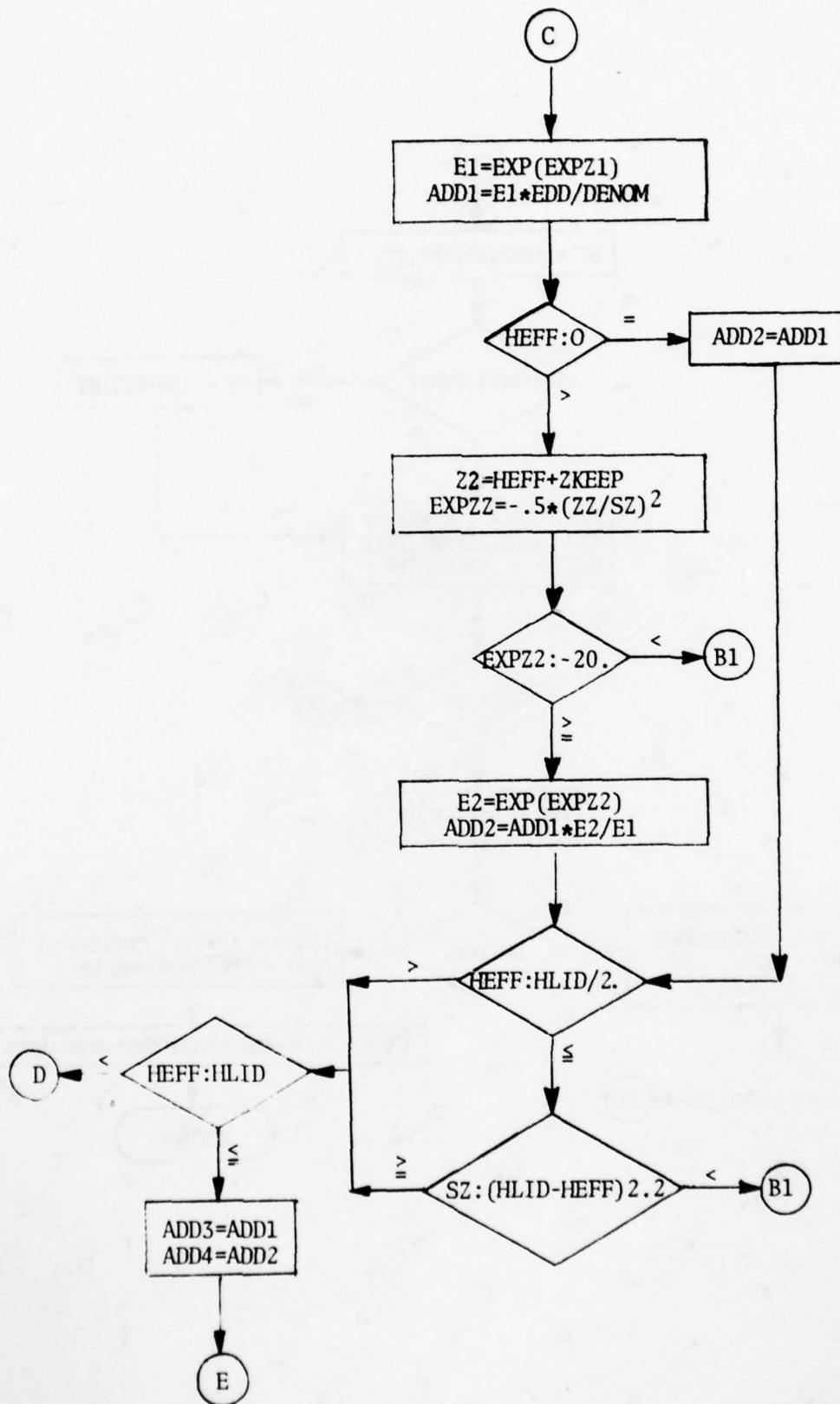
Functions Called:

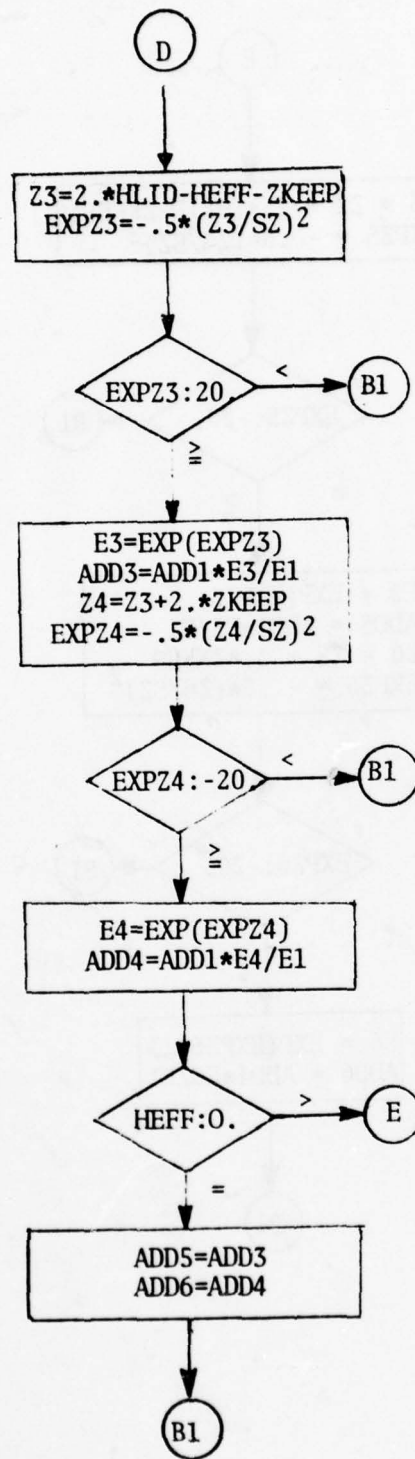
SIGY, SIGZ

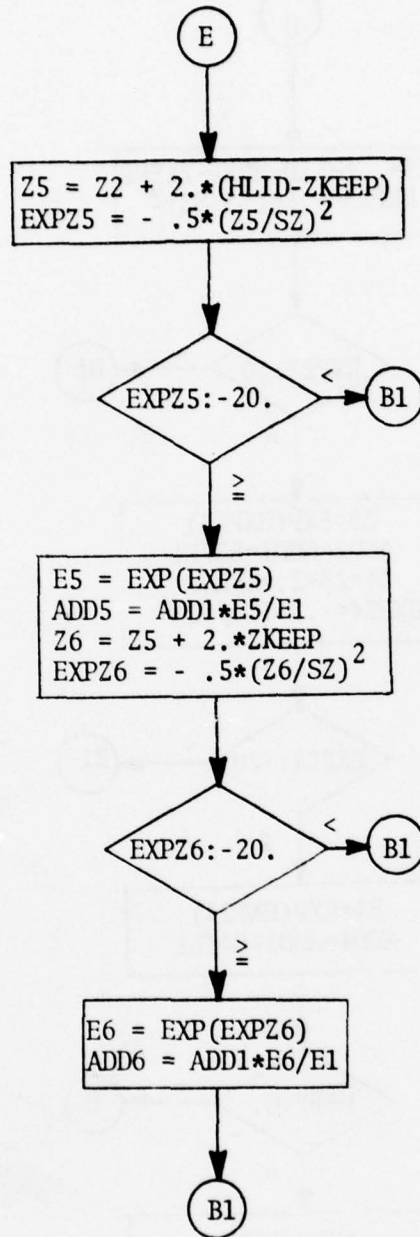


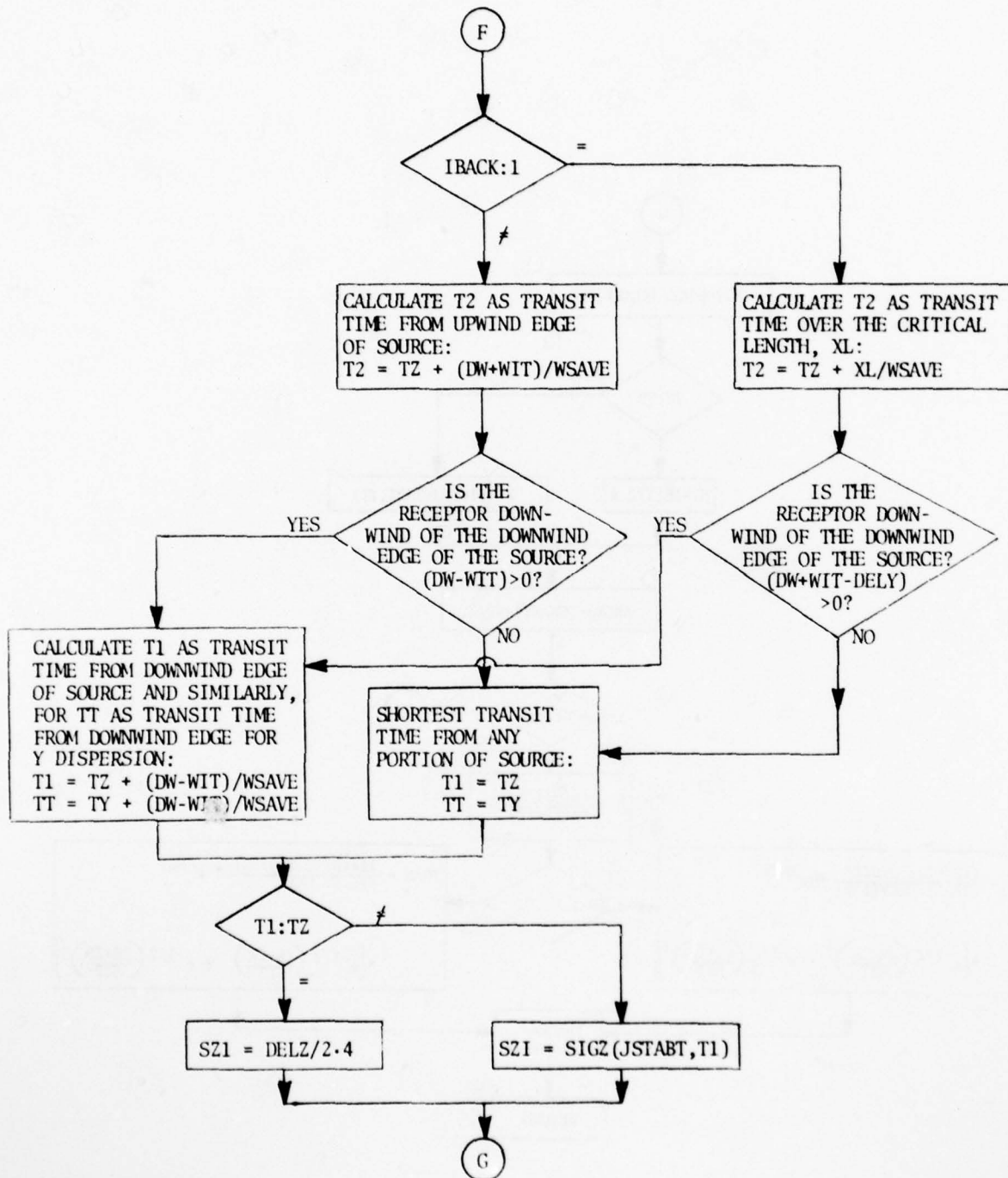


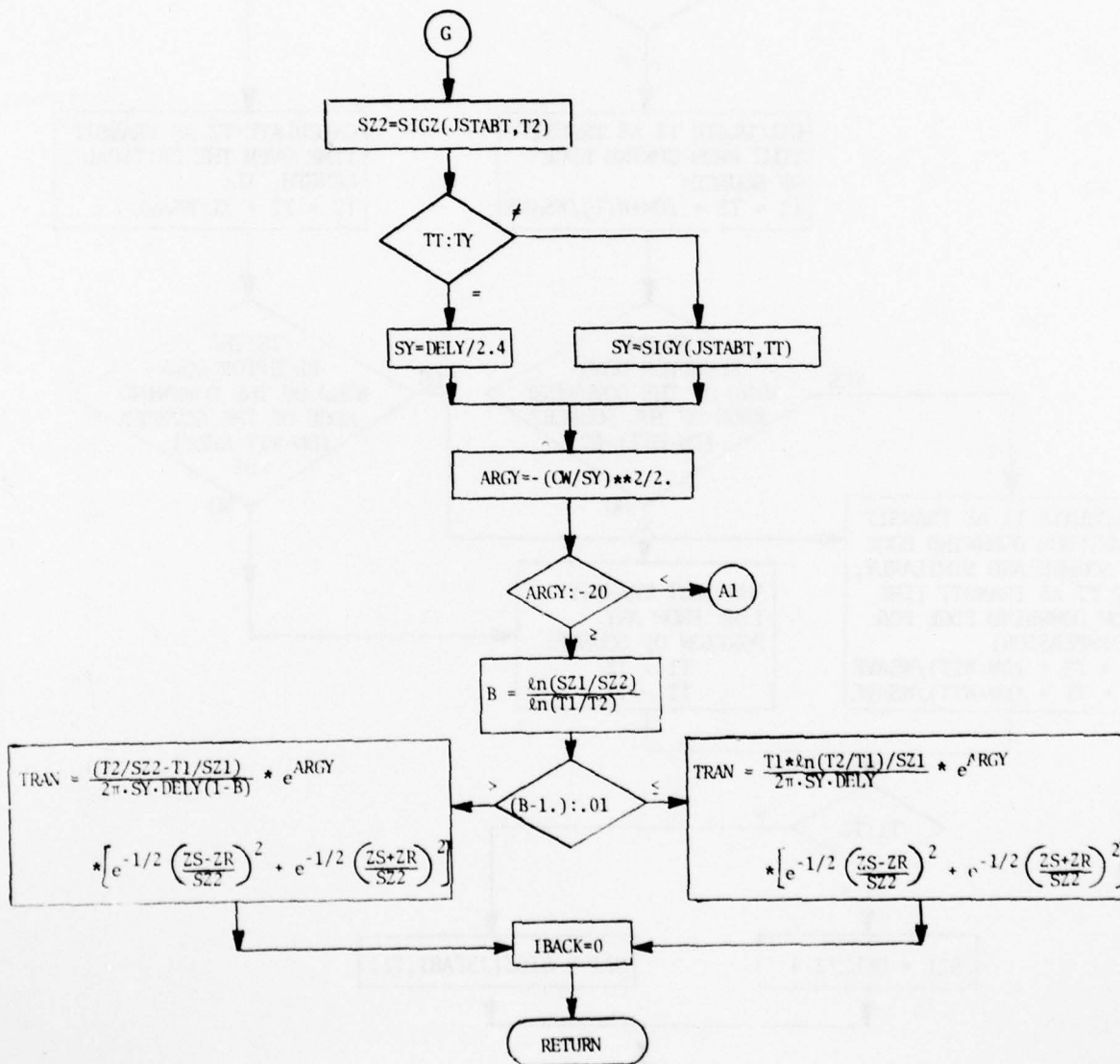












APPENDIX C

FORTRAN LISTING OF THE AVAP MODEL ABBREVIATED VERSION

```

C...  AVAP MAIN PGM                                00000001
REAL*4 TITLE1(20),TITLE(10)                        00000002
REAL*4 NAME(10)                                     00000003
REAL*8 SRNAME(14),NAUT(5)                           00000004
INTEGER OUTPUT,DEFAULT(23)                          00000005
DIMENSION EMIT(5,2)                                  00000006
DIMENSION IKA(10),IKB(10)                          00000007
DIMENSION SDY(2)                                    00000008
C  EMIT CONTAINS FIVE POLLUTANT EMISSION RATES FOR TWO AREA SOURCES 00000009
DIMENSION XRECP(20),YRECP(20),ZRECP(20),NRUSED(20) 00000010
DIMENSION CCN(10)                                   00000011
DIMENSION XA(7),YA(7),ZA(7),XB(7),YB(7),ZB(7)      00000012
DIMENSION RTXY(2),EMLN(5),EMTF(5)                  00000013
DIMENSION CCUP(20),TERM(5),EMTXI(5),EMTXO(5),      00000014
- RWIDL(5,2),EMID(5),EAPU(5)                        00000015
DIMENSION ALSC(60,6)                               00000016
DIMENSION ALSE(60,6)                               00000017
DIMENSION PLTINT(5),SRVHL(14)                      00000018
DIMENSION CWS(2),DWS(2),CWR(20),DWR(20),RECDAT(4,5,20) 00000019
DIMENSION HEFF(5),KSTAB(5)                         00000020
COMMON/DEFLT/NAC(10),FLNCG(10),FTKOF(10),NGIN(10),INGN(10), 00000021
LFMI(5,4,5),CSRW,HRW, FTAXI(10),                  00000022
2FTXII(10),FTXIO(10),DSTW,HTW,DSRA,HRA,EFUH(5),EFUL(5),CSAR,HAR, 00000023
3SPVTIM(10,14),KAPU(10),APU(5),FIDLE(10),TGND(10),DEFAULT 00000024
COMMON/DELTA/DELY,DELZ                             00000025
COMMON/FUEL/FFD(5),EFG(5)                          00000026
COMMON/LN/DL,XW1,YW1,ZW1,XW2,YW2,ZW2,COEF1,COEF2,VA1,VA2,VF1,VD2, 00000027
-C,TIME,VA12,VA22,VD12,VD22,WS2,WSC,JAD,SNAN,CSAN,V1,V2,V12,V22, 00000028
-TAIL,VS,RR,SP                                     00000029
COMMON/LN1/IAEC                                    00000030
COMMON/LGC/DW,CW                                   00000031
COMMON/MET/WS,WD,JSTAB,HLID,TEMP,XL,SUDGY,SUDGZ    00000032
COMMON/PL4/XS(5),YS(5),STKH(5),WIT(5)              00000033
COMMON/POL/NPT,IJ(5)                               00000034
COMMON/RECPT/HRECPT,HTAFRD,ZRECPG                  00000035
COMMON/RISE/ZSS                                    00000036
COMMON/SEUDO/TXT,TYT,TZT                          00000037
COMMON/SERVHL/SRNAME                               00000038
COMMON/XTRAN/WSMD,NCALM,SQTOPI                     00000039
DATA NAME/'CO ','THC ','NOX ','PART','SOX ',5*''/' 00000040
DATA NAUT/'CO (PPM) ','THC (PPM)','NOX (PPM)','PT (M/CM)','SO2 (PPM) '/' 00000041
DATA BLANK/' '/'                                   00000042
DATA SQ2PI /2.5066283 /                             00000043
C  CCNVF CONVERTS LBS/MI**3 INTO MICRO GM/M**3      00000044
DATA CCNVF/.10882139/                              00000045
DATA CCN/1250.,666.,2054.,1.,2854.,5*1./          00000046
INPUT = 5                                           00000047
OUTPUT = 6                                          00000048
READ(INPUT,17) TITLE1                              00000049
READ(INPUT,19) (TITLE(I),I=1,10)                  00000050
WRITE(OUTPUT,17) TITLE1                           00000051
WRITE(OUTPUT,31) (TITLE(I),I=1,10)                 00000052
17 FORMAT(20A4)                                    00000053

```


14 FORMAT(10A4)	00000054
C.. SCAN THE POLLUTANT SPECIFICATION CARD.	00000055
NPT = 0	00000056
I = 1	00000057
L = 1	00000058
IFLAG = 1	00000059
500 IF(NAME(I).EQ.TITLE(L)) GO TO 502	00000060
505 L = L+1	00000061
IF(L.LE.10) GO TO 500	00000062
I = I+1	00000063
IF(I.GT.10) GO TO 501	00000064
L = 1	00000065
GO TO 500	00000066
501 IF(IFLAG.EQ.1) GO TO 503	00000067
GO TO 504	00000068
502 IF(TITLE(L).EQ.BLANK) GO TO 505	00000069
NPT = NPT+1	00000070
IFLAG = 0	00000071
506 IJ(NPT) = 1	00000072
IF(NPT.EQ.1) GO TO 510	00000073
IF(IJ(NPT).EQ.IJ(NPT-1)) GO TO 507	00000074
510 CONTINUE	00000075
IF(I.LT.10) GO TO 505	00000076
GO TO 504	00000077
503 WRITE(OUTPUT,508) (TITLE(I),I=1,10)	00000078
508 FORMAT(1H1,' ERROR---POLLUTANT NAME NOT FOUND ',10A4)	00000079
GO TO 504	00000080
507 WRITE(OUTPUT,509) TITLE(L)	00000081
509 FORMAT(1H1,' DUPLICATE POLLUTANT REQUEST ',A4)	00000082
NPT = NPT-1	00000083
GO TO 506	00000084
504 CONTINUE	00000085
NXTI = 2	00000086
NSVR = 14	00000087
NPAV = 1	00000088
NAPR = 2	00000089
C.. READ HEIGHT OF AEROVANE FOR WIND MEASUREMENT	00000090
READ(INPUT,4713) HTAERO,WSP,DIR,TEMP,JSTAB,NLID,NMONTH,NP	00000091
4713 FORMAT(4F8.0,2I8,2I2)	00000092
READ(INPUT,12) NSR,NACT,NENT,NAVP,NACA,NANA	00000093
C.. SELECT DEFAULT OPTIONS.	00000094
C	00000095
REAL(INPUT,1)(DEFAULT(I),I=1,23)	00000096
C	00000097
C.. READ RECEPTOR COORDINATES X,Y, IN MILES, Z IN FEET.	00000098
READ(INPUT,4711)(NRUSED(N),XRECP(N),YRECP(N),ZRECP(N),N=1,NSR)	00000099
DO 2263 K1=1,4	00000100
DO 2263 IL = 1,NPT	00000101
K2 = IJ(IL)	00000102
DO 2263 K3=1,NSR	00000103
2263 RECDAT(K1,K2,K3)=0.0	00000104
TEM = TEMP	00000105
WD = DIR	00000106
WS = WSP*1.15	00000107
JSTABF = JSTAB	00000108

```

C.. FUNCTION HMX WILL RETURN A VALUE FOR MIXING DEPTH                                00000109
  HLID = NID*10                                                                    00000110
  IF (HLID.EQ.0.0) HLID=HMX(JSTAB,NMETH,NR,WS)                                    00000111
  WRITE(OUTPUT,34) NSR,NRWY,NTXI,NAPR,NACA,NACT,NENT,NSVP,NAVR,NANA 00000112
  WRITE(OUTPUT,9711) NSR,(XRECP(N),YRECP(N),ZRECP(N),N=1,NSR) 00000113
  WRITE(OUTPUT,9744)(NPUSF(N),N=1,NSR) 00000114
  WRITE(OUTPUT,9734) HTAFRO,WS,DIR,TEMP,JSTAB,HLID 00000115
C.. COMPUTE SINE AND COSINE OF THE WIND ANGLE 00000116
  WCRAD=WD*.01745 00000117
  SINWD=SIN(WCRAD) 00000118
  COSWD=COS(WCRAD) 00000119
  A=WS*SINWD 00000120
  B=WS*COSWD 00000121
  HL=HLID*.047/5280. 00000122
  DS=0. 00000123
  KL=2 00000124
  TX=0. 00000125
  TY=0. 00000126
  TZ=0. 00000127
  CALL PSEUDO(DS,A,B,TX,TY,TZ,DX,DY,JSTAB,HL,KL) 00000128
  XL=WS*TZ 00000129
  WS2 = WS*WS 00000130
  WAN = 270.-WD 00000131
  WAN = WAN*3.1415927/180. 00000132
  CSAN = COS(WAN) 00000133
  SSAN= SIN(WAN) 00000134
C.. INPUT AIRCRAFT ARRIVAL AND DEPARTURE ACTIVITY BY TYPE . 00000135
C.. 00000136
  IF(DEFAULT(1).NE.0) 00000137
  IREAD(INPUT,5)(NAC(I),I=1,NACT) 00000138
  WRITE(OUTPUT,580) NACT,(NAC(K),K=1,NACT) 00000139
580 FORMAT(1X,'ARRIVAL ACTIVITY FOR AIRCRAFT TYPES 1 THROUGH',I3 00000140
-,2X,10I3) 00000141
C.. 00000142
C.. INPUT TIME(HOUR) SPENT IN LANDING MODE. 00000143
C.. 00000144
  IF(DEFAULT(2).NE.0) 00000145
  IREAD(INPUT,25)(FLNDG(I),I=1,NACT) 00000146
  WRITE(OUTPUT,597)(FLNDG(I),I=1,NACT) 00000147
C.. 00000148
C.. INPUT TIME(HOUR) SPENT IN TAKE-OFF MODE. 00000149
C.. 00000150
  IF(DEFAULT(3).NE.0) 00000151
  IREAD(INPUT,25)(FTKOF(I),I=1,NACT) 00000152
  WRITE(OUTPUT,598)(FTKOF(I),I=1,NACT) 00000153
C.. 00000154
C.. INPUT THE NUMBER OF ENGINES USED WITH EACH AIRCRAFT TYPE. 00000155
C.. 00000156
  IF(DEFAULT(4).NE.0) 00000157
  IREAD(INPUT,5)(NGIN(I),I=1,NACT) 00000158
C.. 00000159
C.. INPUT THE ENGINE TYPE INDEX OF THE ABOVE ENGINES. 00000160
C.. 00000161
  IF(DEFAULT(5).NE.0) 00000162
  IREAD(INPUT,5)(INGN(I),I=1,NACT) 00000163

```

```

C..                                00000164
C.. INPUT FOR THE SPECIFIED POLLUTANT(S), THE EMISSION RATE(LB/HR) 00000165
C.. OF EACH AIRCRAFT ENGINE TYPE FOR THE FOLLOWING FOUR (4) MODES 00000166
C.. OF OPERATION: 1. TAXI, 2. IDLE, 3. LANDING, 4. TAKE-OFF. 00000167
      IF(DEFAULT(6).EQ.0) GO TO 446 00000168
C..                                00000169
      DO 445 I=1,NENT 00000170
      DO 445 J=1,4 00000171
445 READ(INPUT,3)(EMI(I,J,IJ(K)),K=1,NPT) 00000172
446 CONTINUE 00000173
      IS = 5 00000174
C..                                00000175
      IF(DEFAULT(6).EQ.0) GO TO 447 00000176
      IS = NENT 00000177
C..                                00000178
447 DO 448 I = 1,IS 00000179
      DO 448 J = 1,4 00000180
      WRITE(OUTPUT,150)(J,(EMI(I,J,IJ(K)),K=1,NPT)) 00000181
448 CONTINUE 00000182
C..                                00000183
C.. INPUT INITIAL DIMENSIONS OF RUNWAY WIDTH AND HEIGHT. 00000184
C..                                00000185
      IF(DEFAULT(7).NE.0) 00000186
      READ(INPUT,323) DSRW,HRW 00000187
      DSRW = DSRW/2.4 00000188
      HRW = HRW/1.2 00000189
      KL = 0 00000190
      CALL PSEUDO(DSRW,A,B,TX1,TY1,TZ1,CX,DY,JSTAB,HRW,KL) 00000191
      SUDDY = WS * TX1 00000192
      SUDLZ = WS * TZ1 00000193
C.. INPUT RUNWAY COORDINATES. 00000194
C..                                00000195
      READ(INPUT,1244) X1,Y1,Z1,X2,Y2,Z2 00000196
      WRITE(OUTPUT,9715) X1,Y1,Z1,X2,Y2,Z2 00000197
      Z1 = Z1/5280. 00000198
      Z2 = Z2/5280. 00000199
      RUNX = X2 00000200
      RUNY = Y2 00000201
C..                                00000202
C.. INPUT RUNWAY PARAMETERS: INITIAL AND FINAL VELOCITIES DURING 00000203
C.. ARRIVAL AND DEPARTURE, TAKE-OFF ROLL TIME, AND EXHAUST TAIL LENGTH. 00000204
C.. THESE VALUES WILL DEFAULT AS FOLLOWS* 00000205
C..      VA1 = RUNWAY-ARRIVAL INITIAL VELOCITY = 145 MILES/HOUR. 00000206
C..      VA2 = RUNWAY-ARRIVAL FINAL VELOCITY = 25 MILES/HOUR. 00000207
C..      VD1 = RUNWAY-DEPARTURE INITIAL VELOCITY= 0 MILES/HOUR. 00000208
C..      VD2 = RUNWAY-DEPARTURE FINAL VELOCITY = 180 MILES/HOUR. 00000209
C..      TIME = TAKE-OFF ROLL TIME = .01111 HOURS. 00000210
C..      TAIL = EXHAUST TAIL LENGTH = .8523 MILES. 00000211
C..                                00000212
      IF(DEFAULT(8).NE.0) 00000213
      READ(INPUT,1244) VA1,VA2,VD1,VD2,TIME,TAIL 00000214
      WRITE(OUTPUT,9721) VA1,VA2,VD1,VD2,TIME,TAIL 00000215
      IF(TAIL.LE.0) TAIL = 20./5280. 00000216
      VA12 = VA1*VA1 00000217
      VA22 = VA2*VA2 00000218

```



```

CALL PSEUDO(PSTW,A,B,TX2,TY2,TZ2,DX,DY,JSTAB,HTW,KL)
SUDQY = WS*TX2
SUDQZ = WS*TZ2
IADC = 0
DO 626 IIX = 1,NTXI
C... INPUT TAXIWAY LINE COORDINATES.
C
  READ(INPUT,1244) X1,Y1,Z1,X2,Y2,Z2
  WRITE(OUTPUT,9716) X1,Y1,Z1,X2,Y2,Z2
  Z1 = Z1/5280.
  Z2 = Z2/5280.
  XXSQ = (X1-X2)**2
  YYSQ = (Y1-Y2)**2
  DTXL = SQRT(XXSQ+YYSQ)
C
  FMTAXI = 0.0
C
  COMPUTE TAXI EMISSIONS
C
  DO 8413 II = 1,NPT
  J = IJ(II)
  DO 41 K = 1,NACT
  INENG = NAC(K) * NGIN(K)
  EMTX = INENG * EMI(INGN(K),1,J)
C...
C
  RT1 = 1/FIXII(K)
  FTL = 1/FTXID(K)
  FMTXII = FMTX*DTXL
  IF(ITX.EQ.1) EMTXI(J) = FMTXII*PT1 + EMTXI(J)
  IF(ITX.EQ.2) EMTXO(J) = FMTXII*FTL + EMTXO(J)
41 CONTINUE
  DO 8413 M = 1,NSR
  ZR = ZREFCP(M)/5280.
  CALL LINE(XREFCP(M),YREFCP(M),ZR,X1,Y1,Z1,X2,Y2,Z2,CUP)
  COUPP = CUP*CONVF/WS
  IF(ITX.EQ.1) EMTAXI = EMTXI(J)
  IF(ITX.EQ.2) EMTAXI = EMTXO(J)
  RECDAT(3,J,M) = RECDAT(3,J,M) + COUPP * EMTAXI
  RECDAT(4,J,M) = RECDAT(4,J,M) + COUPP * EMTAXI
8413 CONTINUE
826 CONTINUE
C
  OUTPUTD APRON QUEUING AS LINE SOURCES
C
C... INPUT INITIAL DIMENSIONS OF APRON WIDTH AND HEIGHT.
C
  IF(LEFALT(13).NE.0)
  LEFAL(INPUT,323) DSRA,HRA
  WRITE(OUTPUT,9719) DSKW,HRW,ESTW,HTW,DSRA,HRA
  DSRA = DSRA/2.4
  HRA = HRA/1.2
  KL = 0
  CALL PSEUDO(DSRA,A,B,TX3,TY3,TZ3,DX,DY,JSTAB,HRA,KL)
  SUDQY = WS*TX3

```

```

00000274
00000275
00000276
00000277
00000278
00000279
00000280
00000281
00000282
00000283
00000284
00000285
00000286
00000287
00000288
00000289
00000290
00000291
00000292
00000293
00000294
00000295
00000296
00000297
00000298
00000299
00000300
00000301
00000302
00000303
00000304
00000305
00000306
00000307
00000308
00000309
00000310
00000311
00000312
00000313
00000314
00000315
00000316
00000317
00000318
00000319
00000320
00000321
00000322
00000323
00000324
00000325
00000326
00000327
00000328

```


SUDGZ = WS*TZ3	00000329
EACT1 = 0.0	00000330
EACT2 = 0.0	00000331
IADC = 0	00000332
DC 43 I = 1, NACT	00000333
EFACT = NAC(I)	00000334
IKA(I) = .5*EFACT+.5	00000335
IKB(I) = EFACT-IKA(I)	00000336
EACT1 = EACT1 + IKA(I)	00000337
43 EACT2 = EACT2 + IKB(I)	00000338
RCT1 = (EACT1/180. + 1./60.)	00000339
RCT2 = (EACT2/180. + 1./60.)	00000340
C..	00000341
C.. INPLT AIRPORT APRON COORDINATES.	00000342
C	00000343
READ(INPUT,1244)(XA(N),YA(N),ZA(N),XB(N),YB(N),ZB(N),N=1,2)	00000344
DC 124 N=1,2	00000345
SQXY = (XA(N)-XB(N))**2 + (YA(N)-YB(N))**2	00000346
RTXY(N) = SQRT(SQXY)	00000347
ZA(N) = ZA(N)/5280.	00000348
ZB(N) = ZB(N)/5280.	00000349
124 CONTINUE	00000350
C	00000351
DC 827 L=1,2	00000352
DISP = 300./5280.	00000353
SN1 = 1.	00000354
SN2 = 1.	00000355
X1 = XA(L)	00000356
Y1 = YA(L)	00000357
Z1 = ZA(L)	00000358
X2 = XB(L)	00000359
Y2 = YB(L)	00000360
Z2 = ZB(L)	00000361
WRITE(OUTPUT,9717) X1,Y1,Z1,X2,Y2,Z2	00000362
IF(L.EQ.1) GO TO 820	00000363
CSI = DISP*(YB(L)-YA(L))/RTXY(L)	00000364
ETA = DISP*(XB(L)-XA(L))/RTXY(L)	00000365
CSI = ABS(CSI)	00000366
ETA = ABS(ETA)	00000367
XC = XB(L)-RUNX	00000368
YC = YB(L)-RUNY	00000369
IF(XC.NE.0) SN1 = XC/ABS(XC)	00000370
IF(YC.NE.0) SN2 = YC/ABS(YC)	00000371
X1 = X1 + SN1*CSI	00000372
Y1 = Y1 + SN2*ETA	00000373
X2 = X2 + SN1*CSI	00000374
Y2 = Y2 + SN2*ETA	00000375
820 CONTINUE	00000376
DC 823 M=1,NSR	00000377
CUP(M) = 0.0	00000378
ZR = ZFCP(M)/5280.	00000379
CALL LINE(XFCP(M),YFCP(M),ZR,X1,Y1,Z1,X2,Y2,Z2,CUP)	00000380
CUP(M) = CUP*CONVF/WS	00000381
823 CONTINUE	00000382
	00000383

```

      DC 8414 LL=1,NPT                                00000384
      J = IJ(LL)                                       00000385
      RWIDL(J,L) = 0.0                                00000386
      DC 44 K =1,NACT                                  00000387
      IF(L.EQ.1)                                       00000388
1    FMRIDL = NAC(K) * NGIN(K) * EMI(INGN(K),1,J) * PTXY(L)/FTXII(K) 00000389
      POT = (IKA(K)*ROT1 + IKR(K)*ROT2)               00000390
      IF(L.EQ.2) FMRIDL = NGIN(K) * EMI(INGN(K),2,J) * ROT 00000391
44  RWIDL(J,L) = FMRIDL + RWIDL(J,L)                 00000392
C                                                    00000393
      DC 8414 M=1,NSH                                  00000394
      RECDAT(3,J,M) = RECDAT(3,J,M) + COUP(M)*RWIDL(J,L) 00000395
      RECDAT(4,J,M) = RECDAT(4,J,M) + COUP(M)*RWIDL(J,L) 00000396
8414 CONTINUE                                         00000397
827 CONTINUE                                         00000398
C                                                    00000399
C          ACCESS VEHICLE ROADWAYS AS LINE SOURCES 00000400
C                                                    00000401
      IF(NAVR.EQ.0) GO TO 301                          00000402
C... INPUT AUTOMOBILE EMISSION FACTORS(GM/KM)        00000403
C                                                    00000404
      IF(DEFAULT(14).NE.0)                             00000405
1    READ(INPUT,3)(EFUH(IJ(I)),I=1,NPT)              00000406
      IF(DEFAULT(15).NE.0)                             00000407
1    READ(INPUT,3)(EFUL(IJ(I)),I=1,NPT)              00000408
      WRITE(OUTPUT,773)(EFUH(IJ(I)),I=1,NPT)          00000409
      WRITE(OUTPUT,774)(EFUL(IJ(I)),I=1,NPT)          00000410
C                                                    00000411
C... INPUT INITIAL DIMENSIONS OF ROADWAY WIDTH AND HEIGHT. 00000412
      IF(DEFAULT(16).NE.0)                             00000413
1    READ(INPUT,323) DSAR,HAF                          00000414
      DSAR = DSAR/2.4                                  00000415
      HAF = HAF/1.2                                    00000416
      KL = 0                                           00000417
      CALL PSEUDO(DSAR,A,B,TXA,TYA,TZA,DX,DY,JSTAB,HAF,KL) 00000418
      SLDY = WS * TXA                                  00000419
      SLDZ = WS * TZA                                  00000420
C                                                    00000421
C... INPUT ACCESS VEHICLE ROADWAY COORDINATES.       00000422
C                                                    00000423
      WRITE(OUTPUT,9735)                               00000424
      DC 828 N=1,NAVR                                  00000425
      READ(INPUT,311) X1,Y1,Z1,X2,Y2,Z2,VNOCN,IFS    00000426
      WRITE(OUTPUT,9725) X1,Y1,Z1,X2,Y2,Z2,VNOCN,IFS  00000427
      Z1 = Z1/5280.                                    00000428
      Z2 = Z2/5280.                                    00000429
      XSQ = (X1-X2)**2                                  00000430
      YSQ = (Y1-Y2)**2                                  00000431
      TVL = SQRT(XSQ+YSQ)                               00000432
      TABC = 0                                          00000433
C                                                    00000434
      DC 824 M=1,NSR                                    00000435
      ZR = ZRC(P(M))/5280.                             00000436
      CALL LINE(XRC(P(M)),YRC(P(M)),ZR,X1,Y1,Z1,X2,Y2,Z2,CUP) 00000437
      CUP(P(M)) = CUP*CONVF/WS                        00000438

```

AD-A061 854

ARGONNE NATIONAL LAB ILL

F/G 1/5

AIRPORT VICINITY AIR POLLUTION MODEL ABBREVIATED VERSION USER'S--ETC(U)

SEP 78 L A CONLEY, D M ROTE

DOT-FA71WA1-223

UNCLASSIFIED

FAA-RD-78-111

NL

2 OF 2

AD
A061854



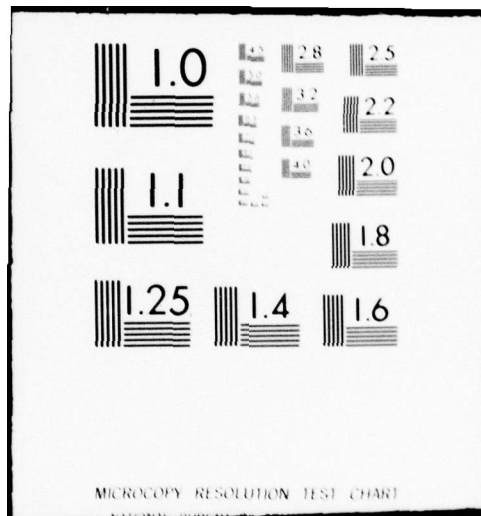
END

DATE

FILMED

2-79

DDC



```

      824 CONTINUE
C
      DO 8415 I=1,NPT
        J = IJ(I)
        EFUEL = EFUL(J)
        IF(IFS.EQ.1) EFUEL = EFUL(J)
        ALSEF(N,J) = VNOON*DVL *EFUEL *1.609/453.59
C
      DO 8415 M=1,NSR
        RECDAT(2,J,M) = RECDAT(2,J,M) + COUP(M)*ALSEF(N,J)
        RECDAT(4,J,M) = RECDAT(4,J,M) + COUP(M)*ALSEF(N,J)
      8415 CONTINUE
      828 CONTINUE
      301 CONTINUE
      IF(NACT.EQ.0) GO TO 3402
C
C          TERMINAL AREA AS AREA SOURCE
C.. ATTRIBUTABLE EMISSIONS ARE THE FOLLOWING:
C      1. SERVICE VEHICLES (14 TYPES)
C      2. AUXILIARY POWER UNITS
C      3. AIRCRAFT WHILE IN THE INBOUND TAXI MODE
C      4. AIRCRAFT WHILE ENGINE THROTTLE IS SET TO IDLE
C
      TN = (273.+5.*(TEMP-32.)/9.)/273.
      NRECPY = NSF
      ZRECPG = HTAFRG
      SCTUPI = SQ2PI
C
      NSRC = NANA + NACA
      IF(NSRC.EQ.0) GO TO 3402
C
C.. INPUT AREA SOURCE COORDINATES AND THE INITIAL DIMENSIONS OF WIDTH
C.. AND HEIGHT.
C
      IF(NACA.EQ.0) GO TO 116
      READ(INPUT,441) XS(1),YS(1),STKH(1),WIT(1)
      WIT(1) = WIT(1)/2.0
C
C..1. SERVICE VEHICLES IN THE TERMINAL AREA
C
C.. INPUT POLLUTANT EMISSION FACTORS FOR BOTH DIESEL(GM/GAL) AND
C.. GASOLINE(GM/MI) ENGINES.
C
      IF(DEFAULT(17).NE.0)
        IREAD(INPUT,3)(EFD(IJ(I)),I=1,NPT)
      IF(DEFAULT(18).NE.0)
        IREAD(INPUT,3)(EFG(IJ(I)),I=1,NPT)
      WRITE(OUTPUT,574)(NAME(IJ(I)),EFD(IJ(I)),I=1,NPT)
      WRITE(OUTPUT,575)(NAME(IJ(I)),EFG(IJ(I)),I=1,NPT)
      574 FORMAT(T5,'POLLUTANT EMISSION FACTORS(DIESEL ENGINE) GM/GAL',/,
        1(T5,A4,'= ',F10.2))
      575 FORMAT(T5,'POLLUTANT EMISSION FACTORS(GASOLINE ENGINE) GM/MI',/,
        1(T5,A4,'= ',F10.2))
      DO 443 I = 1,NSVR

```

```

00000439
00000440
00000441
00000442
00000443
00000444
00000445
00000446
00000447
00000448
00000449
00000450
00000451
00000452
00000453
00000454
00000455
00000456
00000457
00000458
00000459
00000460
00000461
00000462
00000463
00000464
00000465
00000466
00000467
00000468
00000469
00000470
00000471
00000472
00000473
00000474
00000475
00000476
00000477
00000478
00000479
00000480
00000481
00000482
00000483
00000484
00000485
00000486
00000487
00000488
00000489
00000490
00000491
00000492
00000493

```



```

      SRVHR(1) = 0.0
C
C.. INPUT SERVICE VEHICLE OPERATION TIME (MIN)
C
      IF(DEFAULT(19).NE.0)
      IREAD(INPUT,25)(SRVTIM(J,1),J=1,NACT)
C
      DO 410 J=1,NACT
410  SRVHR(1) = SRVHR(1) + SRVTIM(J,1)*NAC(J)/60.
444  CONTINUE
      WRITE(OUTPUT,772)
      DO 411 I=1,14
      WRITE(OUTPUT,415) SRNAME(1),(SRVTIM(J,1),J=1,NACT)
411  CONTINUE
C
C
      DIESEL = 0.0
      GSOLN = 0.0
      IUNIT = 1
      CALL GTIME(1,SRVHR,IUNIT,PLLTNT,DIESEL,GSOLN,NPT)
C
C..2. AUXILIARY POWER UNITS IN THE TERMINAL AREA
C
C.. INPUT APU USE FLAGS AND APU POLLUTANT EMISSION RATE.
C
      IF(DEFAULT(20).NE.0)
      IREAD(INPUT,5)(KAPU(I),I=1,NACT)
      IF(DEFAULT(21).NE.0)
      IREAD(INPUT,3)(APU(IJ(1)),I=1,NPT)
C
C..3. EMISSIONS FROM AIRCRAFT WHILE IN THE INBOUND TAXI MODE
C...
C
C..4. EMISSIONS FROM AIRCRAFT WHILE ENGINE THROTTLE IS SET TO IDLE.
C
C.. INPUT TIME(HOURS) SPENT IN IDLE MODE, AND GATE OCCUPANCY TIME(MIN).
C
      IF(DEFAULT(22).NE.0)
      IREAD(INPUT,25)(FIDLE(I),I=1,NACT)
      WRITE(OUTPUT,595)(FIDLE(I),I=1,NACT)
      IF(DEFAULT(23).NE.0)
      IREAD(INPUT,25)(TGND(I),I=1,NACT)
C
      DO 111 IL=1,NPT
      I = IJ(IL)
      IMPLNT = 2*WIT(1)
      DO 112 K=1,NACT
      TGT = TGND(K)/60.
      FMI(J) = NAC(K)*NGIN(K)*FIDLE(K)*EMI(INGN(K),2,J) + FMI(J)
      TERM(J) = NAC(K)*NGIN(K)*EMI(INGN(K),1,J)*TMPLNT/FTAXI(K)+TERM(J)
      EAPU(J) = APU(J)*NAC(K)*GTOT*KAPU(K) + EAPU(J)
112  CONTINUE
      TOTAL EMISSIONS IN THE TERMINAL AREA.. EMIT(J,1)

```

```

00000494
00000495
00000496
00000497
00000498
00000499
00000500
00000501
00000502
00000503
00000504
00000505
00000506
00000507
00000508
00000509
00000510
00000511
00000512
00000513
00000514
00000515
00000516
00000517
00000518
00000519
00000520
00000521
00000522
00000523
00000524
00000525
00000526
00000527
00000528
00000529
00000530
00000531
00000532
00000533
00000534
00000535
00000536
00000537
00000538
00000539
00000540
00000541
00000542
00000543
00000544
00000545
00000546
00000547
00000548

```

```

111 EMIT(J,1) = PLTNT(J) + TERM(J) + EMID(J) + EAPU(J)      00000549
116 CONTINUE      00000550
    IF(NANA.EQ.0) GO TO 115      00000551
C      00000552
C.. INPUT AIRPORT NON-AIRCRAFT AREA SOURCE COORDINATES, THE INITIAL      00000553
C.. DIMENSIONS OF WIDTH AND HEIGHT, AND THE POLLUTANT EMISSION RATE.      00000554
C      00000555
    N = 2      00000556
    IF(NACA.EQ.0) N=1      00000557
    READ(INPUT,441) XS(N),YS(N),STKH(N),WIT(N)      00000558
    WRITE(OUTPUT,9714) XS(N),YS(N),STKH(N),WIT(N)      00000559
    READ(INPUT,3)(EMIT(IJ(J),R),J=1,NPT)      00000560
    WIT(N) = WIT(N)/2.0      00000561
C      00000562
115 CONTINUE      00000563
    DO 211 N=1,NSRC      00000564
      CWS(N)=XS(N)*COSWD-YS(N)*SINWD      00000565
      DWS(N)=-XS(N)*SINWD-YS(N)*COSWD      00000566
211    DO 212 N=1,NRECPT      00000567
      DWR(N)=-XRECP(N)*SINWD-YRECP(N)*COSWD      00000568
      CWR(N)=XRECP(N)*COSWD-YRECP(N)*SINWD      00000569
212 CONTINUE      00000570
    IF(NSFC.EQ.C) GO TO 3402      00000571
    DO 2402 NS=1,NSRC      00000572
      HEFF(NS)=STKH(NS)      00000573
      KSTAB(NS)=0      00000574
      IF(HEFF(NS).GT.HLID)KSTAB(NS)=1      00000575
      WSMO=WS      00000576
      DLZ=2.*STKH(NS)/(2.4*5280.)      00000577
      DSS=2.*WIT(NS)/2.4      00000578
      KL=0      00000579
      AMOD=A      00000580
      BMOD=B      00000581
      CALL PSEUDO(ESS,AMOD,BMOD,TX,TY,TZ,CX,DY,JSTAB,DLZ,KL)      00000582
      KSTABS=KSTAB(NS)      00000583
      HEFFS=HEFF(NS)      00000584
      DELY=DSS*2.4      00000585
      DELZ=DLZ*2.4      00000586
      TXT=TX      00000587
      TYT=TY      00000588
      TZT=TZ      00000589
      HINT=ZRECPG      00000590
      DO 2409 NR=1,NRECPT      00000591
        STWIT=WIT(NS)      00000592
        DW=DWR(NR)-DWS(NS)      00000593
        CW=CWR(NR)-CWS(NS)      00000594
        HRECPT = ZRECP(NR)      00000595
        PFA=1.      00000596
        IF(DW.LE.-WIT(NS)) GO TO 2409      00000597
        NRFLAG=0      00000598
        IRACK=0      00000599
        IF(DW.LE.WIT(NS)) GO TO 231      00000600
        IF((DWR(NR)-XL).GE.(DWS(NS)+WIT(NS))) GO TO 241      00000601
231    IF((DWR(NR)-XL).LT.(DWS(NS)-WIT(NS))) GO TO 232      00000602
        PFA=(CW-XL+WIT(NS))/(2.*WIT(NS))      00000603

```

```

DWS=(CWS(NS)-WIT(NS))*(CWR(NR)-XL)/2.
KW=K1(NR)-DWSS
K11(NS)=((CWR(NR)-XL)-(CWS(NS)-WIT(NS)))/2.
BACK=1
GOTO 241
37 NRFLAG=1
PEA=1.
PERFORM AREA SOURCE DISPERSION CALCULATIONS BY FUNCTION
"TRAN".
241 TEM=TRAN(NS,KSTARS,HFFS,NRFLAG,BACK)*CEMVE
K11(NS)=STW11
TEM=TEM*PEA
IF (40 LL = 1,APT
  K = 1J(LL)
  IXPT = 1
  IF (NACA,0,0) IXPT = 2
  IF (NS,0,0) IXPT = NS
  FOR EACH RECEIPTOR NR, SUM OVER ALL CONTRIBUTIONS FROM
  AREA SOURCES.
  RECAT(IXPT,KD,NR)=RECAT(IXPT,K1,NR)+EMIT(KD,NS)*TEM
  RECAT(4,KD,NR)=RECAT(4,KD,NR)+EMIT(KD,NS)*TEM
240 CONTINUE
  IF (IS,0,0) GO TO 232
230 CONTINUE
220 CONTINUE
210 CONTINUE
200 CONTINUE
190 CONTINUE
180 CONTINUE
170 CONTINUE
160 CONTINUE
150 CONTINUE
140 CONTINUE
130 CONTINUE
120 CONTINUE
110 CONTINUE
100 CONTINUE
90 CONTINUE
80 CONTINUE
70 CONTINUE
60 CONTINUE
50 CONTINUE
40 CONTINUE
30 CONTINUE
20 CONTINUE
10 CONTINUE
0 CONTINUE

```



```

13 FORMAT(1H+,T80,'*',/,1X,'* TERM. AREA TAXI ',4X,5(F10.1)) 00000659
C 00000660
WRITE(OUTPUT,15)(FMID(IJ(J)),J=1,NPT) 00000661
15 FORMAT(1H+,T80,'*',/,1X,'* TERM AREA ENG. IDLE',3X,5(F10.1)) 00000662
WRITE(OUTPUT,29)(EMIT(IJ(J),1),J=1,NPT) 00000663
29 FORMAT(1H+,T80,'*',/,1X,'* AIRCRAFT AREA',9X,5(F10.1)) 00000664
WRITE(OUTPUT,30)(EMIT(IJ(J),2),J=1,NPT) 00000665
30 FORMAT(1H+,T80,'*',/,1X,'* NON-AIRCRAFT AREA',5X,5(F10.1)) 00000666
32 FORMAT(1H+,T80,'*',/,1X,'* SERVICE VEHICLE',7X,5(F10.1)) 00000667
IF(NAVR.EQ.0) GO TO 1001 00000668
WRITE(6,33) 00000669
33 FORMAT(1H+,T80,'*',/,1X,'* ACCESS VEHICLE') 00000670
DO 37 N=1,NAVR 00000671
WRITE(OUTPUT,35) N,(ALF(N,IJ(J)),J=1,NPT) 00000672
35 FORMAT(1H+,T80,'*',/,1X,'*',16X,13,4X,5(F10.1)) 00000673
37 CONTINUE 00000674
WRITE(OUTPUT,38) 00000675
38 FORMAT(1H+,T80,'*',/,1X,79('**'),/) 00000676
WRITE(OUTPUT,1000) 00000677
1000 FORMAT(1H1) 00000678
1001 CONTINUE 00000679
DO 16 N=1,NSR 00000680
WRITE(OUTPUT,81) NRUSED(N),XRECP(N),YRECP(N),(NAUT(IJ(J)),J=1,NPT) 00000681
81 FORMAT(1X,79('**'),/,1X,'*',T80,'*',/, 00000682
11X,'*',9X,'POLLUTANT CONCENTRATIONS : N/CM=MICROGRAMS PER CUBIC MFC00000683
-TER',T80,'*',/,1X,'*',T80, 00000684
2'**,/,1X,'*',19X,'RECEPTOR',14,T80,'*',/,1X,'*',T80,'*',/,1X 00000685
3'**,19X,'COORDINATES ('',F7.3,'',F7.3,'')',T80,'*',/,2(1X,'*',T800000686
4'**,/,1X,'*',31X,5(A6,2X)) 00000687
WRITE(OUTPUT,83)(RECDAT(1,IJ(L),N),L=1,NPT) 00000688
82 FORMAT(1H+,T80,'*',/,1X,'* AIRCRAFT LINE ',11X,5(F10.3)) 00000689
WRITE(OUTPUT,84)(RECDAT(2,IJ(L),N),L=1,NPT) 00000690
83 FORMAT(1H+,T80,'*',/,1X,'* AIRCRAFT AREA ',11X,5(F10.3)) 00000691
WRITE(OUTPUT,82)(RECDAT(3,IJ(L),N),L=1,NPT) 00000692
84 FORMAT(1H+,T80,'*',/,1X,'* NON-AIRCRAFT AREA-LINES',2X,5(F10.3)) 00000693
WRITE(OUTPUT,85)(RECDAT(4,IJ(L),N),L=1,NPT) 00000694
85 FORMAT(1H+,T80,'*',/,1X,'*',12X,'TOTAL',9X,5(F10.3)) 00000695
WRITE(OUTPUT,38) 00000696
16 CONTINUE 00000697
C..... INPUT FORMATS... 00000698
C 00000699
4711 FORMAT(12,3F8.0) 00000700
12 FORMAT(15X,6I5) 00000701
5 FORMAT(5X,15I5) 00000702
1 FORMAT(6X,23I3) 00000703
25 FORMAT(5X,15F5.0) 00000704
3 FORMAT(15X,5F10.0) 00000705
323 FORMAT(15X,2F10.0) 00000706
1244 FORMAT(15X,6F10.0) 00000707
311 FORMAT(10X,6F10.0,F8.0,I2) 00000708
415 FORMAT(1X,A6,5X,10F5.1) 00000709
441 FORMAT(15X,4F10.0) 00000710
C 00000711
31 FORMAT(1X,'POLLUTANT CHOICE ',10A4) 00000712
34 FORMAT(1X,'AIRPORT PARAMETERS:',/, 00000713

```

THIS PAGE IS BEST QUALITY PRACTICABLE
FROM COPY FURNISHED TO DDQ


```

BLOCK DATA
INTEGER DEFAULT(23)
REAL*8 SRNAME(14)
COMMON/SERVHL/SRNAME
00000764
00000765
00000766
00000767
00000768
00000769
COMMON/DEFLT/NAC(10),FLNDG(10),FTKOF(10),NGIN(10),INGN(10),
1EMI(5,4,5),DSRW,HRW, FTAXI(10),
2FTXII(10),FTXIO(10),DSTW,HTW,DSKA,HRA,FFUH(5),FFUL(5),CSAR,HAR,
3SRVTIM(10,14),KAPU(10),APU(5),FIDLE(10),TGND(10),DEFAULT
00000770
00000771
00000772
00000773
COMMON/FEHL/FEF(5),FFG(5)
00000774
COMMON/LN/DL,XW1,YW1,ZW1,XW2,YW2,ZW2,COEF1,COEF2,VA1,VA2,VD1,VD2,
-C,TIME,VA12,VA22,VD12,VD22,WS2,WSC,JAD,SNAN,CSAN,V1,V2,V12,V22,
-TAIL,VS,RR,SP
00000775
00000776
00000777
00000778
00000779
00000780
00000781
00000782
00000783
00000784
00000785
00000786
00000787
00000788
00000789
00000790
00000791
00000792
00000793
00000794
00000795
00000796
00000797
00000798
00000799
00000800
00000801
00000802
00000803
00000804
00000805
00000806
00000807
00000808
00000809
00000810
00000811
00000812
00000813
00000814
00000815
00000816
DATA NAC/10*10/
DATA FLNDG/6*.0153,.011,.0153,.011,.011/
DATA FTKOF/10*.0111/
DATA NGIN/3,9*2/
DATA INGN/1,1,1,3,4,3,2,3,2,5/
DATA EMI/37,.3,53,15,.60,.11,41,37,.3,53,15,.60,.11,41,
-25.6,2.58,10.1,45.6,11.41,6...39,2,.14,.72,52,9...88,6,.66...38
-,9...88,6,.66...38,5.6...24,3.8,40.3,.38,.4,.05,.4,0.0,1.66,
-2...96,2.0,1...01,2...96,2...01,36.3,1.69,8...42,1...01,
-133.3,3.64,23...153...23,.5,.1,.1,.04,.06,.5,.1,.1,.04,.06,
-6.8,.38,.3,.3,.06,21...62,.6,.8,12,.9,.5,.5,.6,.01,.9,.5,.5,
-.6,.01,3.2,.5,.9,2.2,.01,8.6,1.9,1.9,6.2,.07/
DATA DSRW,HRW/.03,.002/
DATA VA1,VA2,VD1,VD2,TIME,TAIL/145,.25,.0,0,180...0111,.08525/
DATA FTAXI/10*10./
DATA FTXII/10*15./
DATA FTXIO/10*12./
DATA DSTW,HTW/.03,.002/
DATA DSKA,HRA/.095,.002/
DATA FFUH/32.36,4.75,3.46,.19,.11/
DATA FFUL/70.18,8.62,2.86,.19,.11/
DATA CSAR,HAR/.0095,.001/
DATA FEF/126.6,21.9,185.82,5.9,0.0/
DATA FFG/138.81,21.35,9.32,.85,0.0/
DATA SRVTIM/66,.48,.85,.55,.50,.50,.4*0.0,28,.15,.30,.0,0,
- 25,.25,.4*0.0,6,.9*0.0,12,.0,.15,.7*0.0,
- 15,.15,.15,.10,.10,.10,.5,.5,.5,.0,0,
- 0,.10,.0,.10,.10,.10,.5,.5,.5,.0,0,
- 17,.17,.20,.10,.10,.10,.0,0,.0,.0,0,
- 20,.15,.15,.10,.20,.20,.10,.10,.0,0,
- 10,.5,.5,.5,.5,.5,.44*0.3,.9*0./
NAME THE 14 SERVICE VEHICLE TYPES.

```

C-16

DATA SNAME/'TRACTOR ','BELT LRD','CONT LDR','CAR SER ','LAV TRK '00000817
-,'WAT TRK ','FOOD SRV','FUEL TRK','TOW TCTR','CONDTR ','AIR STRT'00000818
-,'GPU FRNT','GPU REAR','TRANSPTR'/00000819
DATA KAPU/4*1.6*0/00000820
DATA APU/2.82,.11,1.24,0.,0./00000821
DATA FIDLE/10*.033/00000822
DATA TGND/10*52./00000823
DATA CFALT/23*0/00000824
END00000825
00000826

```

SUBROUTINE GASDIN(XMIHR,XMIGAL,GAL,XMIHF,PLLTNT,NPLTS,IUNIT)
C-----XMIHR=ASSUMED AVERAGE VEHICLE SPEED
C-----XMIGAL=ASSUMED MILES PER GALLON
C-----GAL = GALLONS OF FUEL CONSUMED
C-----IF DATA GIVEN IN VEHICLE MILES, GAL MUST BE SET EQUAL TO 0.0
C-----XMILE=TOTAL MILES; SET EQUAL TO 0.0 IF USING GALLONS
C-----XPT,XCC,ETC. ARE THE EMISSIONS IN UNITS OF POUNDS OR GRAMS FOR
C-----PARTICULATES, CARBON MONOXIDE, HYDROCARBONS, ETC.
C-----IUNIT = 0 MEANS EMISSIONS IN GRAMS ELSE EMISSIONS IN POUNDS.
C
C      DIMENSION PLLTNT(5)
C      COMMON/PC/L/NPT,JJ(5)
C      COMMON/FUEL/EF(5),EF(5)
C      *****
C      GASOLINE ENGINE POWERED MOTOR VEHICLE EMISSIONS ARE COMPUTED ON
C      THE BASIS OF STANDARD EMISSION FACTORS AND ASSUMED SPEED
C      DEPENDENCE.
C      *****
C
C      SPCC=12.5*(XMIHR)**(-0.845)
C      SPHC=7.0*(XMIHR)**(-0.649)
C      SPNC=1.0+0.01262*(XMIHR-19.6)
C      A=XMIGAL*GAL
C      IF(GAL.EQ.0.0) A=XMILE*XMIGAL/12.5
C      DO 4 J=1,NPLTS
C      I = JJ(J)
C      IF(I.EQ.4) FACT = A*EF(4)
C      IF(I.EQ.3) FACT = A*EF(3)*SPNC
C      IF(I.EQ.1) FACT = A*EF(1)*SPCC
C      IF(I.EQ.2) FACT = A*EF(2)*SPHC
C      PLLTNT(I) = FACT
C      IF(IUNIT.NE.0) PLLTNT(I) = FACT/454.
C
C      CONTINUE
C      RETURN
C      END

```

```

FUNCTION CAVL(XR,YR,ZR)
COMMON/LN/DL,XW1,YW1,ZW1,XW2,YW2,ZW2,COEF1,COEF2,VA1,VA2,VD1,VD2,
-S,TIME,VA12,VA22,VD12,VD22,WS2,WSC,IAD,SNAN,CSAN,V1,V2,V12,V22,
- TAIL,VS,RR,SP
COMMON/MET/WS,W0,JSTAR,HLID,TEMP,XZ,SUD0Y,SUD0Z
C*****
C CALCULATION OF POLLUTANT CONCENTRATION DUE TO FINITE LINE SOURCE.
C*****
ISUB=0
NSUB=0
ISAC=0
CRAR=0.
CAN=0.7071
RMIN=30./5280.
HLEIM=HLID/5280.
C INTRODUCE A GENERAL SET OF NOTATION SO THAT SAME DISPERSION CALCULAT
C CAN BE USED FOR SMALL-ANGLE CASE WHERE LINE IS FURTHER SEGMENTED.
X1=XW1
Y1=YW1
Z1=ZW1
X2=XW2
Y2=YW2
Z2=ZW2
IF(Z1.GE.HLIDM) GO TO 600
IF(Z2.GT.HLIDM) GO TO 11
GO TO 5
11 X2=X1+(X2-X1)*(HLIDM-Z1)/(Z2-Z1)
Y2=Y1+(Y2-Y1)*(HLIDM-Z1)/(Z2-Z1)
Z2=HLIDM
5 DLXY=(X2-X1)**2+(Y2-Y1)**2
DL1=SQRT(DLXY)
IF (DL1.EQ.0.AND.Z1.EQ.Z2)GO TO 600
DLXYZ=DLXY+(Z2-Z1)**2
DLN=SQRT(DLXYZ)
IF (ISUB.NE.0) GO TO 6
DLRS=DLN
CSTH=DL1/DLN
SATH=(Z2-Z1)/DLN
PROJL=Y2-Y1
IF (ABS(PROJL).LT.1.E-20)PROJL=0.
SNFI=PROJL/DL1
ASNF=ABS(SNFI)
6 CONTINUE
IF (Y1.GT.Y2) GO TO 1
XF=X2
YF=Y2
XL=X1
YL=Y1
GO TO 2
1 XF=X1
YF=Y1
XL=X2
YL=Y2

```


2 CONTINUE	00000915
C TEST RECEPTOR LOCATION RELATIVE TO LINE SOURCE AND BRANCH.	00000916
IF (X1-X2) 27,28,28	00000917
27 XMAX=X2	00000918
XMIN=X1	00000919
GO TO 29	00000920
28 XMAX=X1	00000921
XMIN=X2	00000922
29 IF((XMIN-XF).GE..001) GO TO 500	00000923
XFAR=XF-XMIN	00000924
FWDA=XFAR+SUDGY	00000925
DWDB=XFAR+SUDGZ	00000926
TF(WDA,LF,0.,DR,DWDB,LE,0.) GO TO 500	00000927
TFAR=FWDA/WS	00000928
TFBR=FWDB/WS	00000929
SIGF=SIGY(JSTAB,TFAR)	00000930
SIGZ=SIGZ(JSTAB,TFBR)	00000931
APRO=ABS(PROJL)	00000932
IF(X1.GT.X2) GO TO 21	00000933
XA=X2	00000934
YA=Y2	00000935
ZA=Z2	00000936
XH=X1	00000937
YH=Y1	00000938
ZP=Z1	00000939
GO TO 22	00000940
21 XA=X1	00000941
YA=Y1	00000942
ZA=Z1	00000943
XH=X2	00000944
YH=Y2	00000945
ZP=Z2	00000946
22 CCNTINUE	00000947
IF(ISAC.EQ.1) GO TO 4	00000948
IF(YP.GT.(YH+4.*SIGF)) GO TO 500	00000949
IF(YR.LT.(YL-4.*SIGF)) GO TO 500	00000950
IF(ZP.GT.(Z2+4.*SIGFZ)) GO TO 500	00000951
IF(ZR.LT.(Z1-4.*SIGFZ)) GO TO 500	00000952
C GO TO 3 IF ANGLE IS SMALL	00000953
IF (ASNE .LT. CAN .AND. ABS(SNTH) .LT. CAN) GO TO 3	00000954
IF(YP.GT.(YH+3.*SIGF)) GO TO 500	00000955
IF(YR.LT.(YL-3.*SIGF)) GO TO 500	00000956
IF(ZP.GT.(Z2+3.*SIGFZ)) GO TO 500	00000957
IF(ZR.LT.(Z1-3.*SIGFZ)) GO TO 500	00000958
X=X1+(YH-Y1)*(X2-X1)/(Y2-Y1)	00000959
IF(X.LT.XH) GO TO 333	00000960
IF(X.GT.XA) GO TO 33	00000961
Y=YH	00000962
GO TO 4	00000963
C SELECT X,Y VALUES ON LINE FOR SMALL ANGLE CASE	00000964
3 X=XF	00000965
IF(XH.GT.XA) X=XA	00000966
Y=Y1+(X-X1)*(Y2-Y1)/(X2-X1)	00000967
ISAC=1	00000968
Z1=Z1+(X-X1)*(Z2-Z1)/(X2-X1)	00000969

X1=X	00000970
Y1=Y	00000971
X2=XB	00000972
Y2=YB	00000973
Z2=ZB	00000974
X=0.5*(X1+X2)	00000975
Y=0.5*(Y1+Y2)	00000976
GO TO 5	00000977
33 X=XA	00000978
Y=YA	00000979
GO TO 4	00000980
333 X=XB	00000981
Y=YB	00000982
4 DWD=XR-X	00000983
DWD1=DWD	00000984
IF (ISAC.EQ.1) DWD1=XR-X1	00000985
IF (ISAC.EQ.1.AND.NSUB.LE.1) DWD=DWD1	00000986
DWDY1=DWD1+SUDDY	00000987
DWDY=(DWD+SUDCY	00000988
DWDZ=(DWD+SUDCZ	00000989
IF (DWDY.LE.C..OR.DWDZ.LE.0..OR.DWDY1.LE.0.) GO TO 500	00000990
IF (X1.EQ.X2) GO TO 44	00000991
Z=Z1+(X-X1)*(Z2-Z1)/(X2-X1)	00000992
GO TO 444	00000993
44 Z=Z1+(Y-Y1)*(Z2-Z1)/(Y2-Y1)	00000994
444 CONTINUE	00000995
C COMPUTE STANDARD DEVIATIONS.	00000996
THR=WDY/WS	00000997
THR=WDZ/WS	00000998
THR1=WDY1/WS	00000999
SIGH1=SIGY(JSTAB,THR)	00010000
ELEM=AMAX1(0.2*DWDY1,SIGH1)	00010001
IF (IAE.NE.0) ISAC=1	00010002
IF (ISAC.EQ.1) ELEM=.1*ELEM	00010003
IF (ELEM.LT.EMIN) ELEM=EMIN	00010004
C BRANCH IF ANGLE IS SMALL AND LINE SOURCE IS LONG.	00010005
IF (IAE.NE.0.AND.DL1.GT.(1.5*ELEM)) GO TO 55	00010006
IF (ASNF.LT.CAN.AND.DL1.GT.(1.5*ELEM)) GO TO 55	00010007
SIGH=SIGY(JSTAB,THR)	00010008
SIGV=SIGZ(JSTAB,THR)	00010009
FNH=1.4142*SIGH	00010010
DENZ=1.4142*SIGV	00010011
IF (ASNF.LT.0.1.AND.(ABS(SNTH)).LT.0.1) GO TO 45	00010012
GO TO 445	00010013
45 ARGZ1=-(ZR-Z1)**2/DENZ**2	00010014
ARGZ2=-(ZR+Z1)**2/DENZ**2	00010015
GO TO 446	00010016
445 CONTINUE	00010017
ARG=CSTH**2*SNFI**2*SIGV**2+SNTH**2*SIGH**2	00010018
ARG=SQRT(ARG)	00010019
A=ARG/(1.4142*SIGH*SIGV)	00010020
AL=ELN*A	00010021
ARG1=(YR-Y1)*CSTH*SNFI*SIGV**2	00010022
ARGZ1=(ZR-Z1)*SNTH*SIGH**2	00010023
ARGZ2=-(ZR+Z1)*SNTH*SIGH**2	00010024

```

BA1=-(ARG1+ARG21)/(1.4142*SIGH*SIGV*PARG)
BA2=-(ARG1+ARG22)/(1.4142*SIGH*SIGV*PARG)
ARGY1=AL+BA1
ARGY2=AL+BA2
C1=(YR-Y1)**2/DENH**2+(ZF-Z1)**2/DENZ**2
C2=(YR-Y1)**2/DENH**2+(ZR+Z1)**2/DENZ**2
ARGZ1=BA1**2-C1
ARGZ2=BA2**2-C2
446 IF(ARGZ1.LT.-10..AND.ARGZ2.LT.-10.) GO TO 500
    IF(ARGZ1.LT.-10.)GOTO 2411
    IF(ARGZ2.LT.-10.)GOTO 2412
    IF(DWD.GT.XZ) GO TO 100
    FAC1=EXP(ARGZ1)
    FAC2=EXP(ARGZ2)
    GOTO 2414
2411 FAC1=C
    FAC2=EXP(ARGZ2)
    GOTO 2414
2412 FAC2=C
    FAC1=EXP(ARGZ1)
2414 CONTINUE
39 CONTINUE
C GET POLLUTANT DENSITY AND ITS GRADIENT(If ANY).
C MODEL ASSUMES CONSTANT ACCELERATION (OR DE-ACCEL.) AND EMISSION CN RU
C LANDING AND TAKE-OFF.
    XSI2=(X-XW1)**2+(Y-YW1)**2+(Z-ZW1)**2
    XSI=SQRT(XSI2)
    IF(X*XW2.LT.0.OR.Y*YW2.LT.0.OR.Z*ZW2.LT.0) XSI=-XSI
    QL = 1./QL
    IF (IAD.NE. 0) CALL QMOL(XSI,QL)
C BRANCH IF ANGLE IS SMALL
    IF(ASNF.LT.0.1.AND.(ABS(SNTH)).LT.0.1) GO TO 50
    FJ1=FAC1*(ERF(ARGY1)-ERF(BA1))
    FJ2=FAC2*(ERF(ARGY2)-ERF(BA2))
    CBARQ=CBAR
    CBAR=(CBAR+0.35355*CBFF1*QL*(FJ1+FJ2))/(A*SIGH*SIGV)
    IF (CBARQ.EQ.0) GO TO 49
    IF(ABS((CBARQ-CBAR)/CBAR).LE..00010) GO TO 600
    IF(1BUG.EC.0) GO TO 49
49 CONTINUE
    IF(INSUB.GT.1.AND.DLRS.GT.(.01*DL)) GO TO 60
    GO TO 600
C SMALL-ANGLE APPROXIMATION
50 ARGYY=-(YR-Y1)**2/DENH**2
    IF(ARGYY.LT.-10.) GO TO 500
    FAC=0.5*(FAC1+FAC2)
    BRAC=EXP(ARGYY)
2417 CONTINUE
    CBARQ=CBAR
    CBAR=CBAR+(CBFF2*QL*DLN*FAC*BPAC/(SIGH*SIGV)
    IF (CBARQ.EC.0) GO TO 499
    IF(ABS((CBARQ-CBAR)/CBAR).LE..00010) GO TO 600
499 CONTINUE
    IF(ASNF.LT.0.C01) ASNF=0.001
    IF(INSUB.LT.1) GO TO 600

```

	IF(DLRS.LT.(.01*DL)) GO TO 600	00001080
	IF(NSUB.GT.1.AND.DLRS.GT.(.01*DL)) GO TO 60	00001081
55	NSUB=1.+DL1/ELEM	00001082
	RSUB=NSUB	00001083
	SEGL=CLN/RSUB	00001084
	ISUB=0	00001085
	DELX=(X2-X1)/RSUB	00001086
	DELY=(Y2-Y1)/RSUB	00001087
	DELZ=(Z2-Z1)/RSUB	00001088
	XRS=X2-X1	00001089
	YRS=Y2-Y1	00001090
	ZRS=Z2-Z1	00001091
	X2=X1	00001092
	Y2=Y1	00001093
	Z2=Z1	00001094
60	ISUB=ISUB+1	00001095
	IF(ISUB.EQ.1) GO TO 65	00001096
	NSUB=1.+DLRS/ELEM	00001097
	RSUB=NSUB	00001098
	SEGL=DLRS/RSUB	00001099
	DELX=XRS/RSUB	00001100
	DELY=YRS/RSUB	00001101
	DELZ=ZRS/RSUB	00001102
65	CONTINUE	00001103
	XRS=XRS-DELX	00001104
	YRS=YRS-DELY	00001105
	ZRS=ZRS-DELZ	00001106
	X1=X2	00001107
	Y1=Y2	00001108
	Z1=Z2	00001109
	X2=X2+DELX	00001110
	Y2=Y2+DELY	00001111
	Z2=Z2+DELZ	00001112
	DLRS=DLRS-SEGL	00001113
	X=.5*(X1+X2)	00001114
	Y=.5*(Y1+Y2)	00001115
	Z=.5*(Z1+Z2)	00001116
	GO TO 5	00001117
100	YL = Y1	00001118
	ZL = Z1	00001119
	IF (Z1 .IF. Z2) GO TO 105	00001120
	YL = Y2	00001121
	ZL = Z2	00001122
105	FAC3=0.5*SIGVZ/(COFF1*HL1PM)	00001123
	IF(DWC.GT.2.*XZ) GO TO 200	00001124
	DENZL=0.47*HL1PM	00001125
	DENZL2=DENZL**2	00001126
	IF(ASNF.LT.0.1.AND.(ABS(SNTH)).LT.0.1) GO TO 101	00001127
	GO TO 102	00001128
101	ARGZ1=-(ZP-ZL)**2/DENZL**2	00001129
	ARGZ2=-(ZR+ZL)**2/DENZL**2	00001130
	GO TO 103	00001131
102	TL=XZ/WS	00001132
	DENHL=1.4142*SIGY(JSTAB,TL)	00001133
	DENL=CSNH**2*SNF1**2*DENZL**2+SNTH**2*DENHL**2	00001134

ARGZ1=-((YR-YL)*SNTH-(ZR-ZL)*CSTH*SNFI)**2/DEND	00001135
ARGZ2=-((YR-YL)*SNTH-(ZR+ZL)*CSTH*SNFI)**2/DEND	00001136
103 FAC1=EXP(ARGZ1)	00001137
FAC2=EXP(ARGZ2)	00001138
FAC1=FAC1*(DWC-XZ)*(FAC3-FAC1)/XZ	00001139
FAC2=FAC2*(DWC-XZ)*(FAC3-FAC2)/XZ	00001140
GC TO 39	00001141
200 FAC1=FAC3	00001142
FAC2=FAC3	00001143
GC TO 39	00001144
500 IF(DLRS.LT.(.01*DL)) GO TO 600	00001145
IF(1SAC.EQ.1.AND.NSUB.EQ.0) GO TO 55	00001146
IF(NSUB.GE.1) GO TO 60	00001147
600 CAVL=CBAP	00001148
RETURN	00001149
END	00001150


```

SUBROUTINE DIESFLGAL,XMIGAL,XMILE,PLLTNT,IUNIT,NPLTS) 00001151
C-----GAL = TOTAL GALLONS OF DIESEL FUEL CONSUMED;IF USING MILES, GAL MU00001152
C-----BE SET EQUAL TO 0.0-----00001153
C-----XMIGAL = MILES PER GALLON; CAN OMIT IF USING GALLONS-----00001154
C-----XMILE = MILES TRAVELED; NEED NOT BE SPECIFIED IF USING GALLONS---00001155
C-----XPT,XCO,ETC. ARE THE EMISSIONS IN UNITS OF POUNDS OR GRAMS FOR---00001156
C-----PARTICULATES, CARBON MONOXIDE, HYDROCARBONS, ETC.-----00001157
C-----IUNIT = 0 MEANS EMISSIONS IN GRAMS ELSE EMISSIONS IN POUNDS-----00001158
      DIMENSION PLLTNT(5) 00001159
      COMMON/FUEL/EF(5),EFG(5) 00001160
      COMMON/PL/NPT,JJ(5) 00001161
C*****00001162
C      COMPUTE DIESEL ENGINE POWERED MOTOR VEHICLE EMISSIONS. 00001163
C*****00001164
      A=GAL 00001165
      IF(A.EQ.0.0) A=XMILE/XMIGAL 00001166
      CCNFACT=1./454. 00001167
      IF(IUNIT.EQ.0) CCNFACT=1.0 00001168
      DO 10 M=1,NPLTS 00001169
        I=JJ(M) 00001170
        10 PLLTNT(I)=A*EF(I)*CCNFACT 00001171
      RETURN 00001172
      END 00001173

```



```

SUBROUTINE CTEDMD (IMHUR,SRVHR,IUNIT,PLLTNT,DSL,GSLN,NPLTS) 0001174
DIMENSION CNSMRT(14),SRVHR(14),PLLTNT(5) 0001175
DIMENSION A(5) 0001176
COMMON/POL/PPT,JJ(5) 0001177
COMMON/FUEL/FFD(5),FFG(5) 0001178
DATA CNSMRT/1.8,0.7,1.75,3*1.5,2.0,1.7,2.35,1.75,1.4,2.0,5.0,1.5/ 0001179
C***** 0001180
C-----SUBROUTINE CALCULATES HOURLY EMISSIONS IN PASSENGER GATE AREA RESU0001181
C-----FROM DEMANDS PLACED ON GROUND SERVICE VEHICLES-----0001182
C***** 0001183
C-----CALCULATE GALLONS OF DIESEL USED BY AIRSTART AND GROUND POWER VEH0001184
DO 30 I=1,5 0001185
30  PLLTNT(I)*0.0 0001186
GAL=0.75*SRVHR(11)*8.2+0.50*SRVHR(13)*7.1 0001187
IF(GAL.EQ.0.0) GO TO 2 0001188
DSL=DSL+GAL 0001189
CALL LIESFL (GAL,0.0,0.0,PLLTNT,IUNIT,NPLTS) 0001190
2  CONTINUE 0001191
GAL=0.5*SRVHR(15)*CNSMRT(13)+SRVHR(14)*CNSMRT(14) 0001192
DO 10 I=1,12 0001193
10  GAL=GAL+SRVHR(I)*CNSMRT(I) 0001194
GSLN=GSLN+GAL 0001195
IF(GAL.EQ.0.0) GO TO 12 0001196
CALL GASLN (10.,6.0,GAL,0.0,A,NPLTS,IUNIT) 0001197
DO 20 M=1,NPLTS 0001198
1=JJ(M) 0001199
20  PLLTNT(I)=PLLTNT(I)+A(I) 0001200
12  CONTINUE 0001201
RETURN 0001202
END 0001203

```

```

SUBROUTINE GUESS2(FCTN,PGGA,PGGB,PZERO,TOL1,      00001204
1 NITMAX,NFLAG1,NFLAG3,NFLAG4)                  00001205
C                                                00001206
C CCCCC MODIFIED FOR PZERO .GT.0. ONLY          00001207
C SEE STATEMENT 16                             00001208
C                                                00001209
C THIS PROGRAM HAS BEEN TRANSLATED FOR THE      360/50 00001210
C WITH RELEASE 1-A OF THE MOD-50 TRANSDECK      00001211
C JDB                                             00001212
C DIMENSION PGG(50),ERR(50)                     00001213
C *****00001214
C THIS SUBROUTINE FINDS A ZERO OF THE FUNCTION FCTN(X) 00001215
C FCTN MUST BE DEFINED BY AN EXTERNAL FUNCTION STATEMENT. 00001216
C PGGA AND PGGB ARE TWO INITIAL GUESSES          00001217
C TOL1 = ALLOWABLE DEVIATION FROM ZERO IF NFLAG4=1 00001218
C = ALLOWABLE DIFFERENCE BETWEEN LAST TWO PZERO 00001219
C VALUES IF NFLAG4 = -1                        00001220
C NITMAX = MAX NO. OF ITERATIONS                 00001221
C NFLAG3 = 1 IF WANT PRINT OUT VIA THE SUBROUTINE 00001222
C NFLAG3 = 0 IF NO PRINT OUT DESIRED             00001223
C INITIALLY COEF SETS NFLAG1=0 . IF             00001224
C A DIVIDE CHECK OR EXCESS NO. OF ITERATIONS OCCURS, SETS NFLAG1=1 00001225
C *****00001226
C DELTP=ABS(PGGA-PGGB)                          00001227
C NFLAG1=0                                       00001228
C NIT=2                                          00001229
C PGG(1)=PGGA                                  00001230
C PGG(2)=PGGB                                  00001231
C I=3                                           00001232
C IA=1                                          00001233
C IR=2                                          00001234
C FERRA=FCTN(PGGA)                             00001235
C FERR(1)=FERRA                                00001236
C IF(NFLAG4) 2,2,4                             00001237
C 2 GO TO 5                                     00001238
C 4 VALUE=ABS(FERRA)                             00001239
C IF(VALUE-TOL1)400,400,5                      00001240
C 400 FERR=PGG(1)                              00001241
C NIT=1                                          00001242
C FERRB=FERRA                                  00001243
C GO TO 100                                     00001244
C 5 FERRB=FCTN(PGGB)                             00001245
C IF(NFLAG4) 6,6,8                             00001246
C 6 VAL=PGG(IA)-PGG(IR)                         00001247
C VALUE=ABS(VAL)                               00001248
C GO TO 9                                       00001249
C 8 VALUE = ABS(FERRB)                          00001250
C 8 IF(VALUE-TOL1) 100,100,10                  00001251
C 10 CONTINUE                                  00001252
C VALUE=ABS(FERRA-FERRB)                       00001253
C IF(VALUE-1.E-28) 75,75,15                   00001254
C 15 PGG(1)=PGG(IR) - FERRB*(PGG(IA)-PGG(IR))/(FERRA-FERRB) 00001255

```

16	IF(PGG(1).LE.C.PGG(1)=.001*DELTP	00001257
20	ERRA=ERRB	00001258
	ERR(1B)=ERRP	00001259
	PGGB=PGG(1)	00001260
	I=I+1	00001261
	IA=I-2	00001262
	IP=I-1	00001263
	NIT=NIT+1	00001264
	IF(NIT-NITMAX) 5,5,70	00001265
		00001266
70	PRINT 71,NITMAX	00001267
71	FORMAT(1H1,45H MAX. NO. ITER. FOR PZERO EXCEEDED,NITMAX = 15 //)	00001268
	NFLAG1 = 1	00001269
	GO TO 100	00001270
		00001271
75	CONTINUE	00001272
	NFLAG1=1	00001273
	GO TO 100	00001274
		00001275
100	IF(NFLAG2) 80,80,101	00001276
80	J=I-1	00001277
	ERR(J)=ERRP	00001278
	PZEROB=PGGB	00001279
	GO TO 125	00001280
		00001281
101	PZEROC=PGGB	00001282
	J=I-1	00001283
	ERR(J)=ERRP	00001284
104	FORMAT (// ///)	00001285
105	FORMAT(22H NO. OF ITERATIONS = 15 ///)	00001286
115	FORMAT(4X, 4H NIT ,9X, 6H GUESS , 16X, 6H ERROR //)	00001287
120	FORMAT(1B,2F20.8)	00001288
125	RETURN	00001289
	END	00001290

```

FUNCTION HMX(JSTAB,MON,NHR,WS)
  DIMENSION HMM(12)
  DATA HMM/400.,570.,1000.,930.,1120.,1310.,1180.,990.,980.,570.,
    1680.,480./
  C *****
  C   MIXING DEPTH (IN FEET) IS DETERMINED ON THE BASIS OF STABILITY CLASS
  C   AND HULZORTH TABLE OF MEAN MONTHLY MAX. MIXING DEPTHS.
  C *****
  HFT=3.281*HMM(MON)
  GO TO (10,20,20,30,40),JSTAB
10  HMX=1.5*HFT
   RETURN
20  HMX=HFT
   RETURN
30  HMX=HFT
   IF(NHR.GE.7.AND.NHR.LE.11) HMX=.5*(HFT+328.)
   IF(NHR.GE.17.AND.NHR.LE.21) HMX=.5*(HFT+328.)
   IF(WS.GE.13.8) HMX=HFT
   RETURN
40  HMX=328.
   RETURN
END

```



```

SUBROUTINE LINE(XR,YP,ZR,X1,Y1,Z1,X2,Y2,Z2,CUNC) 00001313
COMMON/LN/DL,XW1,YW1,ZW1,XW2,YW2,ZW2,COEF1,COEF2,VA1,VA2,VD1,VD2, 00001314
-A,TIME,VA12,VA22,VD12,VD22,WS2,WSC,IAD,SNAN,CSAN,V1,V2,V12,V22, 00001315
-TAIL,VS,PR,SP 00001316
COMMON/MET/WS,WD,JSTAB,HLID,TEMP,XL,SUDBY,SUDBZ 00001317
COMMON/LN1/IACC 00001318
(***** 00001319
C PREPARE GEOMETRIC AND KINEMATIC PARAMETERS FOR THE FINITE LINE 00001320
C SOURCE DISPERSION MODEL CAVL. 00001321
(***** 00001322
IAD=IADL 00001323
AL2=(X2-X1)*(X2-X1)+(Y2-Y1)*(Y2-Y1)+(Z2-Z1)*(Z2-Z1) 00001324
DL=SQRT(AL2) 00001325
IF(IAD.EQ.0) GO TO 20 00001326
GO TO (1,2),IAD 00001327
C FOR ARRIVAL, TIME IS COMPUTED. 00001328
1 V1=VA1 00001329
V2=VA2 00001330
V12=VA12 00001331
V22=VA22 00001332
TIME=2.*DL/(V1+V2) 00001333
GO TO 10 00001334
C FOR DEPARTURE, DL IS COMPUTED. 00001335
2 V1=VD1 00001336
V2=VD2 00001337
V12=VD12 00001338
V22=VD22 00001339
DL1=.5*TIME*(V1+V2) 00001340
X2=X1+(X2-X1)*DL1/DL 00001341
Y2=Y1+(Y2-Y1)*DL1/DL 00001342
DL=DL1 00001343
TIME=TIME 00001344
10 A=(V2-V1)/TIME 00001345
20 XW1=0. 00001346
YW1=0. 00001347
ZW1=Z1 00001348
U=1. 00001349
TAU=1. 00001350
TWOP1=2.*3.1415927 00001351
SQF=SQRT(TWOP1) 00001352
COEF1=1./(SQF*U*TAU) 00001353
COEF2=2./(TWOP1*U*TAU) 00001354
XW2=(X2-X1)*(CSAN+(Y2-Y1)*SNAN 00001355
YW2=(X1-X2)*SNAN+(Y2-Y1)*CSAN 00001356
ZW2=Z2 00001357
XPCP=(XR-X1)*CSAN+(YP-Y1)*SNAN 00001358
YPCP=(X1-XP)*SNAN+(YR-Y1)*CSAN 00001359
ZPCP=ZR 00001360
IF(IAD.EQ.0) GO TO 50 00001361
CSA = -XW2 / DL 00001362
WSC = 2 * WS * CSA 00001363
EXT = TAIL / DL 00001364
DX = XW2 * EXT 00001365

```

DY = YW2 * EXT	00001366
XW2 = XW2 + DX	00001367
YW2 = YW2 + DY	00001368
XRCF = XRCF + DX	00001369
YRCF = YRCF + DY	00001370
VS = TAIL / TIME	00001371
VT = V2 + VS	00001372
SP2 = WS2 + VT * VT + WSC * VT	00001373
SP = SQRT (SP2)	00001374
W1 = V1 + VS	00001375
W2 = V2 + VS	00001376
YY1 = SQRT(WS2 + W1 * (W1 + WSC))	00001377
YY2 = SQRT(WS2 + W2 * (W2 + WSC))	00001378
ARG = (YY2 + W2 + WSC/2.) / (YY1 + W1 + WSC/2.)	00001379
G = YY2 - YY1 - WSC/2. * ALOG(ARG)	00001380
RR = A / G	00001381
50 CCN=CAVL(XRCF,YRCF,ZRCF)	00001382
RETURN	00001383
END	00001384

```

SUBROUTINE PSEUDO(DS,U,V,TX,TY,TZ,DX,DY,MSTB,HS,NCL) 00001385
EXTERNAL SIGGX,SIGGZ 00001386
COMMON/STAB11/NSTB,SIGXD,SIGZO 00001387
COMMON/WDUN/WSAVE 00001388
C ***** 00001389
C HORIZONTAL AND VERTICAL SOURCE WIDTHS ARE CONVERTED TO PSEUDO 00001390
C TRANSPORT TIMES. 00001391
C ***** 00001392
EPP=.001 00001393
A=1. 00001394
B=.5 00001395
C=.1 00001396
D=.01 00001397
NUL=10 00001398
NP=0 00001399
N4=1 00001400
WSAVE=SQRT(U*U+V*V) 00001401
NSTB=MSTB 00001402
IF(NCL.GE.2) GO TO 9 00001403
SIGXD=DS 00001404
CALL GUESS2(SIGGX,A,B,TX,EPP,NUL,NF1,NP,N4) 00001405
TY=TX 00001406
9 SIGZO=HS 00001407
10 CALL GUESS2(SIGGZ,C,D,TZ,EPP,NUL,NF1,NP,N4) 00001408
40 TX=U*TX 00001409
DY=V*TY 00001410
RETURN 00001411
END 00001412

```

4


```

FUNCTION SIGGX(THOUR)
COMMON/STAB11/NSTR,SIGX0,SIGZ0
SIGGX=SIGY(NSTR,THOUR)-SIGX0
RETURN
END
00001446
00001447
00001448
00001449
00001450

FUNCTION SIGGZ(THOUR)
COMMON/STAB11/NSTR,SIGX0,SIGZ0
SIGGZ=SIGZ(NSTR,THOUR)-SIGZ0
RETURN
END
00001451
00001452
00001453
00001454
00001455

FUNCTION SIGY(J,THOUR)
COMMON/WOUN/WSAVE
DIMENSION A(7),B(7)
DIMENSION C(5),D(5)
DATA C/155.,100.,68.,50.,24./, D/.91.,.90.,.93.,.90.,.93/
DATA A/2.1511,1.5454,1.0606,.68465,.59366,.59366,.59366/
DATA B/.87326,.88261,.89031,.88866,.89138,.89138,.89138/
DATA CONV/.000621371/
00001456
00001457
00001458
00001459
00001460
00001461
00001462
00001463
C *****
C COMPUTE HORIZONTAL DISPERSION COEFFICIENT.
00001464
C *****
C J=1,2,3,4,5 ARE CLASSES R,C,I,F,F
00001465
C XX AND SIGXY ARE IN MILES
00001466
C TSEC=THOUR*3600.
00001467
C
00001468
C SIGY=(A(J)*TSEC**B(J))*CONV*.87
00001469
C WSAVE IS MEAN WIND SPEED UP TO TIME T.
00001470
C XX=WSAVE*THOUR*1.609
00001471
C JJ=MAX0(J-1,1)
00001472
C SIGXY=C(JJ)*(XX**D(JJ))*0.000889
00001473
C .000889=(1/1609.)*(6**.2)
00001474
C SIGY=MAX1(SIGY,SIGXY)
00001475
C
00001476
C DISPERSION COEFFICIENTS BASED ON TURNER WORKBOOK.
00001477
C WHERE THE SIGMAS GIVEN IN THE WORKBOOK FOR
00001478
C TEN MINUTE SAMPLINGS ARE SCALED TO 1 HOUR
00001479
C AVERAGES BY A FACTOR OF 1.43
00001480
C RETURN
00001481
C END
00001482
00001483
00001484

```

```

FUNCTION SIGZ(J,THOUR)                                00001485
COMMON/WDUN/WSAVE                                     00001486
DISPERION COEF. BASED ON TURNERS WORKBOOK           00001487
C J=1,2,3,4,5 ARE CLASSES B,C,D,E,F               00001488
C X AND SIGZ ARE IN MILES                           00001489
DIMENSION C(3,5),D(3,5)                             00001490
REAL TIME(7),A(7,6),B(7,6)                          00001491
C                                                     00001492
DATA TIME/0.,300.,1000.,3000.,10000.,30000.,172000./ 00001493
DATA A/.17122,.27668,.41219,.51921,.50963,.47639,.52140, 00001494
1 .11062,.39953,.41219,.57145,.76485,.71936,.88886, 00001495
2 .01338,.16640,.41219,1.0813,1.9467,2.3931,1.8877, 00001496
3 .01338,.16640,.41219,2.2830,2.9850,3.8684,6.7452, 00001497
3 .01338,.16640,.41219,2.3333,5.7990,16.897,20.673, 00001498
3 .01338,.16640,.41219,5.6801,14.599,64.577,54.149/ 00001499
DATA B/1.2058,1.0572,.92365,.84130,.79689,.76308,.69839, 00001500
1 1.2864,.99275,.92365,.82449,.72571,.69082,.60486, 00001501
2 1.5922,1.1195,.92365,.73217,.59047,.51700,.49583, 00001502
3 1.5922,1.1195,.92365,.63883,.53706,.45686,.33677, 00001503
4 1.5922,1.1195,.92365,.63646,.46497,.29621,.21517, 00001504
5 1.5922,1.1195,.92365,.55016,.37541,.16667,.12177/ 00001505
DATA C/110.,110.,110.,60.,60.,60.,33.,33.,40.,21.5,21.5,36.,14., 00001506
114.,23.5/ 00001507
DATA D/1.,1.09,1.07,.92,.92,.92,.80,.61,.53,.70,.56,.35,.78,.53, 00001508
1.30/ 00001509
DATA CONV/.000621371/ 00001510
C ***** 00001511
C COMPUTE VERTICAL DISPERSION COEFFICIENT. 00001512
C ***** 00001513
TSEC=THOUR*3600. 00001514
DO 10 N=2,7 00001515
IF(TSEC.LE.TIME(N))GO TO 20 00001516
10 CONTINUE 00001517
IF(N.GT.7) N=7 00001518
C TIME OF TRAVEL SHOULD BE LESS THAN 172.E03 SEC APPROX. 2 DAYS 00001519
20 CONTINUE 00001520
N=N-1 00001521
SIGZ=(A(J,N)*TSEC**B(J,N))*CONV 00001522
C TURNER TEST EQUATION 00001523
C SIGZ=(1.17518*TSEC**.72012)*CONV 00001524
XX=WSAVE*THOUR*1.609 00001525
I=1 00001526
IF(XX.GT.1.) I=2 00001527
IF(XX.GT.10.) I=3 00001528
JJ=MAX0(J-1,1) 00001529
SIGTZ=(C(I,JJ)*XX**D(I,JJ))*0.000714 00001530
C .000714=(1/1609)*(20/10)**.2, ASSUMING THAT THE VERTICAL DISPER- 00001531
C SION COEFFICIENT IS INSENSITIVE TO SAMPLING TIMES OVER 20 MIN. 00001532
SIGZ=AMAX1(SIGZ,SIGTZ) 00001533
RETURN 00001534
END 00001535

```

```

FUNCTION TRAN (NS,KSTAB,HEFA,NRFLAG,IRACK) 00001536
COMMON/DELTA/DELY,DELZ 00001537
COMMON/LOC/DW,CW 00001538
COMMON/MET/WS,WD,JSTAB,HMIX1,TEMP,CL,SUDGY,SUDGZ 00001539
COMMON/PL4/XS(5),YS(5),STKH(5),WIT1(5) 00001540
COMMON/RECPT/HRECPA,HTAEPD,ZRECPG 00001541
COMMON/SEUDC/TX,TY,TZ 00001542
COMMON/XTRAN/WSMD,NCALM,SQ2PI 00001543
COMMON/WDUN/WSAVE 00001544
(***** 00001545
C COMPUTE COUPLING COEFFICIENT AT RECEPTOR DUE TO POINT AND AREA 00001546
C SOURCE. 00001547
(***** 00001548
C IF(KSTAB.GT.0) HAVE PLUME INITIALLY ABOVE LID. 00001549
ZS=STKH(NS)/5280. 00001550
HEFF=HEFA/5280. 00001551
WIT=WIT1(NS) 00001552
JSTABT=JSTAB 00001553
WSAVE=WSMD 00001554
HRECPD=HRECPA/5280. 00001555
ZKEEP=HRECPD 00001556
ADD1=0. 00001557
ADD2=0. 00001558
ADD3=0. 00001559
ADD4=0. 00001560
ADD5=0. 00001561
ADD6=0. 00001562
WJWG = 0. 00001563
XL = CL 00001564
C 00001565
IF(KSTAB.GT.0) GO TO 121 00001566
HLID=HMIX1/5280. 00001567
GOTO 140 00001568
121 JSTABT=4 00001569
IF(KSTAB.EQ.2) GOTO 130 00001570
JSTABT=5 00001571
130 CONTINUE 00001572
HLID=1000./5280. 00001573
XL=30./5280. 00001574
140 CONTINUE 00001575
C IF PLUME BELOW LID AND RECEPTOR ABOVE, TRAN=0. 00001576
IF(HRECPD.GT.HLID.AND.KSTAB.EQ.0) GOTO 76 00001577
IF(WSAVE .LE. WJWG) GO TO 9596 00001578
DMIN=4BS(CW) 00001579
TMIN=DW/WSAVE 00001580
305 CONTINUE 00001581
TT=TMIN+TY 00001582
IF(TT.LE.0.) GOTO 76 00001583
IF(NRFLAG.NE.0) GO TO 143 00001584
TMIN = 0. 00001585
IF (DW .GE. WIT) TMIN = (DW - WIT) / WSAVE 00001586
IF(IRACK.EQ.0) GO TO 131 00001587
IF(DW+WIT-DELY) 132,132,133 00001588

```


132	TMIN=C.	00001589
	GO TO 131	00001590
133	TMIN=(DW+WIT-CELY)/WSAVE	00001591
131	TT = TMIN + TY	00001592
	IF (TT.LE..01) TT=.01	00001593
	SY=SICY(JSTART,TT)	00001594
	XRP = WIT + DW	00001595
	IF (XRP .GE. 2.*WIT) GO TO 142	00001596
	DW = XRP / 2.	00001597
142	TTT = TZ + [W / WSAVE	00001598
	SZ=SIGZ(JSTART,TTT)	00001599
	FD=DMIN/SY	00001600
	FXPL=-.5*ED*FD	00001601
	IF (EXPC.LT.-20.) GOTO 76	00001602
	FCD=EXP(EXPC)	00001603
	IF (DW.GT.2.*XI) GOTO 153	00001604
	DENOM=6.2831853*WSAVE*SY*SZ	00001605
	Z1 = HEFF-ZKEEP	00001606
	EXPZ1=(-.5*(Z1/SZ)*(Z1/SZ))	00001607
	IF (EXPZ1.LT.-20.) GOTO 76	00001608
	F1=EXP(EXPZ1)	00001609
	ADD1=F1*FCD/DENOM	00001610
	IF (HEFF.GT.0.0) GO TO 171	00001611
	ADD2=ADD1	00001612
	GOTO 172	00001613
171	CONTINUE	00001614
	Z2 = HEFF + ZKEEP	00001615
	EXPZ2=(-.5*(Z2/SZ)*(Z2/SZ))	00001616
	IF (EXPZ2.LT.-20.) GOTO 61	00001617
	E2=EXP(EXPZ2)	00001618
	ADD2=ADD1*E2/E1	00001619
172	CONTINUE	00001620
	IF (HEFF.GT.HLID/2..OF.SZ.GE.(HLID-HEFF)/2.2) GO TO 18	00001621
	GO TO 61	00001622
18	CONTINUE	00001623
	IF (HEFF.LT.HLID) GO TO 174	00001624
	ADD3=ADD1	00001625
	ADD4=ADD2	00001626
	GOTO 173	00001627
174	CONTINUE	00001628
	Z3 = (2.*HLID-HEFF)-ZKEEP	00001629
	EXPZ3=(-.5*(Z3/SZ)*(Z3/SZ))	00001630
	IF (EXPZ3.LT.-20.) GOTO 61	00001631
	F3=EXP(EXPZ3)	00001632
	ADD3=ADD1*F3/E1	00001633
	Z4 = Z3+2.*ZKEEP	00001634
	EXPZ4=-.5*(Z4/SZ)*(Z4/SZ)	00001635
	IF (EXPZ4.LT.-20.) GOTO 61	00001636
	F4=EXP(EXPZ4)	00001637
	ADD4=ADD1*F4/E1	00001638
	IF (HEFF.GT.0.0) GO TO 173	00001639
	ADD5=ADD3	00001640
	ADD6=ADD4	00001641
	GO TO 61	00001642
173	CONTINUE	00001643

Z5=Z2+2.*(HLID-ZKEEP)	00001644
EXPZ5=-.5*(Z5/SZ)*(Z5/SZ)	00001645
IF(EXPZ5.LT.-20.)GOTO 61	00001646
E5=EXP(EXPZ5)	00001647
ADD5=ADD1+E5/E1	00001648
Z6=Z5+2.*ZKEEP	00001649
EXPZ6=-.5*(Z6/SZ)*(Z6/SZ)	00001650
IF(EXPZ6.LT.-20.)GOTO 61	00001651
E6=EXP(EXPZ6)	00001652
ADD6=ADD1+E6/E1	00001653
GO TO 61	00001654
153 DENOM=SQ2PI*WSAVE*SY	00001655
ADD1=EDD/(DENOM*HLID)	00001656
61 CONTINUE	00001657
TRAN=ADD1+ADD2+ADD3+ADD4+ADD5+ADD6	00001658
RETURN	00001659
143 IF(THACK.EQ.1) GO TO 144	00001660
T2=(CW+WIT)/ WSAVE+TZ	00001661
IF(LEW-WIT) 145,145,146	00001662
145 T1=TZ	00001663
TT=TY	00001664
GO TO 149	00001665
146 T1=(LEW-WIT)/ WSAVE+TZ	00001666
TT=(CW-WIT)/ WSAVE+TY	00001667
GO TO 149	00001668
144 T2=XL/ WSAVE+TZ	00001669
IF(CW+WIT-DELY) 147,147,148	00001670
147 T1=TZ	00001671
TT=TY	00001672
GO TO 149	00001673
148 T1=(CW+WIT-DELY)/ WSAVE+TZ	00001674
TT=(CW+WIT-DELY)/ WSAVE+TY	00001675
149 IF(T1.EQ.T2) GO TO 150	00001676
SZ1=SIGZ(JSTABT,T1)	00001677
GO TO 151	00001678
150 SZ1= DELZ/2.4	00001679
151 SZ2=SIGZ(JSTABT,T2)	00001680
IF(TT.EQ.TY) GO TO 152	00001681
SY=SIGY(JSTABT,TT)	00001682
GO TO 155	00001683
152 SY=DELY/2.4	00001684
155 ARGY=-(CW/SY)**2/2.	00001685
IF(ARGY.LT.-20.) GO TO 76	00001686
H=ALOG(SZ1/SZ2)/ALOG(T1/T2)	00001687
159 FXZ1=C.	00001688
FXZ2=0.	00001689
AGZ1=-((Z5-HRECPT)/SZ2)**2/2.	00001690
AGZ2=-((Z5+HRECPT)/SZ2)**2/2.	00001691
IF(AGZ1.LT.-20) GO TO 157	00001692
FXZ1=EXP(AGZ1)	00001693
157 IF(AGZ2.LT.-20) GO TO 158	00001694
FXZ2=EXP(AGZ2)	00001695
158 CONTINUE	00001696
IF((EXZ1+EXZ2).LE.0.) GO TO 76	00001697
EXY=EXP(ARGY)	00001698

C-38

```
IF(ABS(B-1.).LE..01) GO TO 2
FCNX=(T2/SZ2-T1/SZ1)/(1.-B)
GO TO 3
2 FCNX=T1*ALOG(T2/T1/SZ1
3 TRAN=XY*(EXZ1+EXZ2)*FCNX/((SQ2PI**2)*SY*DELY)
  IBACK=C
  RETURN
76 TRAN=C.
  IBACK=0
  RETURN
2596 CONTINUE
  IBACK=0
  RETURN
  END
```

```
00001699
00001700
00001701
00001702
00001703
00001704
00001705
00001706
00001707
00001708
00001709
00001710
00001711
00001712
```